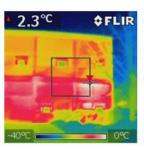
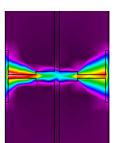
CAE 331/513 **Building Science** Fall 2015







Week 13: November 17, 2015

Cooling load calculations Exam 2 review

Built Environment Research







Advancing energy, environmental, and sustainability research within the built environment

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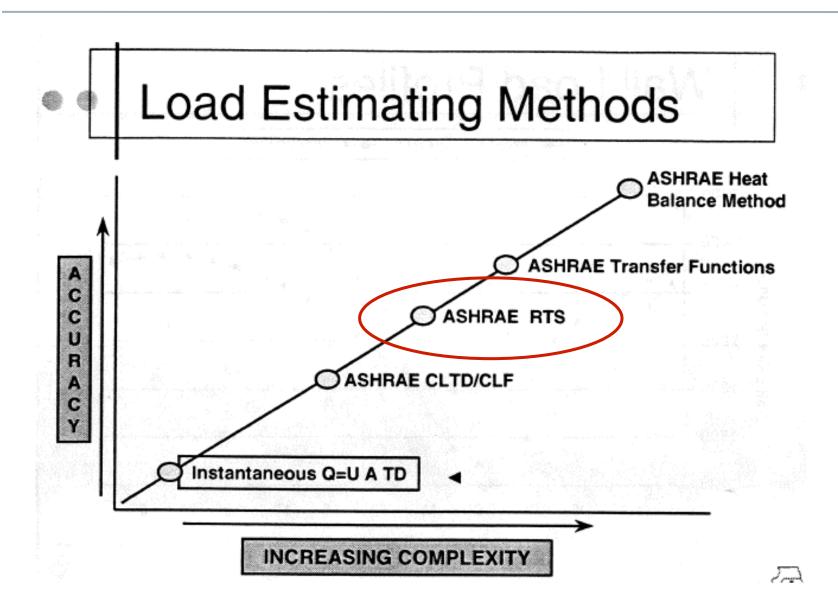
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Last time

- Introduced cooling load calculations
 - Two methods covered so far:
 - Heat balance method (HBM)
 - Cooling load temperature difference (CLTD) / cooling load factor (CLF)
- Today:
 - HW 5 due what heating load did you come up with?
 - One last cooling load calculation method
 - Radiant Time Series (RTS)
 - Introduce Trane Trace 700 for performing load calculations
 - Assign HW 6 (due Thursday December 3)
 - Review for Exam 2 on Thursday Nov 19 in class

Cooling load calculation methods



Radiant time-series method (RTS)

- The Radiant Time-Series method (RTS) is a simplified version of the more complete heat balance method that can be implemented in a spreadsheet or similar software
- RTS accounts for dynamic elements like outdoor air temperatures, solar radiation, and enclosure heat transfer
 - Outdoor air temperatures and solar radiation are cyclic with 24 hour peak day periods
 - Enclosure heat capacity will absorb and release heat with a time delay
 - This is accounted for with "response factors" for typical construction elements

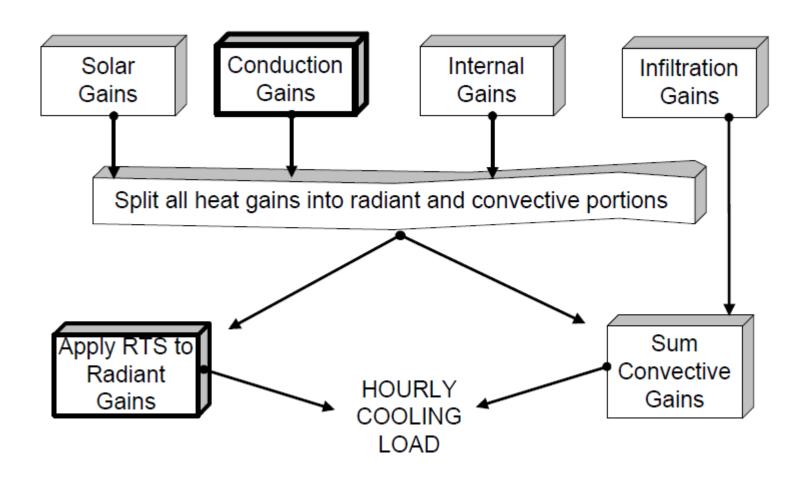
RTS simplifying assumptions

- The combined effects of convective and radiative heat transfer to/from exterior can be modeled by convection to/ from an equivalent exterior air temperature called the sol-air temp, $T_{sol-air}$
 - This means a single combined radiation-convection heat transfer coefficient independent of wind speed, surface temps and sky temps, must be used for all surfaces
- All interior surface temperatures are assumed to be nearly the same, so all radiation between elements in the interior can be ignored
 - Makes calculations much simpler

RTS main idea

The idea behind the radiant time series is this:

- The current heat transfer to/from the interior is equal to:
 - + Part of the current convective heat transfer from the outside of the enclosure
 - + Current solar heat gain through fenestration
 - + Part of the earlier convective and radiative heat transfer from the outside of the enclosure



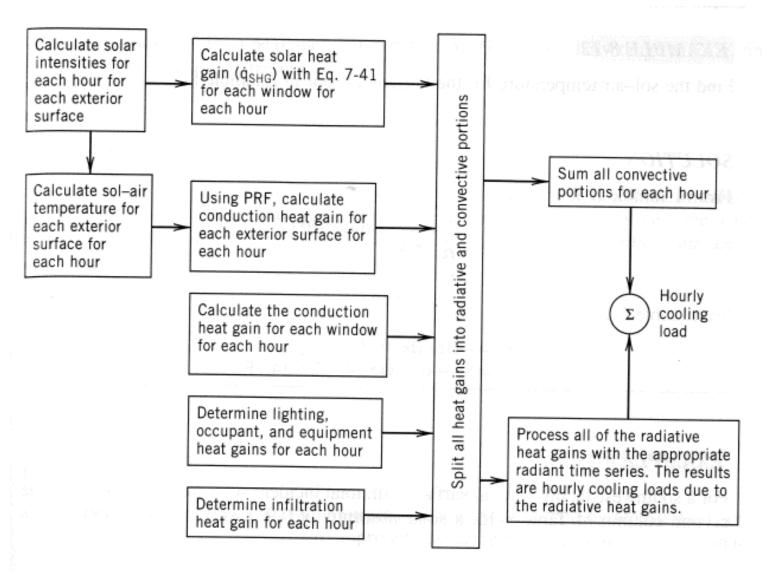


Figure 8-8 Radiant time series method.

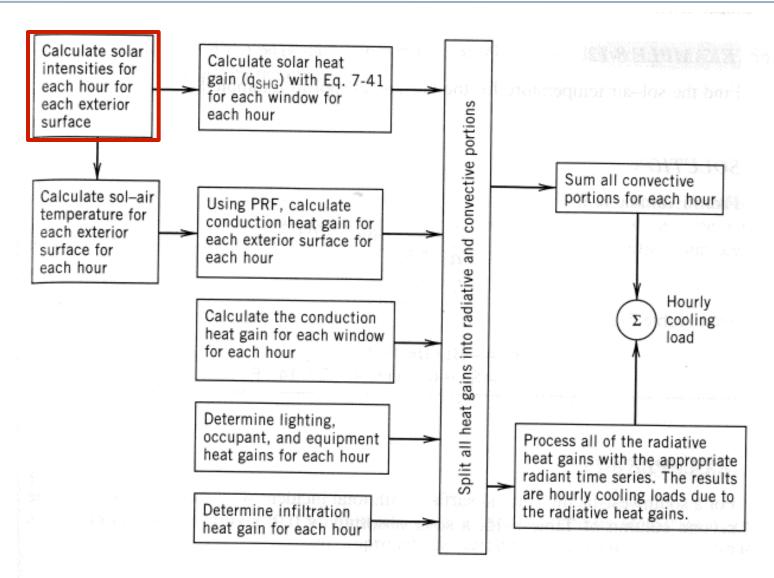
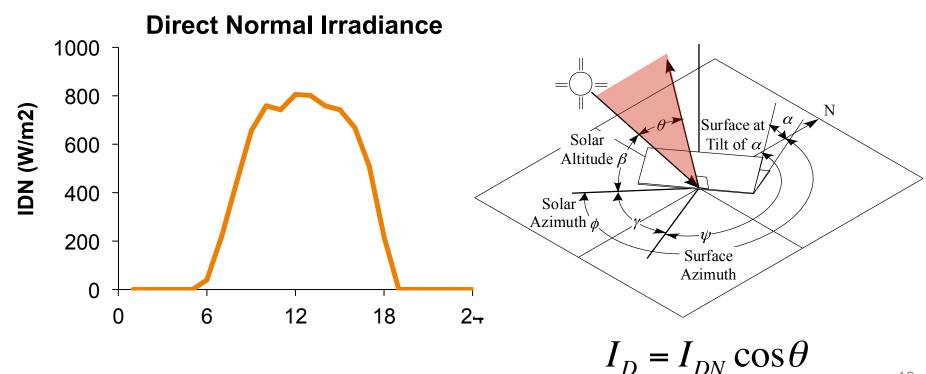


Figure 8-8 Radiant time series method.

Solar intensities

- We can calculate hourly solar intensities based on solar geometry
 - Or download data from the internet
 - http://rredc.nrel.gov/solar/old_data/nsrdb/



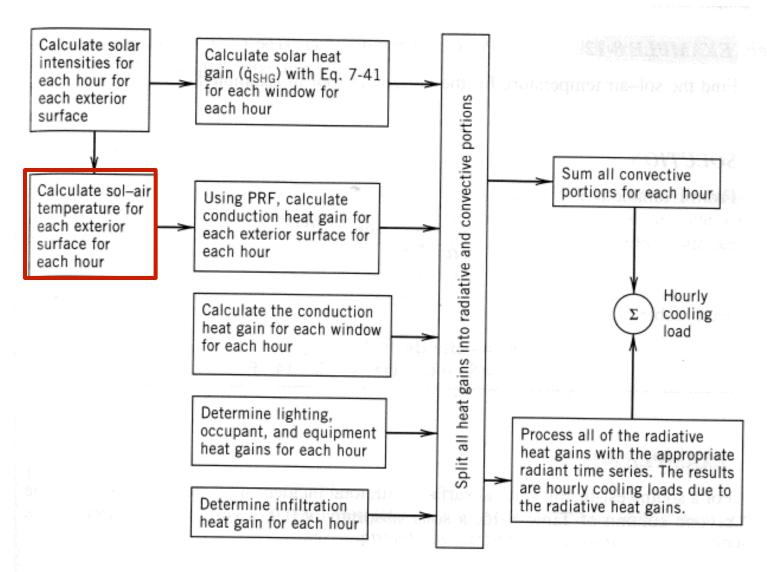


Figure 8-8 Radiant time series method.

Calculate sol-air temperature

For each surface, for each hour

$$T_{sol-air} = T_{air,out} + \alpha \frac{I_{solar}}{h_{ext,conv+rad}} - \varepsilon \frac{\delta R}{h_{ext,conv+rad}}$$

 $\varepsilon \delta R \approx 7^{\circ}$ F for horizontal surfaces

 $\varepsilon \delta R \approx 0^{\circ} F$ for vertical surfaces

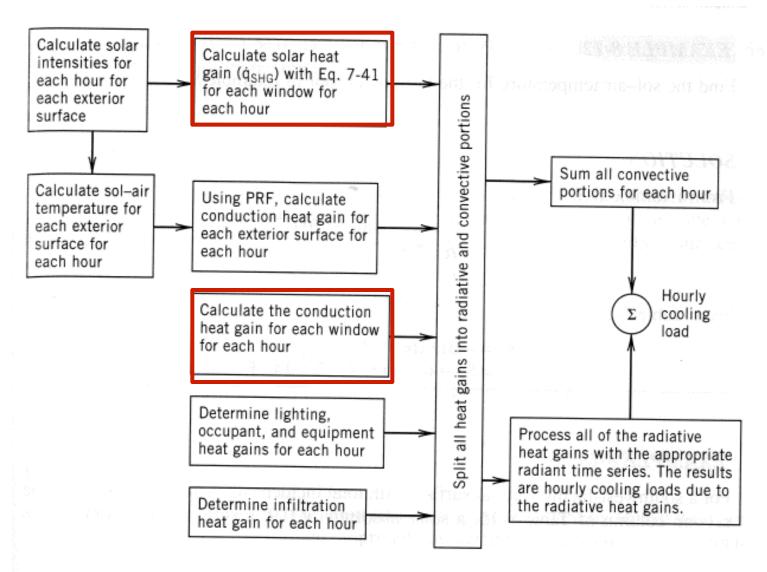


Figure 8-8 Radiant time series method.

Heat gain through windows

For each window, for each hour of the peak day

$$q_{window} = U_{pf} (T_{out} - T_{in}) + I_{solar} SHGC(IAC)$$

We've done this before

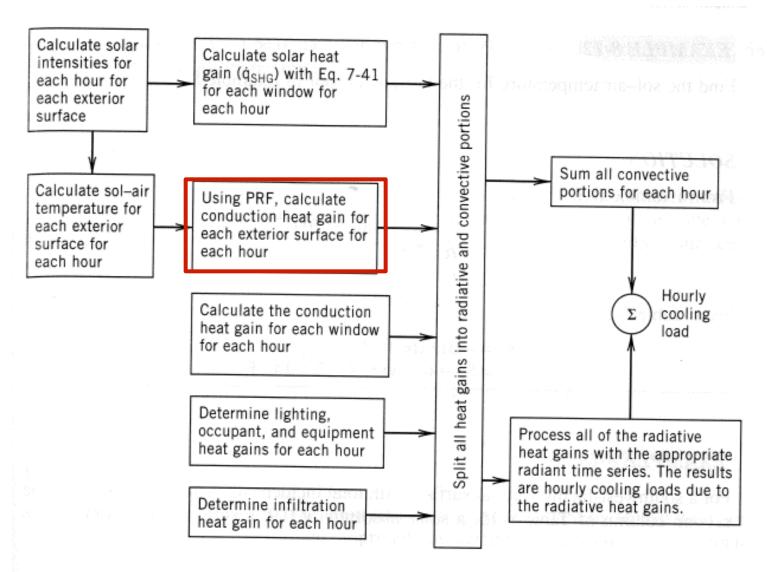


Figure 8-8 Radiant time series method.

Conduction heat gains and "PRF"

- Heat gains to the interior from conduction will be a sum of conduction going on right now + part of the heat transferred to the enclosure from earlier times
- For example:

$$q(n) = C_0 U(T_e(n) - T_i(n)) + C_1 U(T_e(n-1) - T_i(n-1)) + \dots + C_{23} U(T_e(n-23) - T_i(n-23))$$
where $T_e = T_{sol-air}$

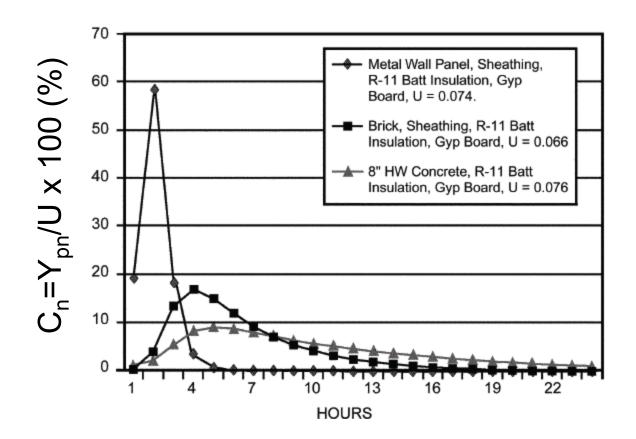
- We call C_n the conduction time series
- $Y_{pn} = C_n U$ is the periodic response factor (PRF) in [W/m²K]
- U is just the U-value of the element in [W/m²K]

Finding Y_{pn} and C_n

- C_n and Y_{pn} depend on the exact details of the enclosure construction (wall or ceiling)
 - Overall insulation, mass, heat capacity and the insulation location both are important
- The ASHRAE handbook has a table of U-values and C_n values for 20 common constructions
 - For the RTS method, you are pretty much limited to these enclosure constructions

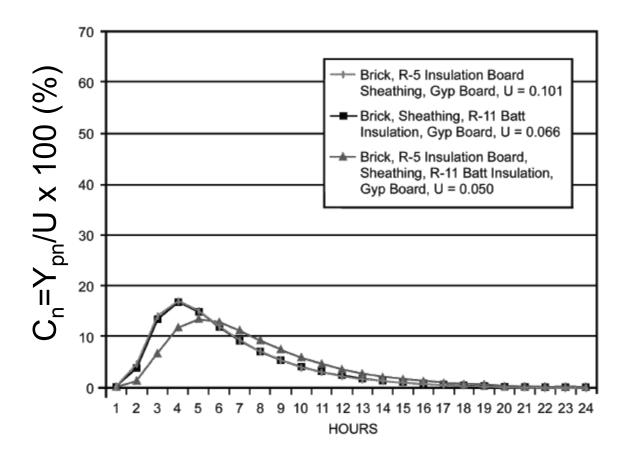
C_n for varying masses of enclosures

Increasing mass (heat capacity) increases the delay in heat transmission



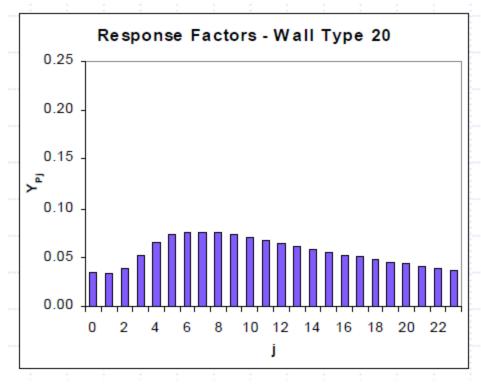
C_n for varying insulation

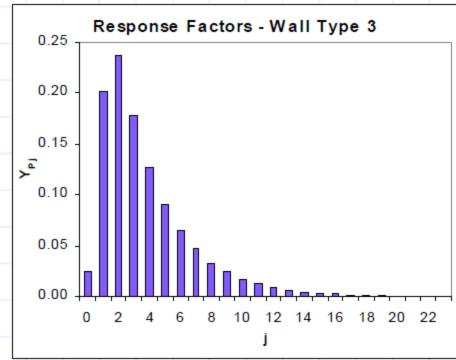
Interior and exterior insulation have smaller effects on this brick wall



Y_{pn} for two different walls

- Type 20: Brick + 8" concrete + R11 insulation + gypsum board
- Type 3: 1" stone + R10 insulation + gypsum board





Conduction heat gains and "PRF"

• Once we have Y_{pn} we can estimate the heat conduction into the room at the current time as:

$$q_{conduction,in,t} = \sum_{n=0}^{23} Y_{pn} \left(T_{e,q-n} - T_{rc} \right) \left[\text{Btu/(h·ft}^2) \text{ or W/m}^2 \right]$$

where

 $T_{e,q-n}$ =the sol-air temp n hours ago

 T_{rc} = constant interior room temp

 Y_{pn} = periodic response function

Conduction heat gains and "PRF": Expanded

- To use the previous equation we need to know the sol-air temp for the previous 24 hours
- The calculation for 8 am would look like this:

$$\begin{split} q_{conduction,in,8am} &= Y_{p0} \left(T_{e,8am} - T_{rc} \right) + Y_{p1} \left(T_{e,7am} - T_{rc} \right) + Y_{p2} \left(T_{e,6am} - T_{rc} \right) + \\ Y_{p3} \left(T_{e,5am} - T_{rc} \right) + Y_{p4} \left(T_{e,4am} - T_{rc} \right) + Y_{p5} \left(T_{e,3am} - T_{rc} \right) + \cdots \\ &+ Y_{p22} \left(T_{e,11am} - T_{rc} \right) + Y_{p23} \left(T_{e,10am} - T_{rc} \right) + Y_{p24} \left(T_{e,9am} - T_{rc} \right) \end{split}$$

The underlined times are from the day before

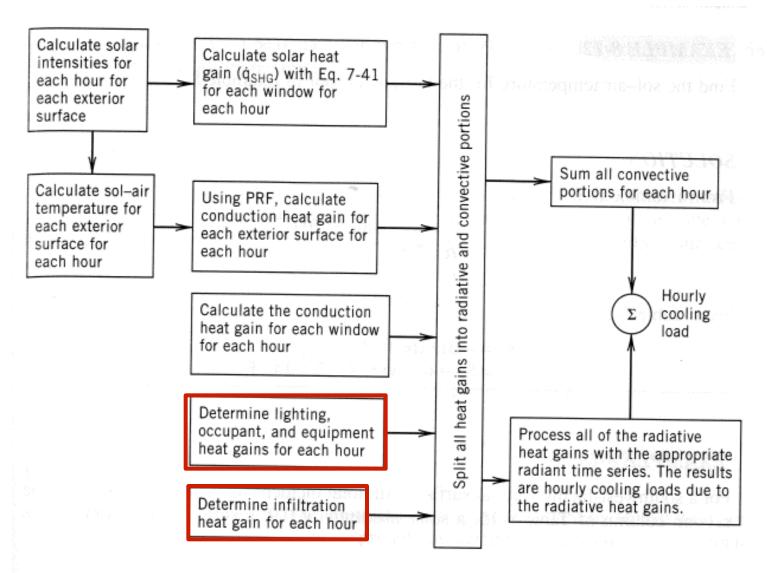


Figure 8-8 Radiant time series method.

Infiltration and internal gains

- We treat infiltration/ventilation gains as instantaneous gains
 - We've already done this
 - We calculate these separately for each hour of the day because the exterior air temperature changes each hour
- We calculate internal gains using methods discussed earlier
 - We calculate these for each hour too because the internal loads will change from hour to hour (need to know schedules)
 - Also need to keep track of the radiative + convective parts

Splitting gains into radiative and convective portions

- At each hour, each heat gain must be split into radiative parts + convective parts
 - "Delayed" versus "instantaneous"

Table 14 Recommended Radiative/Convective Splits f

Heat Gain Type	Recommended Radiative Fraction	Recommended Convective Fraction		
Occupants, typical office conditions	0.6	0.4		
Equipment	0.1 to 0.8	0.9 to 0.2		
Office, with fan	0.10	0.9		
Without fan	0.3	0.7		
Lighting				
Conduction heat gain				
Through walls and floors	0.46	0.54		
Through roof	0.60	0.40		
Through windows	0.33 (SHGC > 0.5) 0.46 (SHGC < 0.5)	0.67 (SHGC > 0.5) 0.54 (SHGC < 0.5)		
Solar heat gain through fenestration				
Without interior shading	1.0	0.0		
With interior shading				
Infiltration	0.0	1.0		

Splitting gains into radiative and convective portions

- Convection is considered instantaneous
- We then estimate the cooling load due to the radiative portion of each heat gain by applying a radiant time series
 - This is analogous to the periodic response factors (PRF) for conduction based on current and past values of sol-air temperatures
- Radiant energy is absorbed + reradiated + absorbed + reradiated + absorbed + ...
 - We must add up portions of radiation from previous hours to find the total radiant contribution now (kind of like we did with conduction)

Total radiant contribution

$$Q_{cooling,t} = \sum_{n=0}^{23} r_n Q_{t-n\delta}$$
 [Btu/h] or [W]

where

 $Q_{cooling,t}$ = radiative cooling load at current hour, Btu/hr or W $Q_{t-n\delta}$ = radiative heat gain n hours ago, Btu/hr or W $r_n = n^{th}$ radiant time factor (RTF)

- RTF depends upon the wavelength (LW vs SW or solar), the mass of the enclosure, and the surface coverings
 - There is a different RTF for transmitted solar light than all the other radiated energy
 - ASHRAE has RTF tables for a number of different constructions with varying amounts of glass and carpet
 - Heavy construction with no carpet has the most contribution by older radiation

Example RTFs

Table 19 Representative Nonsolar RTS Values for Light to Heavy Construc

	Light			Medium				Heavy										
%	With Carpet			No Carpet			With Carpet			No Carpet			With Carpet			No Carpet		pet
Glass	10%	50%	90%	10%	50%	90%	10%	50%	90%	10%	50%	90%	10%	50%	90%	10%	50%	90%
Hour										I	Radia	nt Tim	e Fac	tor, %	,			
0	47	50	53	41	43	46	46	49	52	31	33	35	34	38	42	22	25	28
1	19	18	17	20	19	19	18	17	16	17	16	15	9	9	9	10	9	9
2	11	10	9	12	11	11	10	9	8	11	10	10	6	6	5	6	6	6
3	6	6	5	8	7	7	6	5	5	8	7	7	4	4	4	5	5	5
4	4	4	3	5	5	5	4	3	3	6	5	5	4	4	4	5	5	4
5	3	3	2	4	3	3	2	2	2	4	4	4	4	3	3	4	4	4
6	2	2	2	3	3	2	2	2	2	4	3	3	3	3	3	4	4	4
7	2	1	1	2	2	2	1	1	1	3	3	3	3	3	3	4	4	4
8	1	1	1	1	1	1	1	1	1	3	2	2	3	3	3	4	3	3
9	1	1	1	1	1	1	1	1	1	2	2	2	3	3	2	3	3	3
10	1	1	1	1	1	1	1	1	1	2	2	2	3	2	2	3	3	3

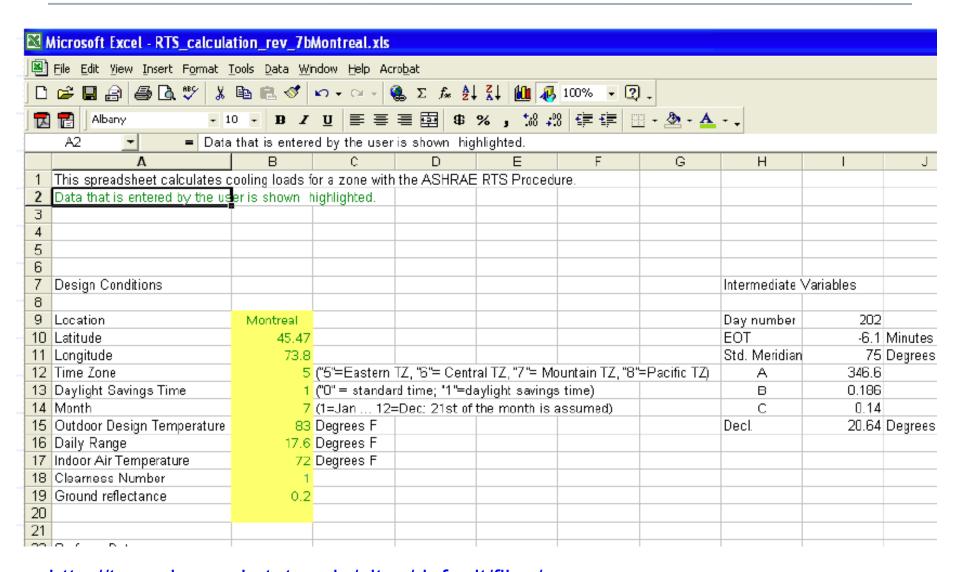
RTS example

- Outdoor conditions
 - Montreal
 - July 21
 - 83°F dry bulb
 - 17.6°F daily range
 - Ground reflectivity = 0.2
- Indoor conditions
 - Air temperature = 72°F
- Assume only S wall and roof are exposed to outside
 - Wall is 280 ft², α =0.9
 - Roof is 900 ft², α =0.9
 - Y_{pn} as shown in the next slides

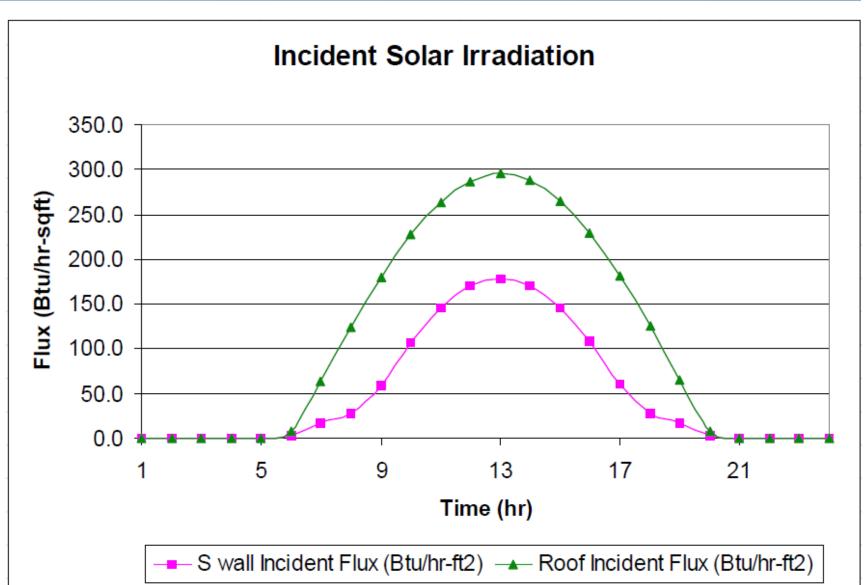
- Other heat gains
 - 10 occupants
 - 1 W/ft² equipment gain
 8AM to 5 PM
 - 0.2 W/ft² 5P-8A
 - 1.5 W/ft² lighting gain
 8AM to 5 PM
 - 0.3 W/ft² 5P-8A
 - Ignore infiltration

- 80 ft² of window on S wall
 - No shading
 - SHGC=0.76, U=0.55

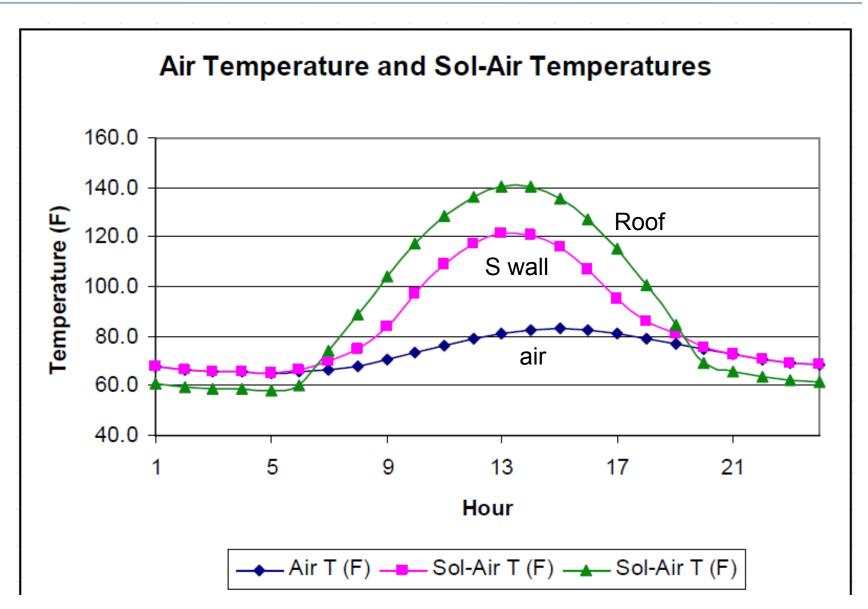
You would create a spreadsheet



Find incident solar radiation

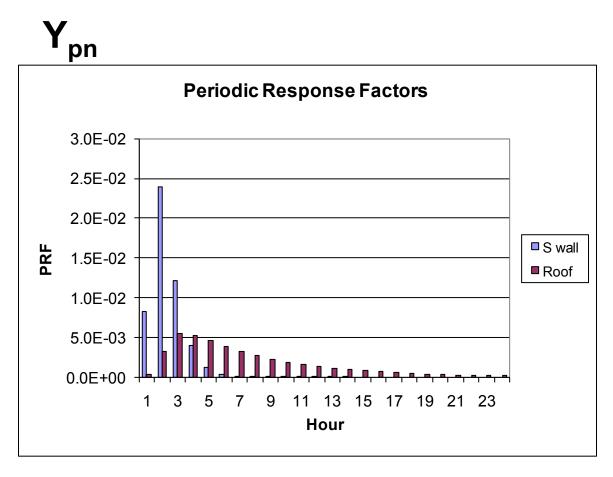


Find sol-air temperatures

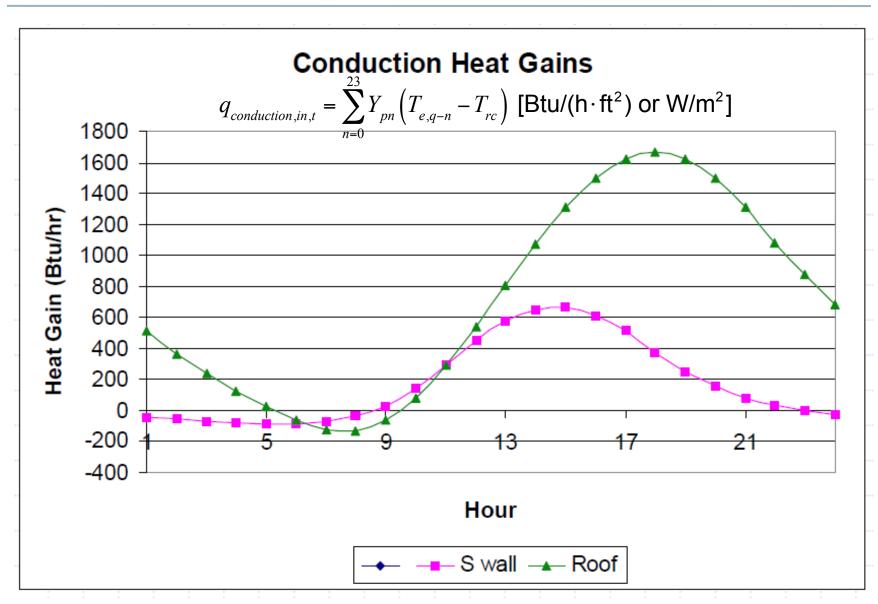


Find periodic response factors for conduction

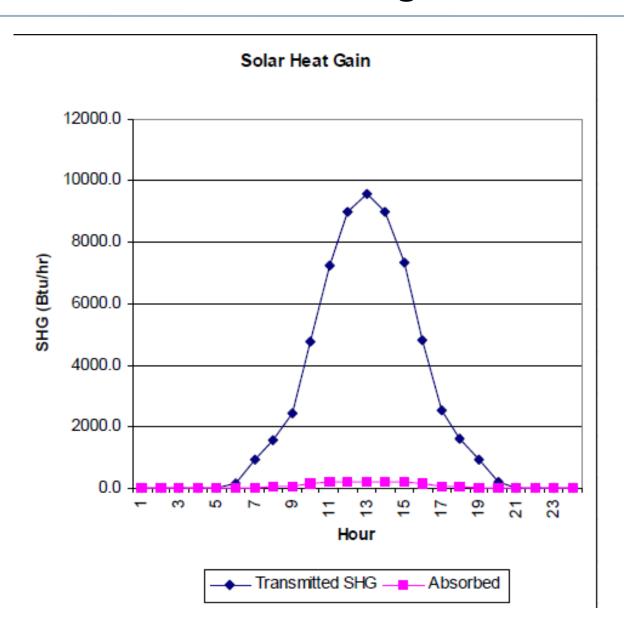
Ypn	S wall	Roof
1	8.2148E-03	3.5460E-04
2	2.3910E-02	3.2232E-03
3	1.2148E-02	5.5313E-03
4	4.0220E-03	5.3005E-03
5	1.1786E-03	4.5555E-03
6	3.2876E-04	3.8405E-03
7	8.9655E-05	3.2265E-03
8	2.4185E-05	2.7090E-03
9	6.4892E-06	2.2743E-03
10	1.7365E-06	1.9092E-03
11	4.6405E-07	1.6028E-03
12	1.2393E-07	1.3455E-03
13	3.3084E-08	1.1296E-03
14	8.8307E-09	9.4828E-04
15	2.3569E-09	7.9608E-04
16	6.2900E-10	6.6831E-04
17	1.6786E-10	5.6104E-04
18	4.4798E-11	4.7099E-04
19	1.1955E-11	3.9540E-04
20	3.1905E-12	3.3194E-04
21	8.5145E-13	2.7866E-04
22	2.2723E-13	2.3393E-04
23	6.0640E-14	1.9639E-04
24	1.6183E-14	1.6487E-04



Estimate hourly conductive heat gains



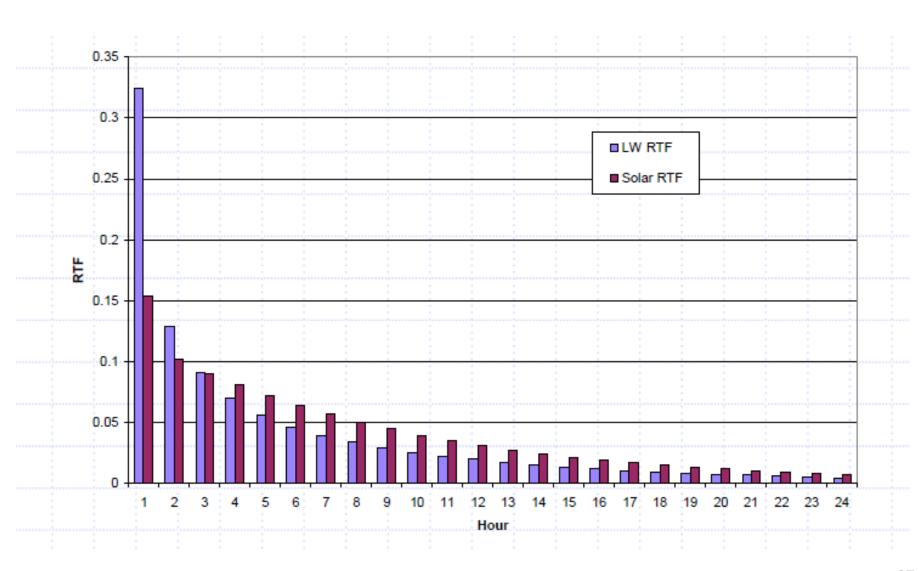
Find solar heat gains



Radiative vs. convective split gains

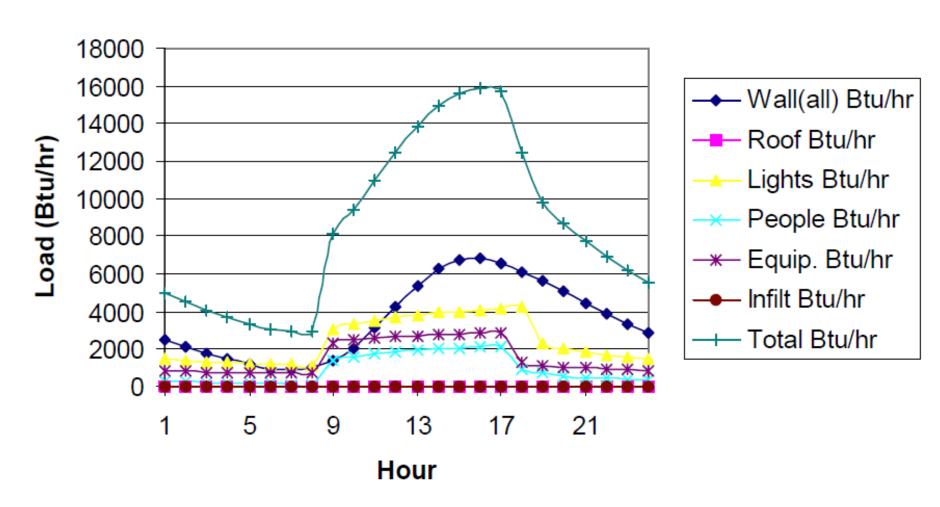
Heat Gain	% radiative	% convective		
Wall, window conduction	63	37		
Roof conduction	84	16		
People	70	30		
Lighting	67	33		
Equipment	20	80		
Transmitted solar heat gain	100	0		
Absorbed solar heat gain	63	37		
Infiltration	0	100		

Enter RTFs from ASHRAE



Component hourly cooling loads

Cooling Loads



Software tools for load calculations

- These are not done by hand, sometimes by spreadsheet
 - Many use ACCA Manual J
- Most use computer programs
- Big list of programs:
 - http://apps1.eere.energy.gov/buildings/tools_directory/subjects.cfm/ pagename=subjects/pagename_menu=whole_building_analysis/ pagename_submenu=load_calculation

Introduction to load calculation software

Two most commonly used programs for load calculations:

- Trane Trace 700
- Carrier HAP
- Your last HW will involve the use of Trane Trace 700 for load calculations
 - Work in teams
 - Download 30-day trial version here:
 http://www.trane.com/commercial/north-america/us/en/products-systems/
 design-and-analysis-tools/download-center/hvac-design-software-download-center.html



HW 6: Trane Trace 700

Getting Started

TRACE™ 700

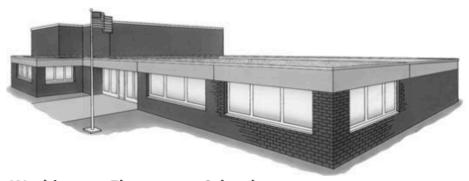
Comprehensive Building Analysis

version 6.2

Load Design Tutorial

Scenario

The architect provided a floor plan, descriptions of the construction materials, and other basic design criteria for the fictitious Washington Elementary School. You will finish creating a project file, define the rooms and HVAC systems, and print the results.



Washington Elementary School

Exam 2 review

- Topic coverage (concepts and calculations):
 - Mechanical systems
 - Refrigeration cycles
 - Air and water distribution systems
 - Fans/pumps
 - Ventilation and IAQ
 - Heating load calculations
 - Cooling load calculation methods
 - No calculations