CAE 331/513 Building Science Fall 2015



Week 4: September 17, 2015 Human thermal comfort



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Last time

- Our TA, Akram Ali, led an example problem session
 How did it go?
- Previously, we covered radiation, solar radiation, and heat transfer through windows
 - I_{solar}
 - Angle of incidence
 - Transmittance
 - Absorptivity
 - SHGC
 - U-values
 - Center of glass, edge of glass, frame
 - Combined modes of heat transfer

Today's objectives

 Combine what we know about *heat transfer* to understand <u>human thermal comfort</u>

Human thermal comfort

- One of our main goals in designing a building and its HVAC system(s) is to provide a suitably <u>comfortable environment</u> for the occupants
- In general, thermal comfort occurs when:
 - Body temperatures are held within narrow ranges
 - Skin moisture is low
 - The physiological effort of regulation is minimized
- Metrics for thermal comfort include quantifying the <u>amount</u> of <u>discomfort</u> that a space might present to people and what <u>fraction</u> of occupants are <u>dissatisfied</u> with a space



Energy balance of the human body

- The heat produced by the body's metabolism dissipates to the environment
 - Otherwise we would overheat
- If the rate of heat transfer away is <u>higher</u> than the rate of heat production, the body cools down and we feel cold
 - If heat transfer to surroundings is <u>lower</u> than our heat production, we feel hot
- This is a complex problem in transient heat transfer, involving radiation, convection, conduction, and evaporation, and many variables including skin wetness and clothing composition
 - We can simplify a lot of this



Energy balance of the human body

Your largest organ, your skin, covers ~2 m² and makes up ~15% of your body weight



https://ssb2012emilyashby.files.wordpress.com/2012/10/metabolism.jpg http://www.theseus-fe.com/images/thermal-manikin/manikinBoundaryConditions_big.JPG

Body energy balance in a space

- Our internal body temperatures are consistent around 36-37°C
- We can set our heat production rate equal to the instantaneous heat flow to the environment (assuming no storage):



$$q = M = q_{conv} + q_{rad} + q_{evap} + q_{resp,sens} + q_{resp,latent}$$

Body energy balance in a space

- Our internal body temperatures are consistent around 36-37°C
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Some obviously important variables for comfort:

- Activity level (heat production)
- Air temperature (convection)
- Air velocity (convection)
- Clothing level (skin temperature)
- Temperature of surrounding surfaces (radiation)
- Air relative and absolute humidity

Modeling gets complicated quickly....

$$\dot{Q} = MA_{skin} = \dot{Q}_{conv} + \dot{Q}_{rad} + \dot{Q}_{evap} + \dot{Q}_{resp,sens} + \dot{Q}_{resp,latent}$$

$$q = M = q_{conv} + q_{rad} + q_{evap} + q_{resp,sens} + q_{resp,latent}$$

Assessing thermal comfort

- To develop guidelines for thermal comfort, we have to have some idea of what we <u>perceive</u> to be comfortable
- Comfort analysis is usually done through <u>surveys</u> of users in real spaces and through controlled human experiments and a questionnaire that rates comfort on a seven point scale
- The result of the questionnaire is the Mean Vote (MV):

-3	-2	-1	0	+1	+2	+3
cold	cool	slightly cool	neutral	slightly warm	warm	hot

Predicted Mean Vote (PMV)

- We can attempt to <u>predict</u> the results of a questionnaire through equations and generate a **predicted mean vote** (PMV)
- The <u>PMV</u> is an estimate of the mean value that would be obtained if a large number of people were asked to vote on thermal comfort using a 7 point scale:



Survey the class...

Percent People Dissatisfied (PPD)

- Once we have the PMV (which are average results), we need to estimate how many people are <u>satisfied</u> with the thermal conditions for that PMV
 - We quantify that as the percent of people dissatisfied (PPD)
- Our design goal usually is to achieve a **PPD < 10%**
- After a lot of surveys and experiments, researchers have found that <u>PPD</u> is a nonlinear function of <u>PMV</u> that can be predicted reasonably well in most environments

Percent People Dissatisfied (PPD)

The PPD Function: 100 Since we want: 80 60 **PPD** < 10% 50 PREDICTED PERCENT DISSATISFIED (PPD) 40 we can see that: 30 -0.5 < PMV < 0.520 is our target 10 8 6 *Notice that the absolute 5 minimum PPD is 5% showing -2.0 -1.5 -1.0-0.50.5 1.0 1.5 2.0 0 that you cannot satisfy **PMV** everyone at the same time!

How many of you are "dissatisfied" with thermal comfort right now?

Predicting PMV and PPD

- How can we predict PMV and PPD?
- Fanger comfort analysis:
 - <u>Physically</u>: a relationship between the imbalance between heat flow from the body and the heat flow required for optimum thermal comfort
 - <u>Empirically</u>: Correlations derived between sensations of thermal comfort (PMV/PPD) and environmental variables:

 $PPD = 100 - 95 \exp[-(0.03353PMV^4 + 0.2179PMV^2)]$



Source: ASHRAE HoF 2013 & ASHRAE Standard 55

Thermal comfort standards in building design

• ASHRAE Standard 55 is the primary resource for engineers and architects to design for thermal comfort



ANSI/ASHRAE Standard 55-2013 (Supersedes ANSI/ASHRAE Standard 55-2010) Includes ANSI/ASHRAE addenda listed in Appendix M

Thermal Environmental Conditions for Human Occupancy

See Appendix M for approval dates by the ASHRAE Standards Committee, the ASHRAE Board of Directors, and the American National Standards Institute.

This standard is under continuous maintenance by a Standing Standard Project Committee (SIPC) for which the Standards Committee has established a documented program for regular publication of addends or revisions, including procedures for timely, documented, consensus action on regions for refunge to any pair of the standard. The change submittal form, instructions, and deadlines may be obtained in electronic form from the ASHRAE Web site (www.abrias.org) or in paper form from the Manager of Standards. The latent obtain of an ASHRAE Standard may be purchased from the ASHRAE Web site (www.abrias.org) or from ASHRAE Customer Service, 1791 Tallie Circle, NE, Atlanta, GA 100129-2005. E-mail: ordens()siterse.org, Fax: 478-519-2129. Telephone: 404-456-4900 (worklande), or sitil free 1:400-527-4723 (for ordens in US and Canada). For reprint permission, go to www.abries.org)eremission.

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1. PURPOSE

The purpose of this standard is to specify the combinations of indoor thermal environmental factors and personal factors that will produce thermal environmental conditions acceptable to a majority of the occupants within the space.

Variables affecting thermal comfort

ASHRAE Standard 55 considers 6 main parameters to govern thermal comfort

Some are familiar:

Ambient air temperature (*T*) Humidity (*W* or *RH*) Local air speed (*v*)

Some are probably not: Metabolic rate (M) Clothing insulation (I_{cl}) Mean radiant temperature (T_r)



• The total energy production rate of the human body is the sum of the production rates of heat (Q) and work (W):

$$\dot{Q} + \dot{W} = MA_{skin}$$

where

M = rate of metabolic energy production per surface area of skin (W/m²) A_{skin} = total surface area of skin (m²)

(work, *W*, is typically neglected), so: $\dot{Q} = MA_{skin}$

$$1 \text{ met} = 18.4 \frac{\text{Btu}}{\text{h} \cdot \text{ft}^2} = 58 \frac{\text{W}}{\text{m}^2}$$

- For an adult, the area of our skin is typically on the order of 16-22 ft² (1.5 to 2 m²)
 - Typically we use 1.8 m²

$$A_D = 0.202 m^{0.425} l^{0.725}$$

- A_D = DuBois surface area, m² m = mass, kg l = height, m
- So for a <u>typical adult</u> doing <u>typical indoor activities</u>, their heat production rate will be:

$$\dot{Q} + \dot{W} = MA_{skin} \approx (1 \text{ met})(1.8 \text{ m}^2)$$

 $\approx (58.2 \frac{W}{m^2})(1.8 \text{ m}^2) \approx 100 \text{ W} (\pm 20 \text{ W})$

Metabolic Rates for Typical Tasks

	Metabolic Rate		
Activity	Met Units	W/m ²	(Btu/h-ft ²)
Resting			
Sleeping	0.7	40	(13)
Reclining	0.8	45	(15)
Seated, quiet	1.0	60	(18)
Standing, relaxed	1.2	70	(22)
Walking (on level surface)			
0.9 m/s, 3.2 km/h, 2.0 mph	2.0	115	(37)
1.2 m/s, 4.3 km/h, 2.7 mph	2.6	150	(48)
1.8 m/s, 6.8 km/h, 4.2 mph	3.8	220	(70)
Office Activities			
Seated, reading, or writing	1.0	60	(18)
Typing	1.1	65	(20)
Filing, seated	1.2	70	(22)
Filing, standing	1.4	80	(26)
Walking about	1.7	100	(31)
Lifting/packing	2.1	120	(39)
Driving/Flying			
Automobile	1.0-2.0	60-115	(18-37)
Aircraft, routine	1.2	70	(22)
Aircraft, instrument landing	1.8	105	(33)
Aircraft, combat	2.4	140	(44)
Heavy vehicle	3.2	185	(59)

Metabolic rates (continued)

	Metabolic Rate		
Activity	Met Units	W/m ²	(Btu/h-ft ²)
Miscellaneous Occupational Activities			
Cooking	1.6-2.0	95-115	(29-37)
House cleaning	2.0-3.4	115-200	(37-63)
Seated, heavy limb movement	2.2	130	(41)
Machine work			
sawing (table saw)	1.8	105	(33)
light (electrical industry)	2.0-2.4	115-140	(37-44)
heavy	4.0	235	(74)
Handling 50 kg (100 lb) bags	4.0	235	(74)
Pick and shovel work	4.0-4.8	235-280	(74-88)
Miscellaneous Leisure Activities			
Dancing, social	2.4-4.4	140-255	(44-81)
Calisthenics/exercise	3.0-4.0	175-235	(55-74)
Tennis, single	3.6-4.0	210-270	(66-74)
Basketball	5.0-7.6	290-440	(92-140)
Wrestling, competitive	7.0-8.7	410-505	(129-160)

Thermal insulation, I_{cl}

- The thermal insulating effects of clothes are measured in clos (1 clo = 0.88 h·ft^{2.°}F/Btu)
- Insulating values for various garments are found in ASHRAE Fundamentals and Appendix B of Standard 55



Thermal insulation, I_{cl}

Clothing Insulation Values for Typical Ensembles^a

Clothing Description	Garments Included ^b	I _{cl} (clo)
Trousers	1) Trousers, short-sleeve shirt	
	2) Trousers, long-sleeve shirt	0.61
	3) #2 plus suit jacket	0.96
	4) #2 plus suit jacket, vest, T-shirt	1.14
	5) #2 plus long-sleeve sweater, T-shirt	1.01
	6) #5 plus suit jacket, long underwear bottoms	1.30
Skirts/Dresses	7) Knee-length skirt, short-sleeve shirt (sandals)	
	8) Knee-length skirt, long-sleeve shirt, full slip	0.67
	9) Knee-length skirt, long-sleeve shirt, half slip, long-sleeve sweater	1.10
	10) Knee-length skirt, long-sleeve shirt, half slip, suit jacket	1.04
	11) Ankle-length skirt, long-sleeve shirt, suit jacket	
Shorts	12) Walking shorts, short-sleeve shirt	0.36
Overalls/Coveralls	13) Long-sleeve coveralls, T-shirt	0.72
	14) Overalls, long-sleeve shirt, T-shirt	0.89
	15) Insulated coveralls, long-sleeve thermal underwear tops and bottoms	1.37
Athletic	16) Sweat pants, long-sleeve sweatshirt	0.74
Sleepwear	17) Long-sleeve pajama tops, long pajama trousers, short 3/4 length robe (slippers, no socks)	0.96

- Radiation to/from occupants is an important form of energy exchange
 - We can estimate its effects using the mean radiant temperature



- Radiation to/from occupants is an important form of energy exchange
 - We can estimate its effects using the mean radiant temperature



- The <u>mean radiant temperature</u> is the temperature of an imaginary uniform black box that results in the same radiation heat loss to the occupant as the current room
- This is particularly important for environments with drastically different surface temperatures
 - e.g. a poorly insulated window on a winter day has a surface temperature much lower than most other surfaces around it
 - e.g. a concrete slab warmed by the sun may have a higher temperature than its surroundings

$$\overline{T}_{r}^{4} = T_{1}^{4}F_{p-1} + T_{2}^{4}F_{p-2} + \dots + T_{N}^{4}F_{p-N}$$

where

 \overline{T}_r = mean radiant temperature, K T_N = surface temperature of surface N, K F_{p-N} = angle factor between a person and surface N

 View factors between people and horizontal or vertical rectangular surfaces



Predicting view factors and MRT gets complicated quickly as well...

Finding T_r from "globe temperature"

- We can measure the temperature of the interior of a black globe as well as the ambient air temperature to estimate MRT (T_r)
 - The black globe acts as a perfectly round black body radiator



$$T_{r} = \left[\left(T_{globe} + 273 \right)^{4} + \frac{1.1 \times 10^{8} v_{air}^{0.6}}{\varepsilon D^{0.4}} \left(T_{globe} - T_{air} \right) \right]^{1/4} - 273$$

 T_{globe} = temperature inside globe (°C) T_{air} = air temperature (°C) v_{air} = air velocity (m/s)

D = globe diameter (m) ϵ = emissivity of globe (-)

Operative temperature, T_o

 The <u>operative temperature</u> is essentially the average value between the air temperature and the mean radiant temperature, adjusted for air velocity effects:

Most accurate:

Less accurate:

Least accurate:

$$t_o = \frac{(h_r t_{mr} + h_c t_a)}{h_r + h_c} \qquad t_o = \frac{(t_{mr} + (t_a \times \sqrt{10v}))}{1 + \sqrt{10v}} \qquad t_o = \frac{(t_a + t_{mr})}{2}$$

 h_c = convective heat transfer coefficient h_r = linear radiative heat transfer coefficient t_a = air temperature t_{mr} = mean radiant temperature

*These are all reasonable to use depending on your application

Operative temperatures, air velocity, clo, and met levels



Fig. 14 Air Velocities and Operative Temperatures at 50% rh Necessary for Comfort (PMV = 0) of Persons in Summer Clothing at Various Levels of Activity

Operative temperatures, air velocity, clo, and met levels



Fig. 10 Percentage of People Dissatisfied as Function of Mean Air Velocity

Operative temperatures, air velocity, clo, and met levels



FIGURE 4.8 Preferred indoor air temperatures at various air velocities.

Defining the ASHRAE comfort zone



	Typical clothing insulation, clo	Optimum operative temperature	Indoor design temperature range
Winter	0.9	71°F (22°C)	69-74°F (20.5-23.5°C)
Summer	0.5	76°F (24.5°C)	74-79°F (23.5-26°C)

Defining the ASHRAE comfort zone



Fig. 5 ASHRAE Summer and Winter Comfort Zones [Acceptable ranges of operative temperature and humidity with air speed ≤ 0.2 m/s for people wearing 1.0 and 0.5 clo clothing during primarily sedentary activity (≤1.1 met)].

ASHRAE comfort zone: CBE Thermal Comfort Tool



http://smap.cbe.berkeley.edu/comforttool