CAE 464/517 HVAC Systems Design Spring 2023

March 21, 2023 Air distribution systems: Duct design

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ANNOUNCEMENTS

Announcements

- Assignment 4 is posted (due next week)
- Do not forget to work on Project Part 2

| IIT-BIM Collaborate • CAE 464_sp23 Group 5 |
|--|
| |
| Welcome to CAE 464_sp23 Group 5 |
| Mohammad Heidarinejad, Mohammad Heidarinejad added you as a project admin to CAE 464_sp23 Group 5. |
| If you can't access the project, <u>contact Mohammad Heidarinejad</u> , the project administrator who invited you to this project. |
| Go to your project |

Announcements

- Final project presentation:
 May 4, 8 am to 10 am
 Location: Hermann Hall
 - □ All students are are required to present

Announcements

• Do not forget to review the Q&A file:

| | SUMMARY - | + |
|---|------------------------------|---|
| | OUTLINE | |
| _ | CAE 464/517 Spring 2023 Q&As | |
| | Project Part 1 | |
| | Assignment 3 | |
| | Assignment 2 | |
| | Assignment 1 | |
| | Midterm Exam 1 | |
| | | |

CAE 464/517 Spring 2023 Q&As

Project Part 1

Question: After class when we spoke with you, you mentioned that the maximum amount of space types we should use is 4. We came up with: Corridor/Transition Operating/Patient Room Office Lounge/Recreation as per ASHRAE common space types for hospitals.

https://docs.google.com/document/d/1m6ezSI6Bi9wGQcjnaYj i AXY2kzRICPYWkKfayNp5WE/edit#heading=h.7xv0zdhfny5a

Ductwork in Practice

• Adding interesting and daily application of HVAC systems:

https://docs.google.com/presentation/d/15bvvZ0VVm9SgonCzZ5N07MBvI0Yd VRYaph6Z3evveJA/edit#slide=id.g1f2938fcdac_0_0



RECAP

• Pressure drop calculations (elbows and transitions)



Recap

$$p_{\nu,o} = \left(\frac{V_o}{4,005}\right)^2$$

| Duct velocity V _o (fpm) | Duct pressure p_{v} (in w.c.) |
|------------------------------------|---------------------------------|
| 4,000 | 1.00 |
| 3,000 | 0.56 |
| 2,000 | 0.25 |
| 1,000 | 0.06 |

Recap



• See Table 12 for the recommended maximum airflow velocities:

| | NC or RC Rating | Maximum Airflow Veloci fpm | | | | |
|-----------------------|---------------------------|-------------------------------|---------------|--|--|--|
| Duct Location | in Adjoining Occupancy | Rectangular Duct | Round Duct | | | |
| 1 | 2 | 3 | 4 | | | |
| In shaft or above | 45 | 3500 | 5000 | | | |
| solid drywall ceiling | 35 | 2500 | 3500 | | | |
| | 25 or less | 1500 | 2500 | | | |
| Above suspended | 45 | 2500 | 4500 | | | |
| acoustical ceiling | 35 | 1750 | 3000 | | | |
| | 25 or less | 1000 | 2000 | | | |
| Duct within occupied | 45 | 2000 | 3900 | | | |
| space | 35 | 1450 | 2600 | | | |
| | 25 or less | 950 | 1700 | | | |

 Table 12
 Recommended Maximum Airflow Velocities to Achieve

 Specified Acoustic Design Criteria*

Ductwork in Practice

• The air distribution includes various components:



Recap

- You can use other resources (e.g., Chapter 8 of the Price Industries Handbook)
- Older version of ASHRAE Handbook

• Some common fitting terminology are:

| Fitting Function | Geometry | Category | Sequential Number |
|------------------------------------|------------------------------|--------------------------------|----------------------|
| S: S upply | D: Round (D iameter) | 1. Entries | 1, 2, 3, |
| | | 2. Exits | |
| E: Exhaust / Return | R: R ectangular | 3. Elbows | |
| | | 4. Transitions | |
| C: C ommon (supply/ return) | F: F lat oval | 5. Junctions | |
| | | 6. Obstructions | |
| | | 7. Fan and system interactions | |
| | | 8. Duct-mounted equipment | |
| | | 9. Dampers | |
| | | 10. Hoods | |

DUCT DESIGN METHODS

- Codes & standards
- Airflow rates
- Single line ductwork
- Size ductwork
- Calculate pressure drop
- Establish system total pressure

- There are different duct design methods:
 - Equal friction: Size based on chosen friction loss rate (per 100 ft) for each duct section to balance the pressure gradient (commonly used)
 - Equal velocity: Size based on maintaining a constant velocity for duct sections (applicable for simple or industrial systems to carry particles out)
 - Balanced capacity: Equal pressure drops from fan to outlets of each branch (e.g., VAV systems)
 - Static regain: Duct size at the fan is selected using the friction chart to get the starting velocity. Other main ducts are sized to achieve static regain from section to section, meaning keep static pressure same throughout a system

• The velocity classifications are important:

| Method | Velocity | Velocity Range | Pressure Drop | | |
|-------------------|---------------|--------------------------------|---|--|--|
| Equal friction | | Less than 0.1 | | | |
| Equal velocity | | in./100 ft | | | |
| | Low Velocity | Less than 2500 tpm (13 m/s) | (1 Pa/m) | | |
| Balanced capacity | | | [0.1 in./100 ft is a common value] | | |
| Static regain | High Velocity | Up to 4500 fpm (23 m/s) | Less than 0.7 in./100 ft (4.7 Pa/m) | | |

• When do we use high velocity design?

When the heating or cooling loads are large (e.g., commercial buildings)

Special considerations are required (e.g., balancing and leakage control)

• When do we use low velocity design?

When the low flow rate is adequate, and it is possible to to run large ductwork

□ Can achieve low fan energy use

EQUAL FRICTION METHOD

- The design friction rate per unit length (in. w.c per 100 ft) is maintained
- The aim is to design a well-balanced system
- If the layout is symmetrical and all runs from fan to diffuser approximately the same length this method works well

- However, in most duct systems, there are variety of duct runs from long to short.
- Thus, short runs need to use balancing dampers in order to balance the flow rate to each space, which can cause considerable noise

- The design friction rate depends upon the velocity allowable in the system
- Start from usually know flow rates adjacent to the fan to establish the lost pressure per unit of length
- After sizing the designer need to compute the total pressure loss of the longest run with the consideration of all fittings

• Example:

- □ Loss for each outlet is 0.05 in. w.c.
- □ Maximum velocity mains = 1,300 fpm, branches = 900 fpm
- □ Uniform pressure loss/100 ft and for elbows r/W = 1.0



• Solution:

□ Add labels for different branches and fittings



• Solution:

Estimate the equal friction method

 $Q_{main} = 500 \, cfm + 1500 \, cfm + 1000 \, cfm = 3000 \, cfm$ $V_{max} = 1300 \, fpm$



• Solution:

□ Construct a tabular air flow

| Section | Air Flow Rate (cfm) | Duct Size (in) | Duct (in Rectangular) | Velocity (fpm) |
|---------|------------------------|----------------|--------------------------|----------------|
| AB | 3,000 | | | |
| BC | 1,500 | | | |
| B1 | 1,500 | | | |
| C2 | 1,000 | | | |
| C3 | 500 | | | |

- Solution:
 - □ Find round diameters and velocities



• Solution:

□ Add the duct sizes and velocity rates

| Section | Air Flow Rate (cfm) | Duct Size (in) | Duct (in Rectangular) | Area (ft ²) | Velocity (fpm) |
|---------|------------------------|-------------------|--------------------------|-------------------------|-------------------|
| AB | 3,000 | 21 | | | 1,059 |
| BC | 1,500 | 16 | | | 1,000 |
| B1 | 1,500 | 16 | | | 1,000 |
| C2 | 1,000 | 14.5 | | | 750 |
| C3 | 500 | 11 | | | 600 |

• Solution:

□ Find square duct sizes

| | | | | | | | | • | | | | | | | | | | | | |
|-----------|----|----|----|----|----|----|-----|---------|--------|----------|---------|---------|----------|--------|----|----|----|----|----|----|
| Circular | | | | | | | Le | ngth of | One S | ide of F | Rectang | ular D | uct (a) | in. | | | | | | |
| Duct | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 |
| Diameter, | | | | | | | Len | gth Ad | iacent | Side of | Rectan | gular I | Duct (b |). in. | | | | | | |
| <u> </u> | | | | | | | | 8 | , | | | 8 | | ,, | | | | | | |
| 5 | 5 | | | | | | | | | | | | | | | | | | | |
| 5.5 | 6 | 5 | | | | | | | | | | | | | | | | | | |
| 6 | 8 | 6 | | | | | | | | | | | | | | | | | | |
| 6.5 | 9 | 7 | 6 | | | | | | | | | | | | | | | | | |
| 7 | 11 | 8 | 7 | | | | | | | | | | | | | | | | | |
| 7.5 | 13 | 10 | 8 | 7 | | | | | | | | | | | | | | | | |
| 8 | 15 | 11 | 9 | 8 | | | | | | | | | | | | | | | | |
| 8.5 | 17 | 13 | 10 | 9 | | | | | | | | | | | | | | | | |
| 9 | 20 | 15 | 12 | 10 | 8 | | | | | | | | | | | | | | | |
| 9.5 | 22 | 17 | 13 | 11 | 9 | | | | | | | | | | | | | | | |
| 10 | 25 | 19 | 15 | 12 | 10 | 9 | | | | | | | | | | | | | | |
| 10.5 | 29 | 21 | 16 | 14 | 12 | 10 | | | | | | | | | | | | | | |
| 11 | 32 | 23 | 18 | 15 | 13 | 11 | 10 | | | | → (| 2-3 | | | | | | | | |
| 11.5 | | 26 | 20 | 17 | 14 | 12 | 11 | | | | | | | | | | | | | |
| 12 | | 29 | 22 | 18 | 15 | 13 | 12 | | | | | | | | | | | | | |
| 12.5 | | 32 | 24 | 20 | 17 | 15 | 13 | | | | | | | | | | | | | |
| 13 | | 35 | 27 | 22 | 18 | 16 | 14 | 12 | | | | | | | | | | | | |
| 13.5 | | 38 | 29 | 24 | 20 | 17 | 15 | 13 | | | | | | | | | | | | |
| 14 | | | 32 | 26 | 22 | 19 | 17 | 14 | | | | | 0 | 0 | | | | | | |
| 14.5 | | | 35 | 28 | 24 | 20 | 18 | 15 | | | | | <u> </u> | 2 | | | | | | |
| 15 | | | 38 | 30 | 25 | 22 | 19 | 16 | 14 | | | | | | | | | | | |
| 16 | | | 45 | 36 | 30 | 25 | 22 | 18 | -15 | | | | B- | С | | | | | | |
| 17 | | | | 41 | 34 | 29 | 25 | 20 | 17 | 16 | | | _ | - | | | | | | |
| 18 | | | | 47 | 39 | 33 | 29 | 23 | 19 | 17 | | | | | | | | | | |
| 19 | | | | 54 | 44 | 38 | 33 | 26 | 22 | 19 | 18 | | | | | | | | | |
| 20 | | | | | 50 | 43 | 37 | 29 | 24 | 21 | 19 | | | | _ | | | | | |
| 21 | | | | | 57 | 48 | 41 | 33 | 27 | 23 | 20 | | | ► A· | -В | | | | | |

• Solution:

□ Add the rectangular values to the table

| Section | Air Flow Rate (cfm) | Duct Size (in) | Duct (in Rectangular) | Area (ft ²) | Velocity (fpm) |
|---------|------------------------|-------------------|--------------------------|-------------------------|-------------------|
| AB | 3,000 | 21 | 34 / 12 | 2.83 | 1,059 |
| BC | 1,500 | 16 | 18 /12 | 1.50 | 1,000 |
| B1 | 1,500 | 16 | 18 / 12 | 1.50 | 1,000 |
| C2 | 1,000 | 14.5 | 16 / 12 | 1.33 | 750 |
| C3 | 500 | 11 | 10 / 12 | 0.83 | 600 |

Solution:

□ Add the calculated ductwork sizes to the diagram



• Solution:

Find the friction loss (in/100 ft) since we made slight changes to the duct cross sections

| Section | Air Flow Rate (cfm) | Duct (in Rectangular) | D _e (in) | Friction Loss (in/100 ft) | Length (ft) | Section Loss (in. w.c.) |
|---------|------------------------|--------------------------|------------------------|------------------------------|----------------|----------------------------|
| AB | 3,000 | 34 / 12 | 21.4 | | 40 | 0.035 |
| BC | 1,500 | 18 /12 | 16 | | 30 | 0.03 |
| B1 | 1,500 | 18 / 12 | 16 | | 40 | 0.04 |
| C2 | 1,000 | 16 / 12 | 15.1 | | 50 | 0.033 |
| C3 | 500 | 10 / 12 | 12 | | 120 | 0.067 |

- Solution:
 - □ Friction losses (in/100 ft)



• Solution:

□ Find the friction losses (in/100 ft)

| Section | Air Flow Rate (cfm) | Duct (in Rectangular) | D _e (in) | Friction Loss (in/100 ft) | Length (ft) | Section Loss (in. w.c.) |
|---------|---------------------------|--------------------------|------------------------|---------------------------------|----------------|---|
| AB | 3,000 | 34 / 12 | 21.4 | 0.088 | 40 | $0.088 \times \left(\frac{40}{100}\right) = 0.035$ |
| BC | 1,500 | 18 /12 | 16 | 0.1 | 30 | $0.1 \times \left(\frac{30}{100}\right) = 0.03$ |
| B1 | 1,500 | 18 / 12 | 16 | 0.1 | 40 | $0.1 \times \left(\frac{40}{100}\right) = 0.04$ |
| C2 | 1,000 | 16 / 12 | 15.1 | 0.065 | 50 | $0.065 \times \left(\frac{50}{100}\right) = 0.0325$ |
| C3 | 500 | 10 / 12 | 12 | 0.056 | 120 | $0.056 \times \left(\frac{120}{100}\right) = 0.067$ |

• Solution:

□ Select fittings

| | | A 34"x12 | 2" B | 18"x12" |
|--|-------------------------|----------|----------|----------------------|
| | Plonum | 40 ft | F1 | 30 ft |
| l | Fiellulli | F6 | | Balancing |
| | | | 40 fi | ^t 18"x12" |
| | | F7 | Ļ. | |
| | | | ţ | |
| | | | 1500 cfm | |
| | $W_s \times H_s $ A_s | - | 1 | |
| H× % | | | | |
| L = 0.25 W _b , 75 mm min. $Q_b A_b$ | | | | |

SR5-13 Tee, 45 Degree Entry Branch, Diverging

| | C _b Values | | | | | | | | | | | | | |
|-----------|-----------------------------|-------|------|------|-----------|------|------|---------|------|--|--|--|--|--|
| | | | | | Q_b/Q_c | | | | | | | | | |
| A_b/A_c | _c 0.1 0.2 0.3 0. | | | | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | | | | | |
| 0.1 | 0.73 | 0.34 | 0.32 | 0.34 | 0.35 | 0.37 | 0.38 | 0.39 | 0.40 | | | | | |
| 0.2 | 3.10 | 0.73 | 0.41 | 0.34 | 0.32 | 0.32 | 0.33 | 0.34 | 0.35 | | | | | |
| 0.3 | 7.59 | 1.65 | 0.73 | 0.47 | 0.37 | 0.34 | 0.32 | 0.32 | 0.32 | | | | | |
| 0.4 | 14.20 | 3.10 | 1.28 | 0.73 | 0.51 | 0.41 | 0.36 | 0.34 | 0.32 | | | | | |
| 0.5 | 22.92 | 5.08 | 2.07 | 1.12 | 0.73 | 0.54 | 0.44 | 0.38 | 0.35 | | | | | |
| 0.6 | 33.76 | 7.59 | 3.10 | 1.65 | 1.03 | 0.73 | 0.56 | 0.47 | 0.41 | | | | | |
| 0.7 | 46.71 | 10.63 | 4.36 | 2.31 | 1.42 | 0.98 | 0.73 | 0.58 | 0.49 | | | | | |
| 0.8 | 61.79 | 14.20 | 5.86 | 3.10 | 1.90 | 1.28 | 0.94 | 0.73 | 0.60 | | | | | |
| 0.9 | 78.98 | 18.29 | 7.59 | 4.02 | 2.46 | 1.65 | 1.19 | 0.91 | 0.73 | | | | | |
| | C _s Values | | | | | | | | | | | | | |
| | | | | | Q_s/Q_c | | | | | | | | | |
| A_s/A_c | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 0.9 | | | | | | |
| 0.1 | 0.04 | | | | | | | | | | | | | |
| 0.2 | 0.98 | 0.04 | | | | | | | | | | | | |
| 0.3 | 3.48 | 0.31 | 0.04 | | | | | | | | | | | |
| 0.4 | 7.55 | 0.98 | 0.18 | 0.04 | | | | | | | | | | |
| 0.5 | 13.18 | 2.03 | 0.49 | 0.13 | 0.04 | | | | | | | | | |
| 0.6 | 20.38 | 3.48 | 0.98 | 0.31 | 0.10 | 0.04 | | | | | | | | |
| 0.7 | 29.15 | 5.32 | 1.64 | 0.60 | 0.23 | 0.09 | 0.04 | | | | | | | |
| 0.8 | 39.48 | 7.55 | 2.47 | 0.98 | 0.42 | 0.18 | 0.08 | 0.04 | | | | | | |
| 0.9 | 51.37 | 10.17 | 3.48 | 1.46 | 0.67 | 0.31 | 0.15 | 0.07 | 0.04 | | | | | |



• **Solution:** Compute fittings

| Section | Fitting No | Fitting Type | ASHRAE Fitting No. | Parameters | Loss Coefficient | Velocity (fpm) | P _∨ (in. w.c.) | P _t (in. w.c.) |
|---------|-----------------|-----------------|--------------------------|---|---------------------|-------------------|------------------------------|------------------------------|
| AB | F1 _b | Tee Branch | SR5-13 | $\frac{A_b}{A_c} = \frac{1.5}{2.83} = 0.53 \frac{Q_b}{Q_c} = \frac{1500}{3000} = 0.5$ | 0.82 | 1,000 | 0.062 | 0.051 |
| | F1 _s | Tee Straight | SR5-13 | $\frac{A_b}{A_c} = \frac{1.5}{2.83} = 0.53 \frac{Q_b}{Q_c} = \frac{1500}{3000} = 0.5$ | 0.06 | 1,000 | 0.062 | 0.004 |
| BC | F2 | Tee Branch | SR5-13 | $\frac{A_b}{A_c} = \frac{1.33}{1.50} = 0.9 \frac{Q_b}{Q_c} = \frac{1000}{1500} = 0.67$ | 1.33 | 752 | 0.035 | 0.047 |
| | F2 | Tee Straight | SR5-13 | $\frac{A_b}{A_c} = \frac{0.83}{1.5} = 0.55 \frac{Q_b}{Q_c} = \frac{500}{1500} = 0.3$ | 0.58 | 602 | 0.023 | 0.013 |
| B1 | F3 | Damper | CR9-1 | $q = 0^0$ | 0.19 | 600 | 0.022 | 0.004 |
| | F4 | Elbow | CR3-1 | $\frac{r}{W} = 1 \frac{H}{W} = 1.2$ | 0.20 | 600 | 0.022 | 0.004 |
| | F5 | Outlet | | | | | | 0.050 |
| C2 | F7 | Damper | CR9-1 | $q = 0^0$ | 0.19 | 1,000 | 0.062 | 0.012 |
| | F8 | Outlet | | | | | | 0.050 |
| C3 | F6 | Damper | CR9-1 | $q = 0^0$ | 0.19 | 750 | 0.035 | 0.007 |
| | F9 | Outlet | | | | | | 0.050 |

• **Solution:** Pressure loss summary for different paths

| Path | Note | Duct | Тее | Duct | Тее | Damper | Duct | Outlet | Total | Differe ntial |
|----------|----------------------|-------|-------|------|-------|--------|-------|--------|-------|------------------|
| ABC | Path/Fitting Duct | AB | F1S | BC | F2S | F3 | C3 | Value | | Path ∆P |
| 3 | | 0.035 | 0.004 | 0.03 | 0.013 | 0.004 | 0.067 | 0.05 | 0.204 | 0.000 |
| ABC 2 | Path/Fitting Duct | AB | F1 | BC | F2 | F6 | C2 | Value | | Path ΔP |
| | | 0.035 | 0.004 | 0.03 | 0.013 | 0.007 | 0.033 | 0.05 | 0.171 | 0.032 |
| AB1 | Path/Fitting | AB | F1 | | | F7 | B1 | Value | | Path ∆P |
| | Duct | 0.035 | 0.051 | | | 0.012 | 0.04 | 0.05 | 0.188 | 0.015 |

ΔP (in. w.c.)

• Solution (summary):



Another example is presented in this reference:

8.2 Duct Design Fundamentals



Example 8.3 - Duct Sizing

IP

As shown below, a schematic duct layout has been prepared for a building HVAC system that shows dampers, air volumes, duct length, and other information needed to properly size the duct. Note that all supply and return locations are numbered. A friction loss of 0.1 in. w.c./100 ft will be used for the sizing calculations. The total required discharge static pressure needed to supply the duct layout will be estimated.

The ductwork will be rectangular, but is sized as round and then converted to the rectangular format.



 See Chapter 21 – Page 21.24 of the Fundamentals for another example:

Example 8. For the VAV system shown in Figure 26, design the duct system by both the equal friction (EF) and static regain (SR) methods, and compare the section duct sizes, total pressure required for each path, and the unbalance between paths.

The system is located in Denver (5430 ft elevation) and the duct is spiral round, galvanized steel (absolute roughness $\varepsilon = 0.0004$ ft). The duct system is located above a suspended acoustical ceiling, and the allowable background sound in the occupied spaces is NC-35. Terminals T1, T2, T3, and T4 (VAV boxes with a one-row hot-water coil) are 800 cfm. VAV box loss coefficients are 1.68.

BALANCED CAPACITY METHOD

- The balanced design method uses the duct network
 principle
- For all network problems, it satisfies the continuity and the work-energy principles throughout the network

 Based on the continuity equation, the summation of air flow rate into any junction is zero

$$\Sigma \pm Q = 0$$

 Based on the network-energy equation, the total pressure loss around any single loop of the network is zero

$$\Sigma \pm P = 0$$

• Satisfy all the possible pressure drops



 $P_{total} = \Delta p_1 + \Delta p_3 + \Delta p_4 + \Delta p_9 + \Delta p_7 + \Delta p_5$ $P_{total} = \Delta p_1 + \Delta p_3 + \Delta p_4 + \Delta p_9 + \Delta p_7 + \Delta p_6$ $P_{total} = \Delta p_1 + \Delta p_3 + \Delta p_4 + \Delta p_9 + \Delta p_8$ $P_{total} = \Delta p_2 + \Delta p_4 + \Delta p_9 + \Delta p_7 + \Delta p_5$ $P_{total} = \Delta p_2 + \Delta p_4 + \Delta p_9 + \Delta p_7 + \Delta p_6$ $P_{total} = \Delta p_2 + \Delta p_4 + \Delta p_9 + \Delta p_7$

Satisfy all the possible pressure drops



SYSTEM CHARACTERISTICS CURVE

• There are a couple of components required for the design of an air distribution



• Overall system resistance can be written as:

$$\Delta P_{total} = \sum \Delta P_{Ductwork} + \sum \Delta P_{fittings} =$$

$$= \sum f \frac{L}{D} \left(\frac{\rho V^2}{2g_c} \right) + \sum K \left(\frac{\rho V^2}{2g_c} \right)$$

• Overall system resistance can be written as:

$$\Delta P_{total} = (Constant) \times \dot{Q}^2$$

 Flow through any resistance (i.e., duct and fittings) is proportional to the square root of the pressure causing the flow



This relationship defines the flow versus pressure characteristics of a system



Airflow Rate (cfm)

This relationship defines the flow versus pressure characteristics of a system



 The best operating point varies based on the resistance in the system (i.e., system curves)



FAN PERFORMANCE CURVE

Fan Performance Curve



https://content.greenheck.com/public/DAMProd/Original/10002/CentrifugalDWPerfSuppl_catalog.pdf

•

% WOV = (CFM X 100) / (RPM X 2.08)

Fan Performance Curve

• An example of a fan curve:

24 BIDW

Wheel Diameter = 241/2 in.

Outlet Area = 6.21 ft.²

Tip Speed = 6.41 x RPM

Maximum BHP = (RPM/599)³

Minimum Starting HP = 1

Maximum RPM Class I = 1568

Maximum RPM Class II = 2045

Maximum RPM Class III = 2577

| | | | | | | | | | STA | TIC F | RES | SURE | E (in. | wg) | | | | | | | |
|-------|------|------|------|------|------|------|------|------|------|-------|------|------|--------|------|------|------|------|------|------|------|------|
| CFM | ov | 0.25 | | 0.50 | | 0.75 | | 1.00 | | 1.25 | | 1.50 | | 1.75 | | 2.00 | | 2.25 | | 2.50 | |
| | | RPM | BHP | RPM | BHP | RPM | BHP | RPM | BHP | RPM | BHP | RPM | BHP | RPM | BHP | RPM | BHP | RPM | BHP | RPM | BHP |
| 5000 | 805 | 416 | 0.34 | 504 | 0.58 | 585 | 0.85 | 656 | 1.14 | | | | | | | | | | | | |
| 6000 | 966 | 462 | 0.46 | 542 | 0.74 | 613 | 1.04 | 681 | 1.36 | 744 | 1.71 | 801 | 2.06 | | | | | | | | |
| 7000 | 1127 | 512 | 0.62 | 586 | 0.94 | 650 | 1.26 | 711 | 1.62 | 769 | 1.99 | 826 | 2.39 | 878 | 2.79 | 927 | 3.20 | 972 | 3.63 | | |
| 8000 | 1288 | 564 | 0.82 | 632 | 1.17 | 692 | 1.54 | 748 | 1.92 | 801 | 2.32 | 851 | 2.74 | 903 | 3.18 | 951 | 3.64 | 997 | 4.10 | 1040 | 4.57 |
| 9000 | 1449 | 619 | 1.07 | 679 | 1.46 | 737 | 1.87 | 789 | 2.28 | 838 | 2.70 | 886 | 3.16 | 931 | 3.62 | 977 | 4.11 | 1022 | 4.61 | 1065 | 5.11 |
| 10000 | 1610 | 675 | 1.36 | 730 | 1.79 | 783 | 2.23 | 833 | 2.70 | 879 | 3.15 | 923 | 3.62 | 968 | 4.12 | 1009 | 4.63 | 1049 | 5.16 | 1090 | 5.70 |
| 11000 | 1771 | 731 | 1.72 | 782 | 2.19 | 831 | 2.66 | 879 | 3.16 | 924 | 3.68 | 965 | 4.17 | 1005 | 4.68 | 1046 | 5.23 | 1085 | 5.78 | 1122 | 6.35 |
| 12000 | 1932 | 789 | 2.14 | 836 | 2.64 | 882 | 3.16 | 925 | 3.69 | 969 | 4.24 | 1009 | 4.80 | 1048 | 5.34 | 1084 | 5.88 | 1122 | 6.47 | 1159 | 7.08 |
| 13000 | 2093 | 848 | 2.63 | 891 | 3.17 | 933 | 3.73 | 975 | 4.29 | 1015 | 4.87 | 1055 | 5.47 | 1092 | 6.08 | 1128 | 6.66 | 1162 | 7.25 | 1196 | 7.86 |
| 14000 | 2254 | 907 | 3.20 | 947 | 3.76 | 986 | 4.37 | 1025 | 4.97 | 1063 | 5.58 | 1101 | 6.21 | 1137 | 6.86 | 1172 | 7.51 | 1205 | 8.14 | 1237 | 8.78 |
| 15000 | 2415 | 967 | 3.85 | 1003 | 4.44 | 1040 | 5.08 | 1077 | 5.73 | 1113 | 6.37 | 1148 | 7.03 | 1183 | 7.71 | 1217 | 8.41 | 1250 | 9.11 | 1281 | 9.79 |
| 16000 | 2576 | 1027 | 4.58 | 1060 | 5.21 | 1095 | 5.88 | 1129 | 6.57 | 1164 | 7.26 | 1198 | 7.95 | 1230 | 8.66 | 1264 | 9.39 | 1295 | 10.1 | 1326 | 10.9 |
| 17000 | 2737 | 1087 | 5.41 | 1118 | 6.07 | 1151 | 6.78 | 1184 | 7.50 | 1216 | 8.24 | 1248 | 8.97 | 1280 | 9.71 | 1310 | 10.5 | 1342 | 11.2 | 1372 | 12.0 |
| 18000 | 2898 | 1147 | 6.34 | 1177 | 7.04 | 1207 | 7.77 | 1239 | 8.53 | 1269 | 9.31 | 1300 | 10.1 | 1330 | 10.9 | 1359 | 11.6 | 1388 | 12.4 | 1418 | 13.3 |
| 19000 | 3059 | 1208 | 7.38 | 1236 | 8.11 | 1264 | 8.86 | 1294 | 9.67 | 1323 | 10.5 | 1352 | 11.3 | 1381 | 12.1 | 1410 | 12.9 | 1437 | 13.8 | 1465 | 14.6 |
| 20000 | 3220 | 1269 | 8.52 | 1295 | 9.29 | 1321 | 10.1 | 1350 | 10.9 | 1378 | 11.8 | 1405 | 12.6 | 1433 | 13.5 | 1460 | 14.3 | 1487 | 15.2 | 1513 | 16.1 |