Combining Measurements and Models to Predict the Impacts of Climate Change and Weatherization on Indoor Air Quality and Chronic Health Effects in U.S. Residences

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Importance of residential indoor environments

People spend the majority of their time at home (~69%)

Klepeis et al. 2001 J Exp Anal Environ Epidem 11:231-252

- The cumulative chronic health impacts from inhalation of indoor air pollutants in residences has been estimated to be between 400 and 1100 disability-adjusted life-years (DALYs) per 100,000 persons
 - Between 5-14% of the annual non-communicable, non-psychiatric disease burden in the US (excludes radon and secondhand smoke)

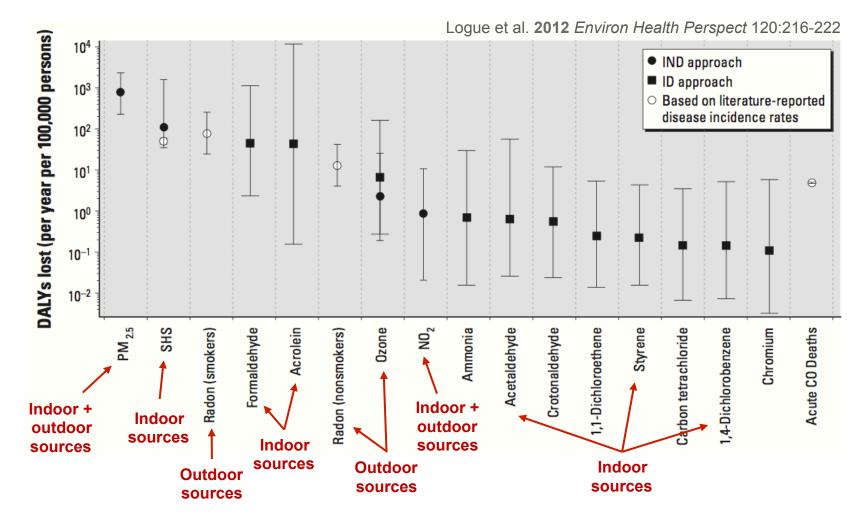
Logue et al. 2012 Environ Health Perspect 120:216-222

Cumulative lifetime cancer risk from exposure to several hazardous indoor air pollutants ranges between 1-10 excess cases per 10,000 people
 Wallace et al. 1991 Environ Health Perspect 95:7-13

Wallace et al. **1991** Environ Health Perspect 95:7-13 Sax et al. **2006** Environ Health Perspect 114:1558-1566 Hun et al. **2009** Environ Health Perspect 117:1925-1931

Residential indoor air and chronic health outcomes

Likely the **most harmful indoor air pollutants** inside residences:



Climate change, the indoor environment, and health

 Climate change is expected to influence indoor pollutant exposures in a number of direct and indirect ways

1) Changes in concentrations of outdoor pollutants of outdoor origin

2) Buildings are operated differently
 (intentionally or unintentionally)
 Changes in ventilation rates or HVAC operation alter indoor concentrations of pollutants of both indoor and outdoor origin

3) People altertheir activities(e.g., timespent indoors)

Changes in indoor exposures to pollutants of both indoor and outdoor origin

EPA STAR: Impacts of climate change on indoor air

"Combining measurements and models to predict the impacts of climate change and weatherization on indoor air quality and chronic health effects in U.S. residences"

Objectives:

- To use a combination of field measurements and a nationally representative set of dynamic residential indoor air quality models to predict indoor exposures and associated chronic health effects of several priority pollutants of both indoor and outdoor origin across:
 - 1. The current U.S. residential building stock
 - 2. The current U.S. residential building stock under future climate conditions in 2050 and 2080
 - The future U.S. building stock under future climate conditions in 2050 and 2080, considering a number of climate policy scenarios that lead to widespread application of weatherization retrofits and turnover of the existing building stock to more energy efficient homes

"Combining measurements and models to predict the impacts of climate change and weatherization on indoor air quality and chronic health effects in U.S. residences"

Research questions:

• What are the likely impacts of (a) changing meteorological conditions in future climate scenarios and (b) widespread application of weatherization retrofits on indoor air quality and chronic health effects in residential buildings across the U.S.?

Research approach:

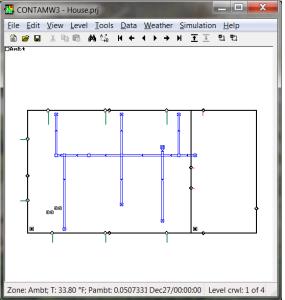
- Modeling concentrations, exposures, and chronic health effects of indoor air in homes across U.S.
- Field measurements in homes before and after energy retrofits
 - Envelope airtightness
 - Outdoor pollutant infiltration factors and penetration factors

MODELING APPROACH

Modeling approach

 We originally proposed to use CONTAM and a set of 209 home models that represent approximately 80% of the U.S. housing stock





A Collection of Homes to Represent the U.S. Housing Stock

Persily et al. 2006 NISTIR 7330; Persily et al. 2010 Indoor Air 20:473-485

Modeling approach

- Instead, we decided to develop a custom set of combined building energy and indoor air mass balance models to predict hourly energy use and indoor concentrations of a number of pollutants of both indoor and outdoor origin across the U.S. residential building stock
 - Model inputs are based on the NIST 209 home database
- The custom tool can be easily automated to run a large number of simulations
 - Allows for exploring complex interactions between energy and IAQ on a scale that is large enough to evaluate changes across the building stock under various scenarios (e.g., adoption of new energy policies or IAQ standards, as well as **future climate scenarios**)

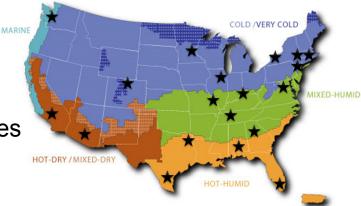
Modeling approach

The model framework combines energy simulations in BEopt and EnergyPlus with a custom hourly mass balance model for indoor pollutant simulations, written in Python

 A set of 209 dwellings (~100 home geometries) were modeled in 19 cities in 9 U.S. census and climate divisions that represent approximately 80% of all U.S. residences*

Dwelling categories:

- ✓ Detached Homes
- ✓ Attached Homes
- ✓ Manufactured Homes
- ✓ Apartments



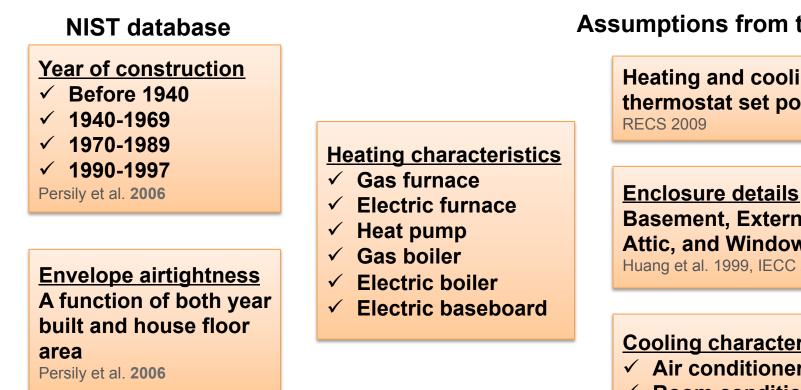
Dwelling characteristics: Floor area, year built, number of floors, number of rooms, foundation type, whether or not they have a forced air distribution system, and presence of a garage

*Home geometries and other basic characteristics are based on the NIST CONTAM database of homes representing the U.S. building stock: <u>http://www.bfrl.nist.gov/IAQanalysis/case%20studies/cwcase_11.htm</u>

Building the nationally representative model set

Selecting model home characteristics:

Home characteristics were then varied by climate zone based on 4 vintages



Assumptions from the literature

Heating and cooling thermostat set points

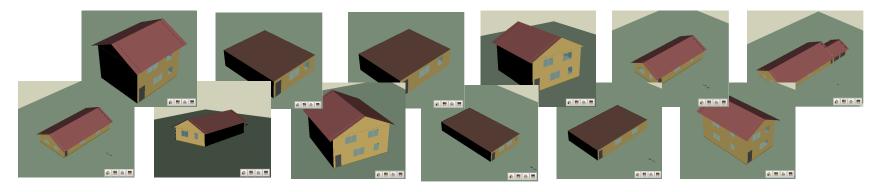
Basement, External Walls, Attic, and Windows Huang et al. 1999, IECC 2009

Cooling characteristics

- ✓ Air conditioner
- ✓ Room conditioner

Building the nationally representative model set

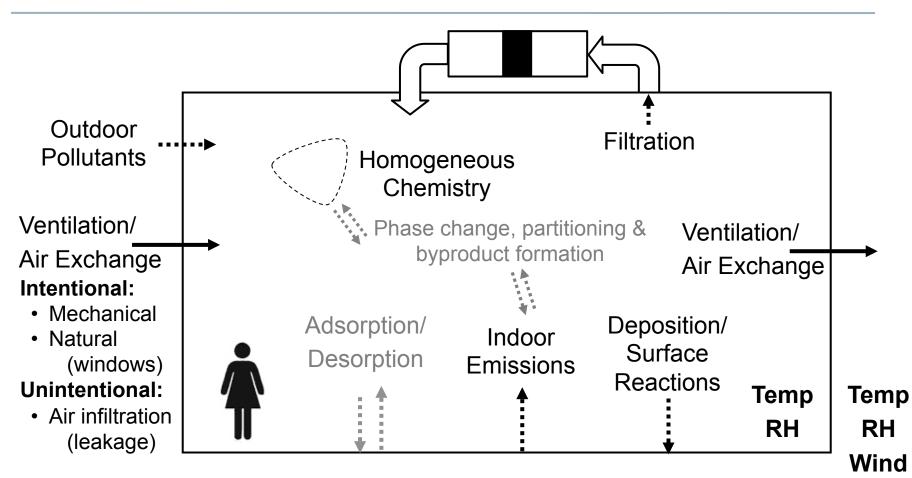
 About 100 baseline geometries of individual homes were first modeled in BEopt energy simulation software and then converted to EnergyPlus IDF input files using an automated process (explained in 2 slides)



 After energy simulations are run for each home, hourly outputs for energy use, air infiltration rates, window opening and airflows through window, and HVAC runtime are used as inputs to a custom single-zone mass balance model to predict hourly indoor concentrations of pollutants of both indoor and outdoor origin

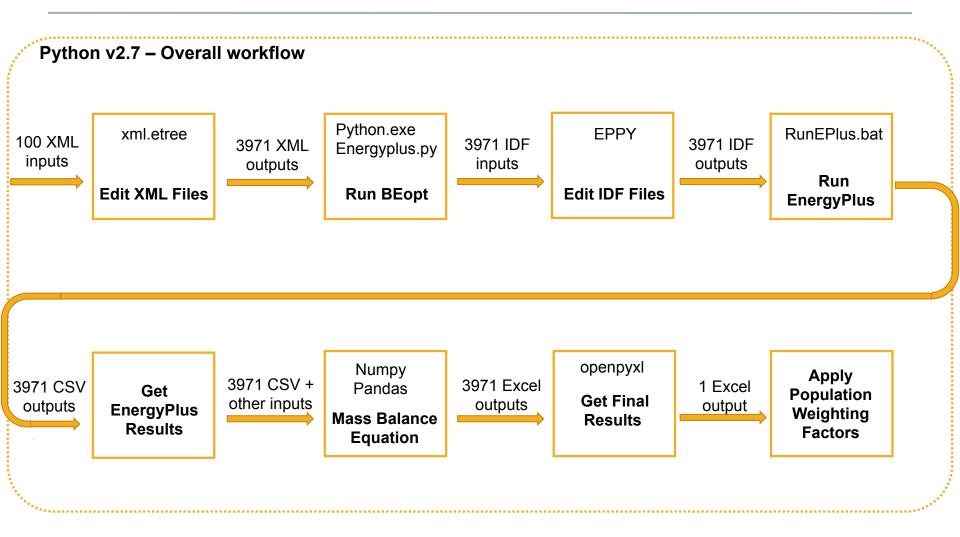
$$\frac{dC_{in}}{dt} = P\lambda_{inf}C_{out} + \frac{Q_{supply}}{V}(1 - \eta_{supply})C_{out} + \frac{E}{V} - \lambda_{inf}C_{in} - \frac{Q_{exhaust}}{V}C_{in} - \beta C_{in} - f_{filt}\frac{\eta_{filt}Q_{filt}}{V}C_{in} - kC_{in}C_{j} - \frac{dC_{in}}{dt}K_{eq}\frac{A}{V}$$

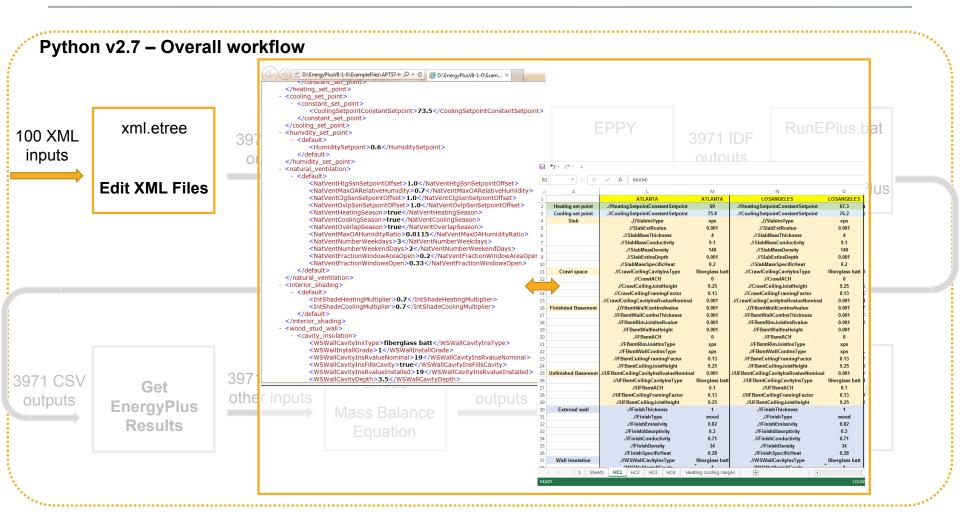
Single-zone mass balance model

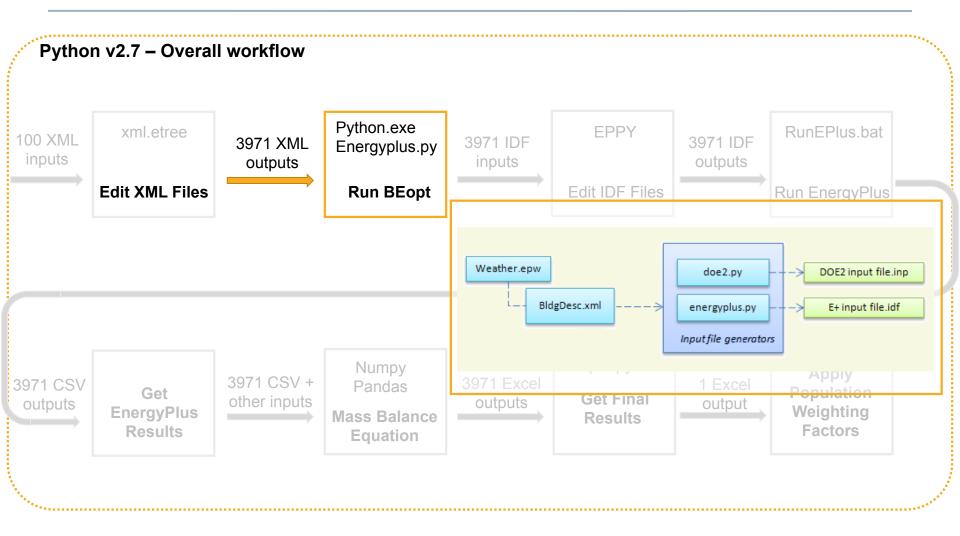


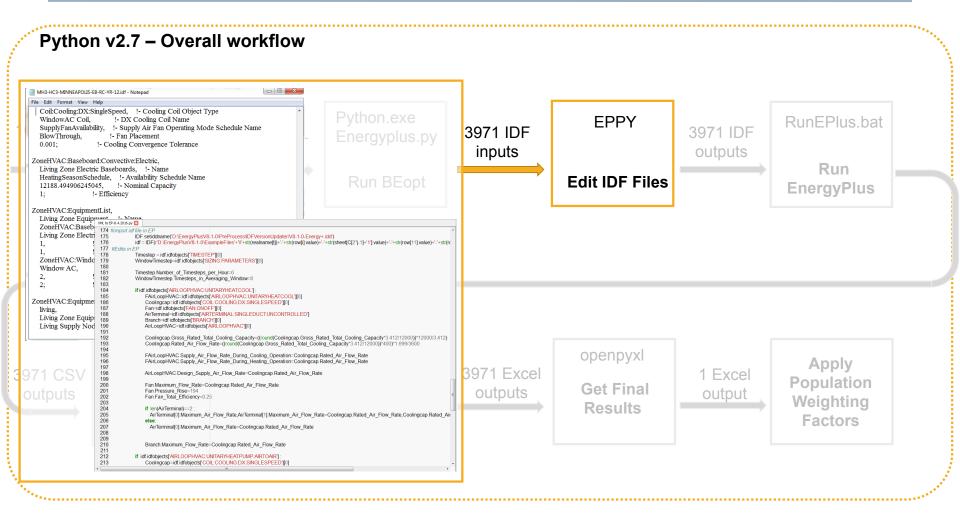
Primary pollutant classes:

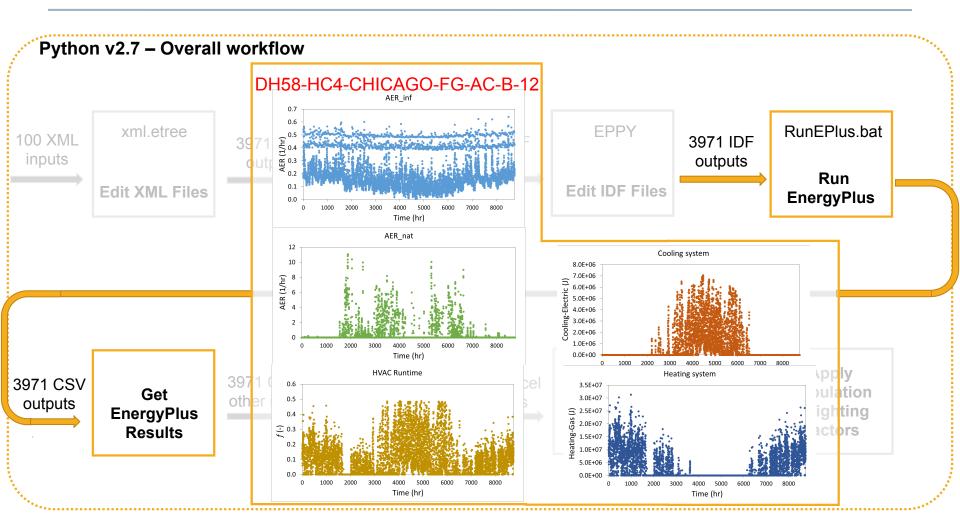
- (1) Particulate matter (e.g., PM_{2.5} and UFPs)
- (2) Non-reactive gases (e.g., several VOCs, formaldehyde)
- (3) Reactive gases (e.g., O_3 and NO_2)

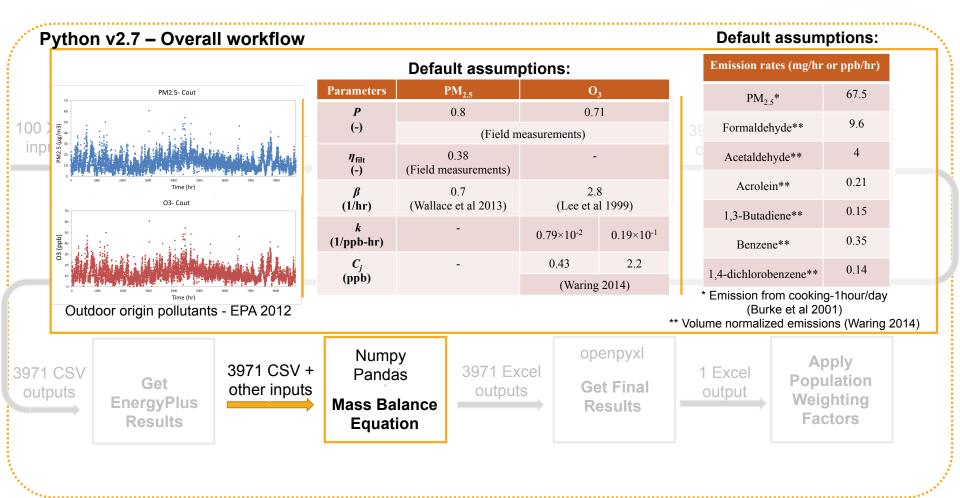












Data sources:

- EPA monitoring network for hourly pollutant concentrations of outdoor origin
- Existing literature for indoor emission rates and some physical parameters (e.g., rate constants)
- Fieldwork in this project for other physical parameters (e.g., penetration factors for PM_{2.5} and O₃)

Python v2.7 -		Home Name			Formaldehyde		etaldehyde	Acrolein	1,3-Butadiene	Benzene	1,4-dichlorobe
	Organize → Ir ★ Favorites III Desktop III Tries III Tries III Tries	AH1-HC1-MIAMI-FG-AC-B-12			19.4990	•	8.124606448	0.42654	0.304672742		0.284361226
		AH1-HC1-CORPUSCHRISTI-FG-AC-B-12			13.55413129		5.647554704	0.2965	0.211783301	0.494161	0.197664415
		AH1-HC1-PHOENIX-FG-AC-B-12			14.5633	6958	6.068070658	0.31857	0.22755265	0.530956	0.212382473
00 XML	Libraries	AH1-HC1-B	IRMINGHAM-FG	-AC-B-12	19.3597	3697	8.06655707	0.42349	0.30249589	0.705824	0.282329497
Image: Circle of Circle	AH1-HC1-CH AH1-HC1-DE AH1-HC1-NA AH1-HC1-STI AH2-HC3-BIF AH2-HC3-CII AH2-HC3-LO	LANTA-FG-AC- IICAGO-FG-AC- NVER-FG-AC-B ASHVILLE-FG-AC LOUIS-FG-AC-B RMINGHAM-FG NCINNATI-FG-A ISANGELES-FG-/	B Image: Cin-AH1 -12 Image: Cin-AH1 C-B Image: Cin-AH1 C-B Image: Cin-AH1 C-12 Image: Cin-AH2 C-12 Image: Cin-AH2	HC1-BIRMINGHAI HC1-CINCINNATI HC1-LOSANGELES HC1-NEWYORK-F HC1-WASHINGTC HC3-BOSTON-FG HC3-CORPUSCHF HC3-CORPUSCHF HC3-MIAMI-FG-A	-FG-AC S-FG-AC G-AC-B)N-FG-A -AC-B-1 USTI-FG	NEX-NEWORK 66 AC6 NEX-NEWORK 66 AC6 NEX-WARRANGTON F40 NEX-WARRANGTON F40 NEX-WARR	1.3.2298386 5.53992276 1.3.2298386 5.53992276 8-12 1.2.4486927 6.87101947 8-12 1.7.1659217 7.4609848 8-12 1.7.0582237 7.4699348 8-12 1.7.0582234 7.0989275 2 1.2.19970 4.57713112 2 1.2.19970 4.57713112 2 1.2.19970 4.57713112 2 1.2.19970 4.57813111 1 1.000026 4.51871311 2 1.2.19971 5.3000167 2 1.3.209409 7.37831311 2 1.3.209409 7.37832712 2 1.3.209409 7.37832712 2 1.3.209409 7.37832712 2 1.3.209409 7.37825797 1.2 1.3.209409 7.37825797 2 2.2.2490099 7.37825797 2 2.3.2094099 7.37825797 2 3.3123714 6.4991577941 2 3.31023714 6.499157744 <	0.2886 0.1917/2612 0.4775 0.2987 0.2987 0.2987 0.3989 0.2984 1.771 0.29898 0.3989 0.2984 1.771 0.29898 0.3971 0.26797 0.2989 0.3727 0.267970 0.26797 0.4482 0.3727 0.267970 0.26797 0.4482 0.2672 0.1802077 0.4482 0.2672 0.1802077 0.4482 0.2671 0.199732 0.4388 0.2671 0.2989 0.43807 0.2680 0.45817 0.24799 0.2680 0.45817 0.24799 0.2680 0.45817 0.24799 0.2680 0.45817 0.24799 0.4483 0.2582097 0.64892 0.2690 0.48827 0.4882 0.2690 0.4882 0.2690 0.4882 0.2771 0.179240 0.48528 0.2770 0.179240 0.48528	0.194389765 27.88795662 5.07683687 11.55545 0.239323067 27.97956621 4.44064765 12.04635 0.181339227 27.9789543 5.2096559 8.70970 0.250113096 19.0841895 2.94698579 11.08382	60 11.0227 6.84729468 11.03227 6.84729468 11.03227 6.84729468 12 10.4487 7.03225314 12 11.24867 7.03226318 12 11.24867 7.03226318 12 11.4487 7.03226318 12 11.4487 7.032956 13 10.27221 6.74481986 13 10.27228 6.74481986 14 12.4491 6.4389299 13 0.722384 5.851177 14 10.44977 7.4648364 14 10.44977 7.16448364 14 10.46976 0.7277861 14 10.44977 1.9448178 12 12.44971 1.9448178 12 12.44971 1.9448178 12 12.449718 1.9449787 13 12.4497186 1.9449787 14.14977 1.94481787 1.94481787 14.14977 1.94481787 1.94481987 14.129871787 <td>9.98857427 1.98900079 1.98900077 1.98900077 1.98900077 1.98000481 1.49857942 1.9800481 1.9</td>	9.98857427 1.98900079 1.98900077 1.98900077 1.98900077 1.98000481 1.49857942 1.9800481 1.9
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Model output:

- Hourly energy use and pollutant concentrations for each model home, which can be averaged and applied across the building stock with population weighting factors
- Concentrations will eventually be linked to DALYs and CCRs to estimate impact on chronic health 20

Model scenarios

- 1. Baseline year: 2012
 - Most recent year with both actual weather data and outdoor pollutant data available when the project began

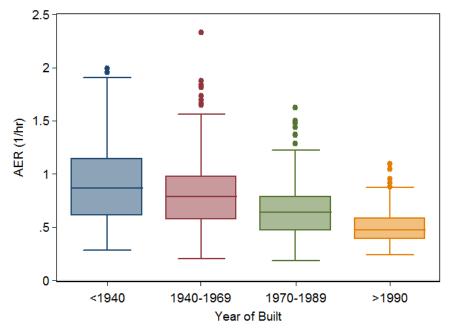
2. Future meteorological conditions: 2050 and 2080
– Using CCWorldWeatherGen to 'stretch' weather files

Jentsch et al. 2008 Energy and Buildings 40:2148-2168; Jentsch et al. 2013 Renewable Energy 55:514-524

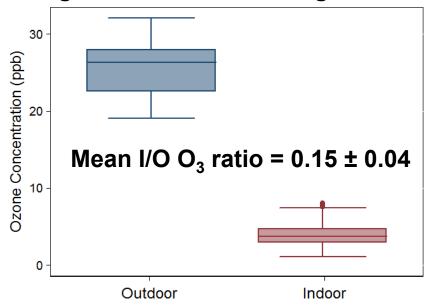
- Future meteorological conditions + climate policy responses (e.g., widespread energy retrofits, building stock turnover): 2050 and 2080
 - Not yet simulated; informed by field work

Preliminary model results: 2012

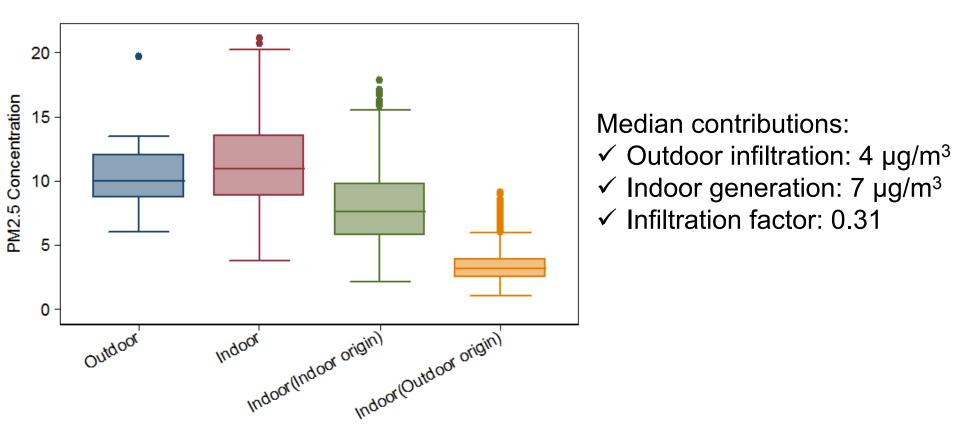
Air exchange rates are higher in older homes



Indoor ozone concentrations are within ranges seen in the existing literature

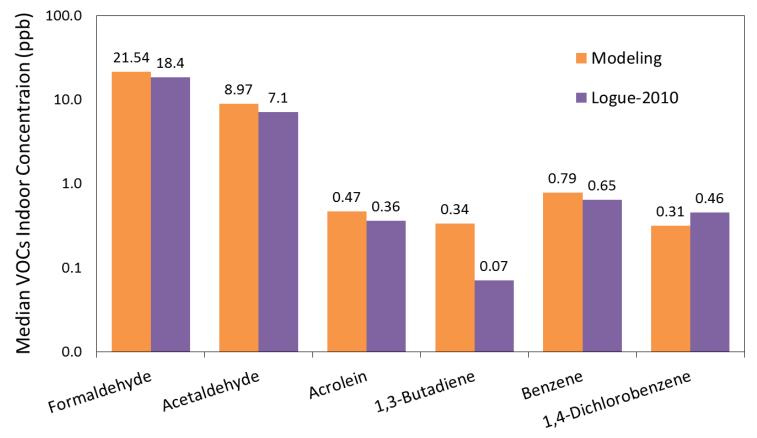


Indoor $PM_{2.5}$ concentrations compare well to existing literature



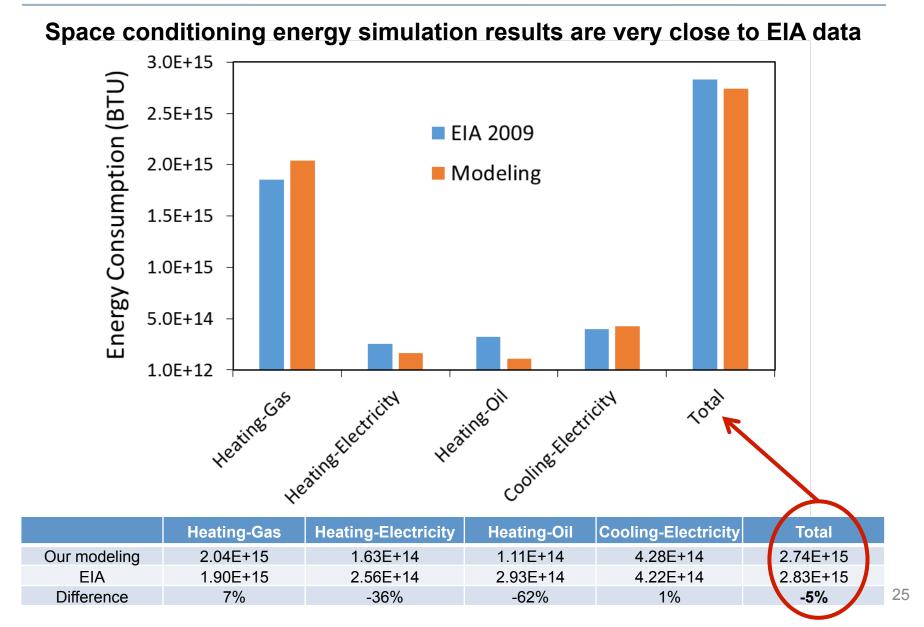
Preliminary model results: 2012

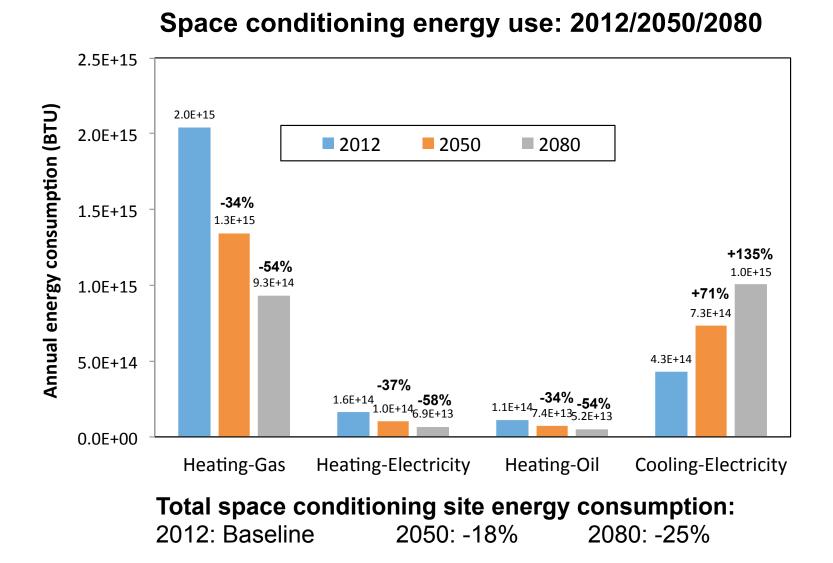
Median indoor VOC and aldehyde concentrations are similar to those reported in previous field studies

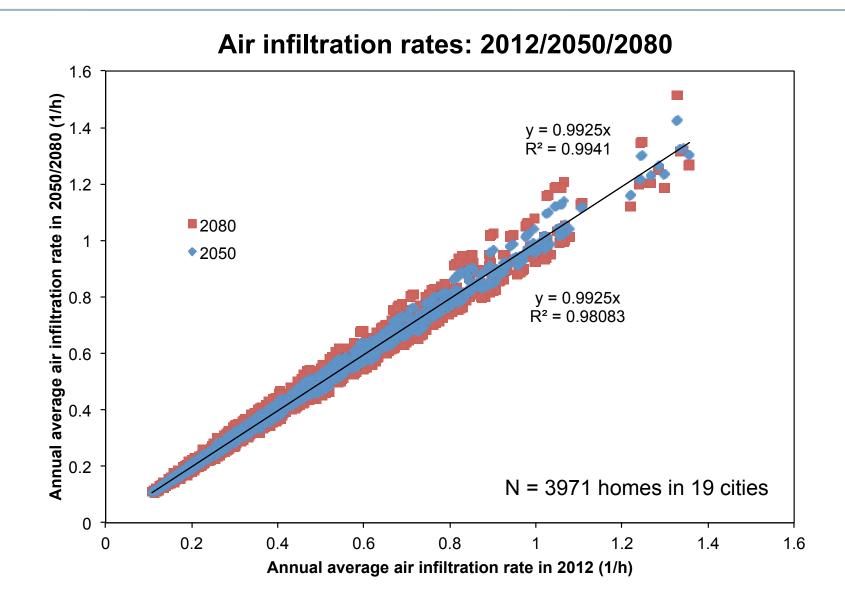


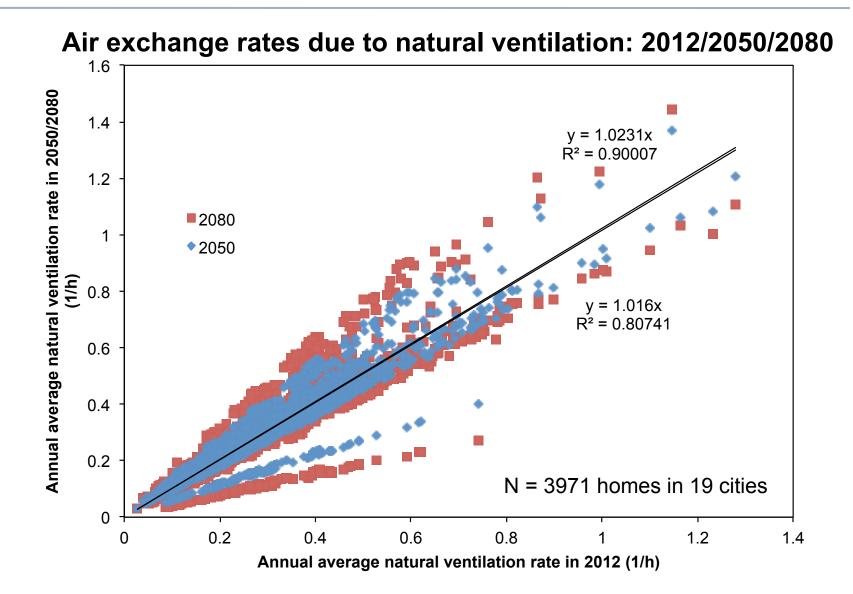
Logue et al. 2011 Indoor Air 21:92-109

Preliminary model results: 2012









Population weighted annual average indoor concentrations						
	2050 vs. 2012	2080 vs. 2012				
Formaldehyde	+0.8%	+0.8%				
Acetaldehyde	+0.8%	+0.8%				
Acrolein	+0.8%	+0.8%				
1,3-Butadiene	+0.8%	+0.8%				
Benzene	+0.8%	+0.8%				
1,4-dichlorobenzene	+0.8%	+0.8%				
Ozone	-1.5%	-2.6%				
PM _{2.5} (all sources)	-7.1%	-9.4%				
PM _{2.5} (indoor sources)	-7.7%	-10.3%				
PM _{2.5} (outdoor sources)	-5.9%	-7.6%				
NO ₂ (all sources)	+0.1%	+0.2%				
NO ₂ (indoor sources)	+0.3%	+0.2%				
NO ₂ (outdoor sources)	-0.2%	+0.4%				

FIELD MEASUREMENTS

Field measurement approach

- Goal: Measure envelope airtightness, pollutant infiltration factors (*F_{inf}*) and, when possible, pollutant penetration factors (*P*) and deposition loss rate constants (*k*) in 30 homes before and after energy retrofits are applied
 - Focus on outdoor pollutants: UFPs, $PM_{2.5}$, BC, O_3 , and NO_x
 - Help fill important data gaps in the modeling effort:
 - Initial penetration factors
 - How infiltration/penetration factors change after energy retrofits

Home recruitment status:

Target:	Completed to date:
30 homes pre/post retrofit	 6 SF homes + 3 MF units - 1 failed MF test = 8 units pre/post retrofit complete + 5 non-retrofit MF homes = 13 tests complete

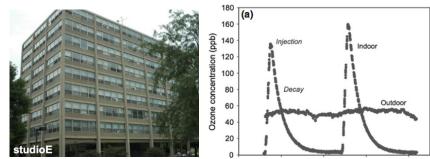


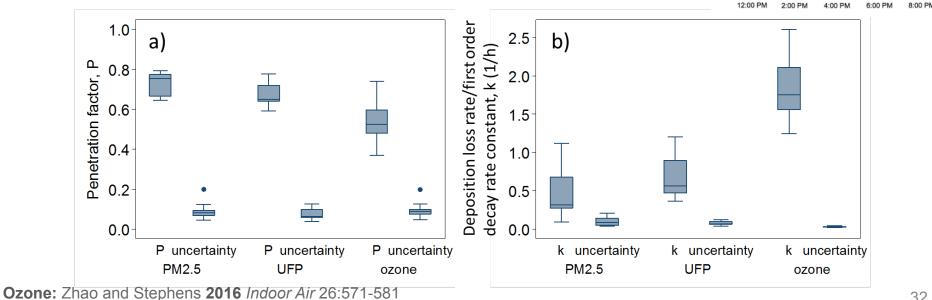
ELEVATE ENERGY

Smarter energy use for all

Field measurement approach

- We began by developing/refining penetration test methods in an unoccupied apartment unit on campus
 - Size-resolved PM (for integral measures of UFPs and PM_{25})
 - Ozone (O₃)
 - Nitrogen oxides ($NO_x = NO + NO_2$)
 - Unable to realistically measure NO_x P





PM: Zhao and Stephens (in press) Indoor Air

Field measurement approach

- Pre/post retrofit measurements in 6 SF + 2 MF units
 - Homes planning to undergo energy efficiency improvements



Homes built between 1894 and 1956 (avg = 1926)

Typical retrofit measures

- All homes:
 - Attic air sealing and blown-in insulation for all homes
 - Typically to R-49
 - Typically with attic hatch insulation
 - Weather stripping on doors
- Some homes:
 - Attic knee wall air sealing and insulation
 - Can light boxes
 - Crawlspace insulation and air sealing
 - Blown-in wall insulation in balloon framing wall cavities (2 homes)





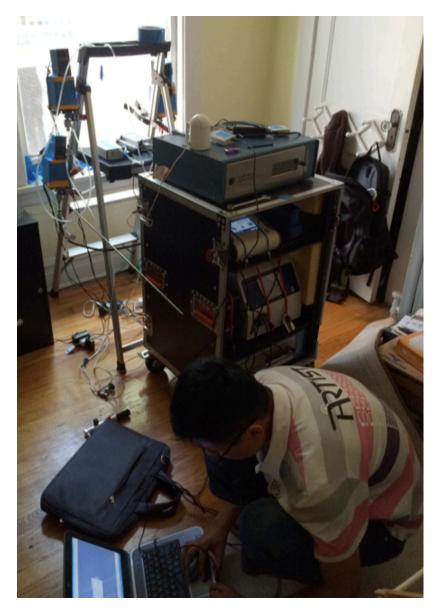


Field measurements: Blower door

- Blower door tests were performed before and after retrofits
- Resulting airtightness parameters include:
 - Leakage flow at 50 Pa (CFM_{50})
 - Effective leakage area (ELA)
 - Normalized leakage (NL)
 - Air changes per hour at 50 Pa (ACH₅₀)



Field measurements: Pollutant infiltration



Particles:

TSI Model 3330 Optical Particle Sizer (0.3 to 10 μ m) TSI Nanoscan SMPS (0.01 μ m to ~0.2 μ m) TSI DustTrak #8534 (light scattering PM_{2.5}+PM₁₀) AethLabs MicroAethelometer (for BC) (not shown)

Gas-phase pollutants:

Ozone: 2B Technologies Model 211 monitor NO_x: 2B Technologies Model 405 monitor CO₂: PP Systems SBA-5 monitor

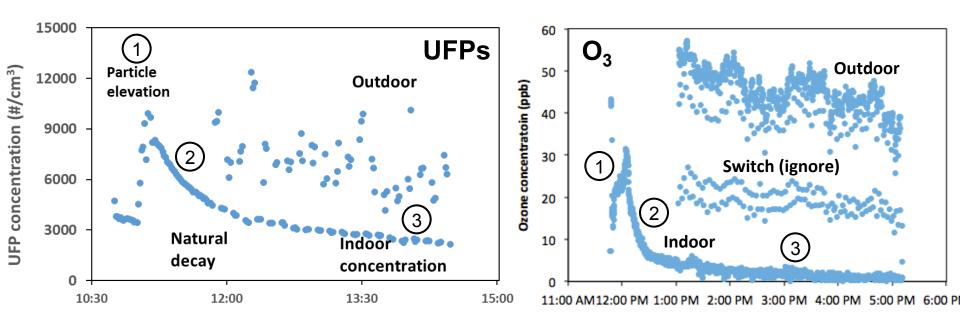
• CO₂ injection and decay to measure air exchange Shinyei/GrayWolf formaldehyde monitor (indoor only)

Electronically actuated switching valves:

Stainless steel sampling lines (for PM) Teflon sampling lines (for O_3 and NO_x)

Houses are unoccupied during testing

Example data: Pollutant infiltration

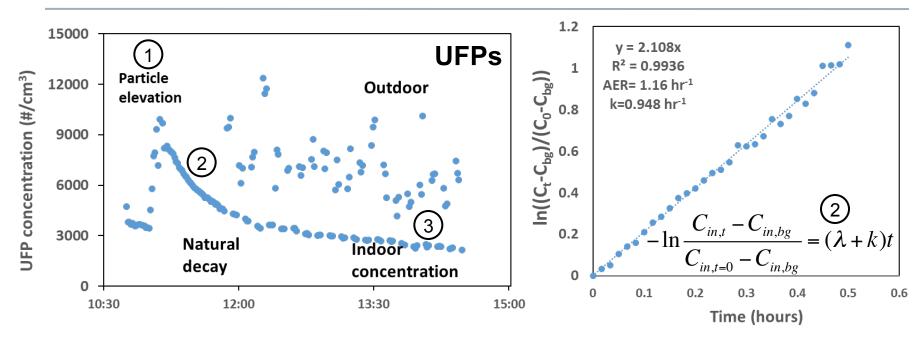


Three distinct test periods to solve for *P* and *k*:

- 1. Elevation w/ open windows + blower door
 - Indoor only for ~15 minutes
- 2. Decay to background
 - Indoor only for ~45 minutes
- 3. Response/rebound period \rightarrow infiltration factor
 - Alternating indoor/outdoor for ~3 hours

Houses are unoccupied during testing

Solving for infiltration and penetration factors



Mass or number balance:

$$\frac{dC_{in}}{dt} = P\lambda C_{out} - (\lambda + k)C_{in} \longrightarrow F_{inf} = \frac{P\lambda}{\lambda + k} \quad (3)$$

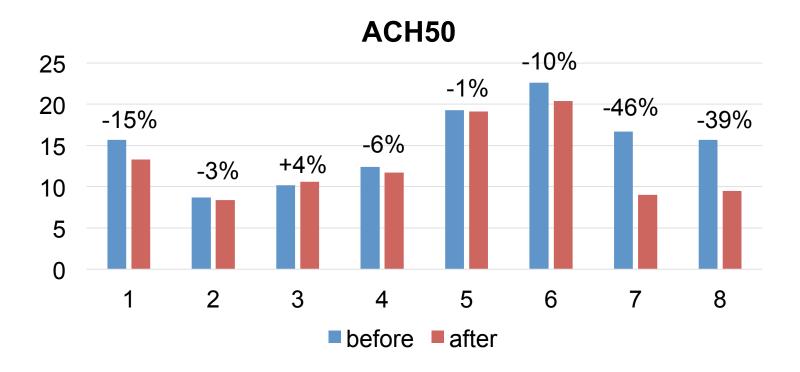
- C_{in} and C_{out} are indoor and outdoor concentrations (ppb or μ g/m³ or #/cm³)
- *P* is the penetration factor (-)
- *k* is the first order deposition loss rate constant/first order reaction rate (h⁻¹)
- λ is the air exchange rate (AER) (h⁻¹), which is simultaneously measured using injection and decay of CO₂ as a tracer gas

Solve for *P* using *k* and λ : $C_{in,t} = P\lambda C_{out,t}\Delta t + (1 - (\lambda + k)\Delta t)C_{in,t-1}$ (2+(3)) 38

Preliminary results: ACH₅₀

The retrofits reduced ACH_{50} by between -4% and 46%

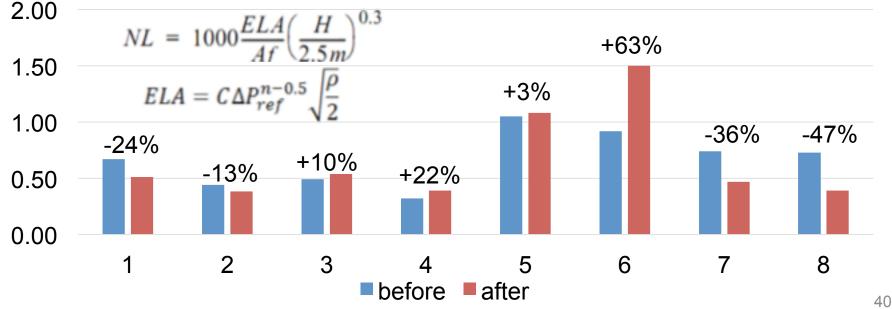
• Average change: -15%



Preliminary results: Normalized Leakage (NL)

The retrofits decreased *NL* by as much as -47% but *increased* as much as 63%

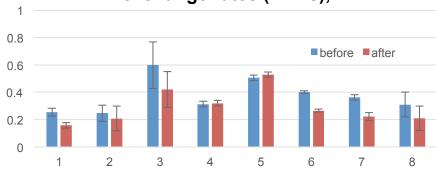
- Average change: -4%
- NL is calculated based on both the leakage coefficient (*C*) and the leakage exponent (*n*)
 - ✓ Influenced by the nature of building crack geometry



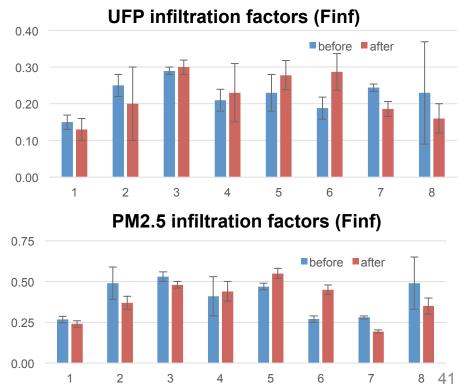
Normalized Leakage (NL)

Preliminary results: AERs and infiltration factors

- Air exchange rates were between 39% lower and 5% higher during measurements before and after retrofits
 - Influenced by airtightness, temperature differences, and wind speed/direction
- Average UFP infiltration factors were 0.22±0.04 before retrofits and 0.22±0.06 after retrofits
 - No difference (some up, some down)
- Average PM_{2.5} infiltration factors were 0.40±0.11 before retrofits and 0.39±0.12 after retrofits
 - No difference (some up, some down)
- *F_{inf}* influenced by multiple factors
 - Retrofits + climate conditions + PSDs



Air exchange rates (AERs), 1/hr



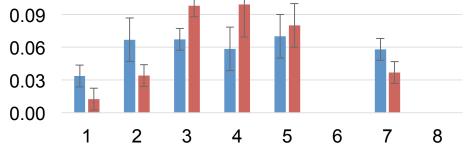
Preliminary results: AERs and infiltration factors

0.15

0.12

- Average ozone infiltration factors were 0.05±0.02 before retrofits and 0.06±0.03 after retrofits
 - No difference (some up, some down)

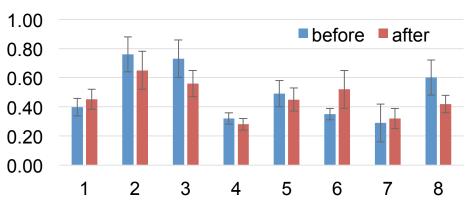
- Average black carbon infiltration factors were 0.48±0.18 before retrofits and 0.46±0.12 after retrofits
 - No difference (some up, some down)



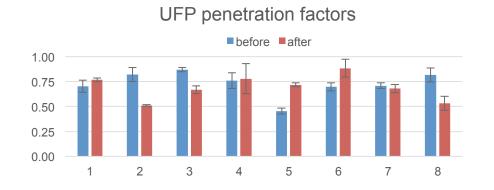
Ozone infiltration factors (Finf)

before after

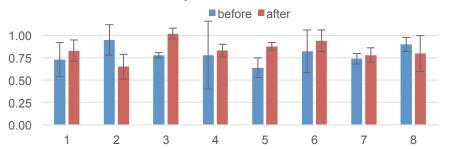


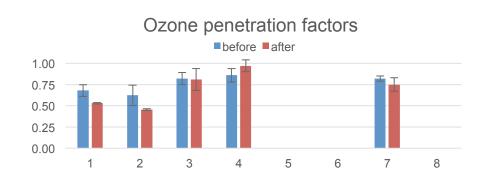


Preliminary results: UFP, PM_{2.5}, and O₃ penetration factors



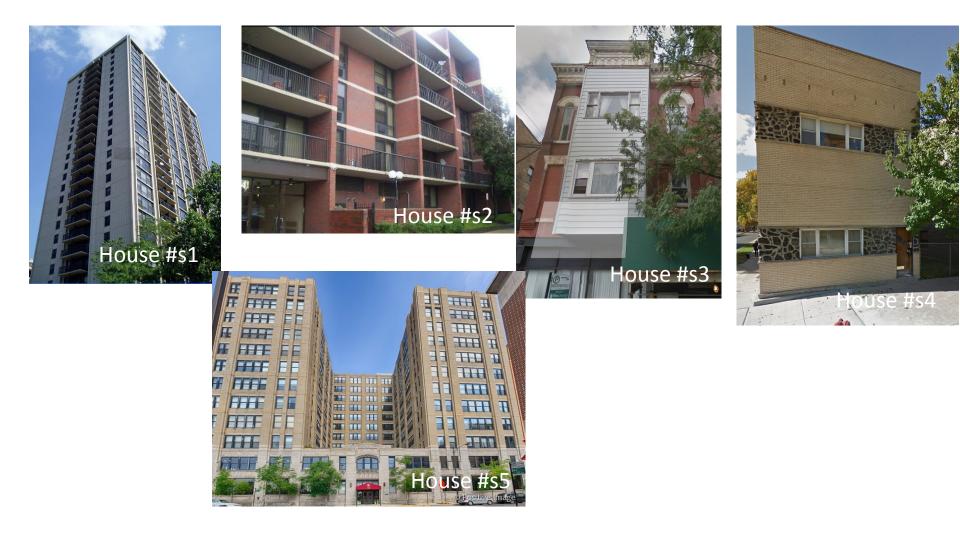
PM2.5 penetration factors



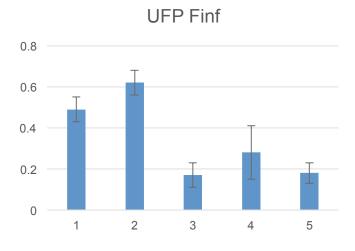


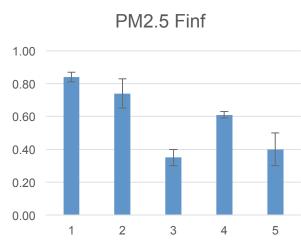
- Estimates of UFP penetration factors (mean ± SD) were 0.72±0.12 before retrofits and 0.72±0.10 after retrofits
 - Ranging from 0.46±0.03 to 0.88±0.09
- Estimates of PM_{2.5} penetration factors (mean ± SD) were 0.78±0.09 before retrofits and 0.85±0.11 after retrofits
 - Ranging from 0.64±0.11 to 1.02±0.06
- Estimates of ozone penetration factors (mean ± SD) were 0.76±0.09 before retrofits and 0.70±0.19 after retrofits
 - Ranging from 0.68±0.07 to 0.97±0.07

Non-retrofit homes (all multi-family)

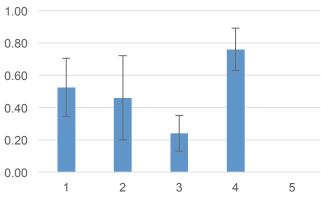


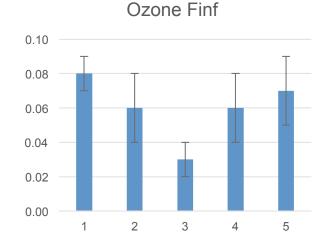
Preliminary results: Non-retrofit home infiltration factors





BC Finf





- Average (SD) UFP infiltration factors: 0.35±0.07
 - Ranging from 0.17 to 0.62
- Average (SD) PM_{2.5} infiltration factors: 0.59±0.06
 - Ranging from 0.40 to 0.84
- Average (SD) BC infiltration factors: 0.49±0.17
 - Ranging from 0.24 to 0.76
- Average (SD) ozone infiltration factors: 0.06±0.02
 - Ranging from 0.03 to 0.08

All homes were multi-family units

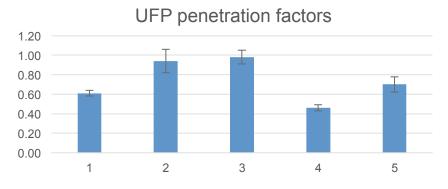
Preliminary results: Non-retrofit home penetration factors

- Estimates of UFP penetration factors (mean ± SD) were 0.74±0.07
 - Ranging from 0.46±0.03 to 0.98±0.07

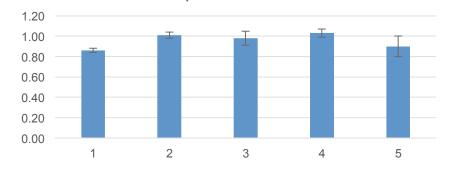
- Estimates of PM_{2.5} penetration factors (mean ± SD) were 0.96±0.05
 - Ranging from 0.86±0.02 to 1.03±0.04

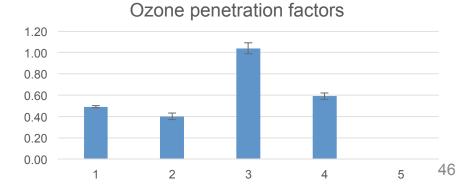
- Estimates of ozone penetration factors (mean ± SD) were 0.76±0.03
 - Ranging from 0.40±0.0 to 1.04±0.04

All homes were multi-family units



PM2.5 penetration factors





Summary of work to date

Modeling

- New residential building energy and IAQ modeling framework developed
- Still need to incorporate health outcomes analysis (e.g., DALYs, CCRs), develop future policy scenarios, and figure out how to handle future hourly outdoor pollutant data

Field measurements

- Tested 8 homes pre/post retrofit (6 SF + 2 MF) and 5 non-retrofit MF units
- No apparent strong correlations between changes in pollutant infiltration factors or penetration factors with envelope airtightness alone
 - Some suggestion of the impact of a combination of change in envelope airtightness (i.e., NL or ACH50) in addition to changes in meteorological and/or pollutant conditions during testing
- Original goal of testing 30 homes pre/post retrofit will be difficult to meet

Acknowledgments

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