CAE 208 / MMAE 320: Thermodynamics Fall 2023

October 17, 2023 Mass & energy analysis of control volumes (1)

Built Environment Research @ III] 🗫 🚓 M 💜

Advancing energy, environmental, and sustainability research within the built environment

www.built-envi.com

Dr. Mohammad Heidarinejad, Ph.D., P.E. Civil, Architectural and Environmental Engineering Illinois Institute of Technology muh182@iit.edu

ANNOUNCEMENTS



9TH ANNUAL CAEE CAREER FAIR

Hosted by CAEE orgs and Career Services

> OCTOBER 17, 2023 2:00PM - 5:00PM HERMAN HALL

A digital resume book will be made available to registered companies a week before the fair begins. For more information scan the QR code below!



• Assignment 5 due Thursday

- Midterm exam 1:
 - $\hfill\square$ The solutions files are uploaded
 - □ The exams were graded

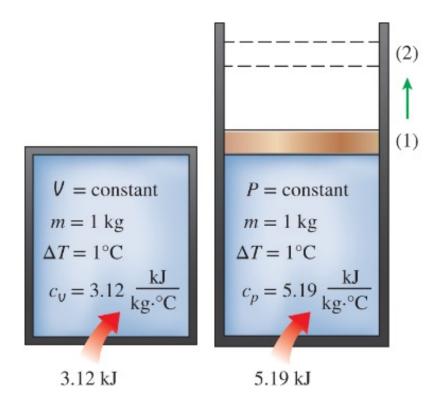
Midterm exam 1: Watch the recordings if you need additional review time

CAE_208_MMAE_320.2024 Panopto Content 10 (Thermodynamics)	
Home	
Syllabus	Q Search in folder "CAE_208_MMAE_320.202410: Thermodynamics"
Content	
Assignments	
Discussions	CAE_208_MMAE_320.202410: Thermodynamics
Collaborate Ultra	Sort by: Name Duration Date - Rating
Class Recording Pa	anopto
	Add folder
My Grades	
Email	I0/05/2023 Lecture14_Energy analysis of closed systems (2)
Galvin Library	
Tools 🗹	

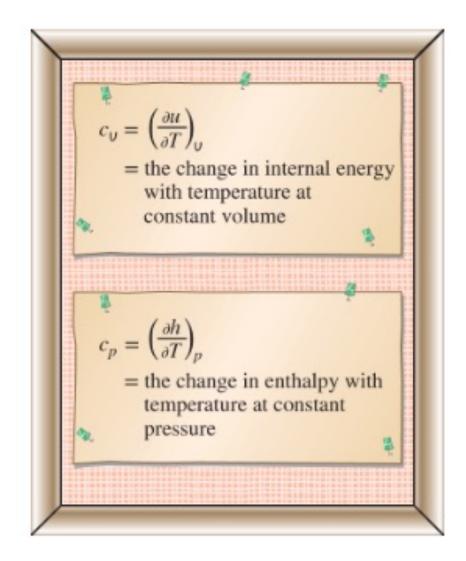
- Midterm exam 2:
 - November 07 (If we need to change it, please let me know as soon as possible)
 - □ All students are responsible for their open book exam part
 - No book / tables sharing will be allowed
 - I will not bring any extra books

RECAP

- Specific heat is defined as the energy required to raise temperature of a unit mass of substance by one degree
 - \Box Specific heat at constant volume (c_v)
 - \Box Specific heat at constant pressure (c_p)

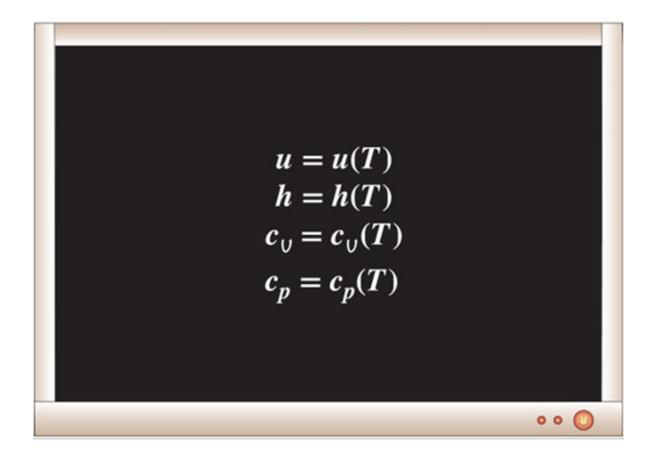


Recap



Recap

• We have:



• Three ways to calculate Δh and Δu :

$$\Delta u = u_2 - u_1 \text{ (table)}$$
$$\Delta u = \int_1^2 c_0 (T) dT$$
$$\Delta u \cong c_{0,\text{avg}} \Delta T$$

OBJECTIVES

- Develop the conservation of mass principle
- Apply the conservation of mass principle to various systems including steady- and unsteady-flow control volumes
- Apply the first law of thermodynamics as the statement of the conservation of energy principle to control volumes

Objectives

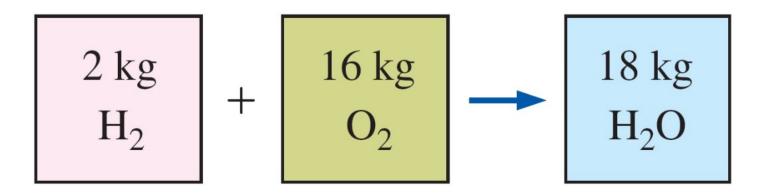
 Identify the energy carried by a fluid stream crossing a control surface as the sum of internal energy, flow work, kinetic energy, and potential energy of the fluid and to relate the combination of the internal energy and the flow work to the property enthalpy

Objectives

- Solve energy balance problems for common steady-flow devices such as nozzles, compressors, turbines, throttling valves, mixers, heaters, and heat exchangers
- Apply the energy balance to general unsteady-flow processes with particular emphasis on the uniform-flow process as the model for commonly encountered charging and discharging processes

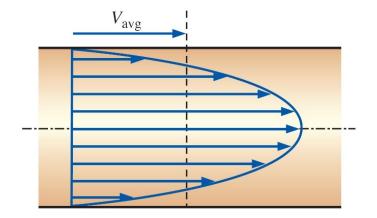
CONSERVATION OF MASS

 Conservation of mass: Mass, like energy, is a conserved property, and it cannot be created or destroyed during a process

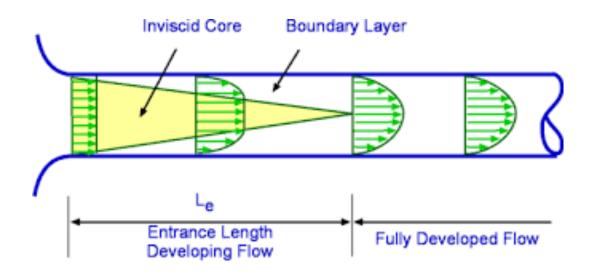


 In using control volumes, mass can cross the boundaries, and so we must keep track of the amount of mass entering and leaving the control volume

• Let's look at a flow in a pipe:

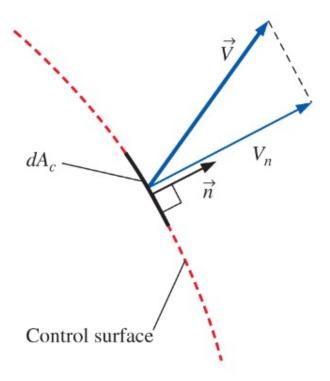


• Let's look at a flow in a pipe:



Mass and volume flow rates

 $\delta \dot{m} = \rho V_n dA_c$



• Mass and volume flow rates

$$\delta \dot{m} = \rho V_n dA_c$$

$$\dot{m} = \int \delta \dot{m} = \int \rho V_n dA_c$$

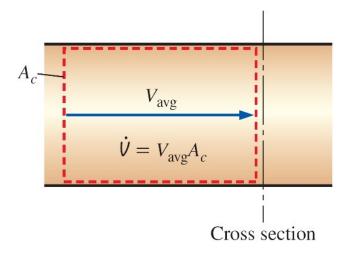
$$\dot{m} = \rho V_{avg} A_c$$

$$\dot{m} = \rho \dot{\forall} = \frac{\dot{\forall}}{\nu}$$

Mass and volume flow rates

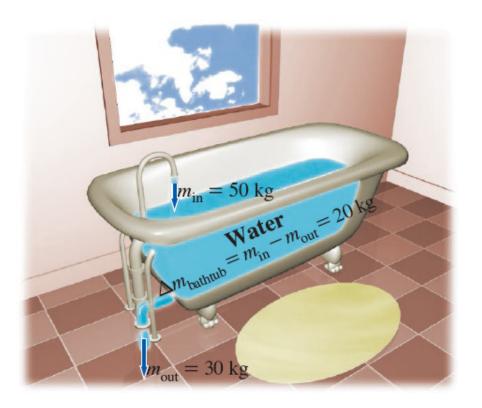
$$V_{avg} = \frac{1}{A_c} \int V_n dA_c$$

$$\dot{\forall} = \int V_n dA_c = V_{avg} A_c$$



• The conservation of mass for a control volume:

(Total mass entering the CV during Δt) – (Total mass leaving the CV during Δt) = (Net change of mass within the CV during Δt)



• The conservation of mass for a control volume:

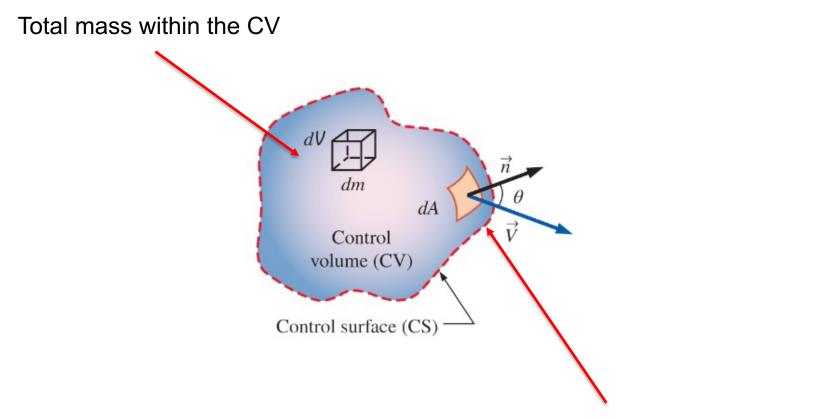
$$m_{in} - m_{out} = \Delta m_{CV}$$

$$\Delta m_{CV} = m_{final} - m_{initial}$$

$$\dot{m}_{in} - \dot{m}_{out} = \frac{dm_{CV}}{dt}$$

These equations are often referred to as the **mass balance** and are applicable to any control volume undergoing any kind of process.

• We can write in the integral form:

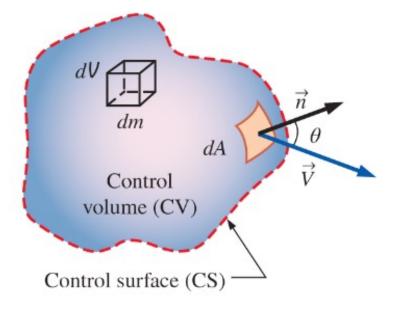


The mass flow rate through the boundaries

• Total mass within the CV:

Total mass within the CV

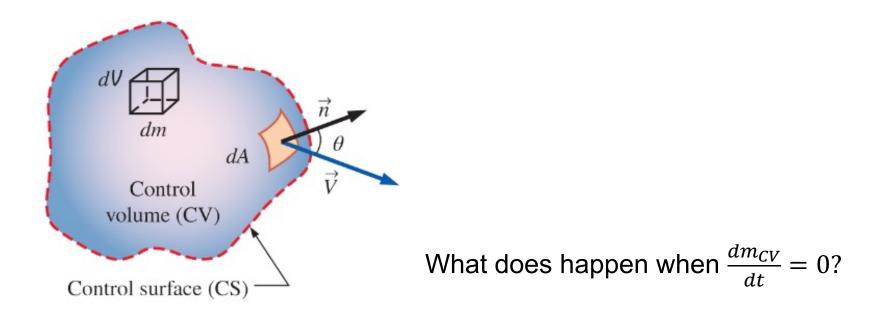
$$m_{CV} = \int_{CS} \rho d \forall$$



• The time rate of change of the amount of mass within the control volume is expressed as:

Rate of change of mass within the CV:

$$\frac{dm_{CV}}{dt} = \frac{d}{dt} \int_{CS} \rho d \forall$$



 The mass flow rate through dA is proportional to the fluid density and normal velocity (V_n)

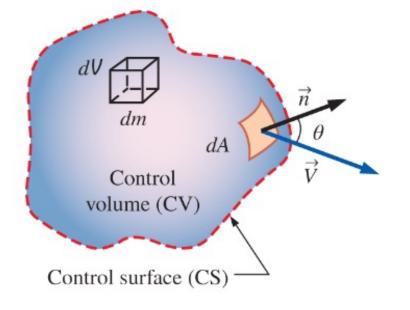
Normal component of velocity

$$V_n = V\cos(\theta) = \vec{V}.\vec{n}$$

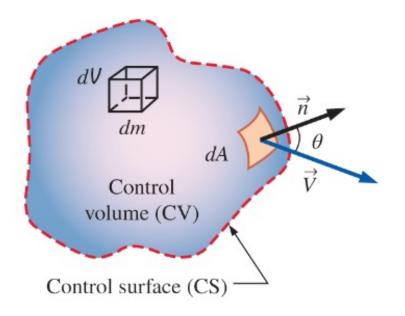
Differential mass flow rate

 $\delta \dot{m} = \rho V_n dA = \rho \big(V \cos(\theta) \big) dA$

$$=
ho(\vec{V}.\vec{n})dA$$



Net mass flow rate:
$$\dot{m}_{net} = \int_{CS} \delta \dot{m} = \int_{CS} \rho V_n dA = \int_{CS} \rho (\vec{V} \cdot \vec{n}) dA$$



$$\frac{dm_{CV}}{dt} + \dot{m}_{out} - \dot{m}_{in} = 0$$

$$\frac{dm_{CV}}{dt} = \frac{d}{dt} \int_{CS} \rho d \forall$$

$$\dot{m}_{net} = \int_{CS} \delta \dot{m} = \int_{CS} \rho V_n dA = \int_{CS} \rho \left(\vec{V} \cdot \vec{n} \right) dA$$

$$\frac{d}{dt} \int_{CS} \rho d\forall + \int_{CS} \rho \left(\vec{V} \cdot \vec{n} \right) dA = 0$$

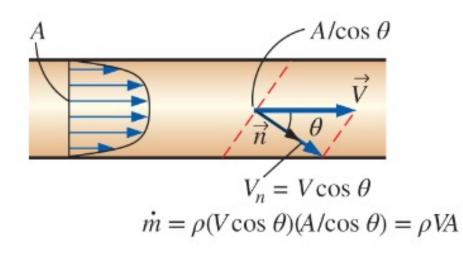
$$\frac{d}{dt} \int_{CS} \rho d\forall + \int_{CS} \rho \left(\vec{V} \cdot \vec{n} \right) dA = 0$$

$$\frac{d}{dt} \int_{CS} \rho d\forall + \sum_{out} \rho |V_n| A - \sum_{in} \rho |V_n| A = 0$$

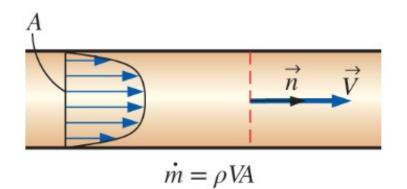
$$\frac{d}{dt} \int_{CS} \rho d \forall = \sum_{in} \dot{m} - \sum_{out} \dot{m}$$

$$\frac{dm_{CV}}{dt} = \sum_{in} \dot{m} - \sum_{out} \dot{m}$$

A control surface



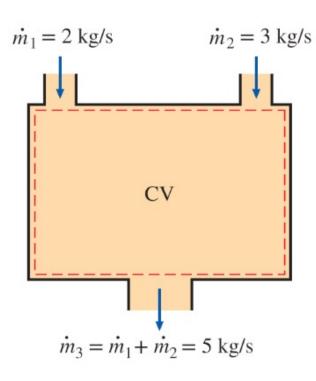
at an angle to the flow



normal to the flow

• Steady–flow:

$$\sum_{in} \dot{m} = \sum_{out} \dot{m}$$



• Steady–flow for a single stream:

$$\dot{m}_1 = \dot{m}_2 \qquad \rightarrow \qquad \rho_1 V_1 A_1 = \rho_2 V_2 A_2$$

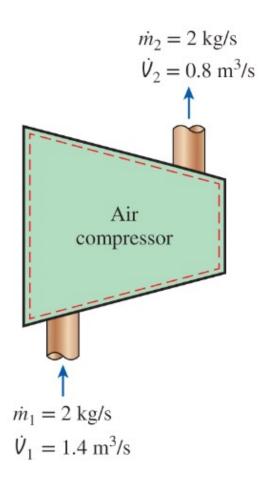
• Special case: Incompressible flow:

$$\sum_{in} \dot{\forall} = \sum_{out} \dot{\forall}$$

• Steady, incompressible flow (single stream):

$$\dot{\forall}_1 = \dot{\forall}_2 \quad \rightarrow \quad V_1 A_1 = V_2 A_2$$

• Let's look at the following steady-state:



CLASS ACTIVITY

Class Activity

- A garden hose attached with a nozzle is used to fill a 10gallon bucket. The inner diameter of the hose is 2 cm and it reduces to 0.8 cm at the nozzle exits. If it takes 50 s to fill the bucket with water, determine:
 - a) The volume and mass flow rates of water through the hose
 - b) The average velocity of water at the nozzle exit

• Solution (a):

$$\forall = 10 \ gal \times \left(\frac{3.7854 \ L}{1 \ gal}\right) = 37.854 \ L$$

$$\dot{\forall} = \frac{\forall}{\Delta t} = \frac{37.854 L}{50 s} = 0.757 \frac{L}{s}$$

$$\dot{m} = \rho \dot{\forall} = \left(1000 \frac{kg}{m^3}\right) \left(\frac{1000 \frac{kg}{L}}{1\frac{kg}{m^3}}\right) \left(0.757 \frac{L}{s}\right) = 0.757 \frac{kg}{s}$$

• Solution (b):

 $A_e = \pi \times r_e^2 = \pi \times (0.4 \ cm)^2 = 0.5027 \ cm^2 = 0.5027 \times 10^{-4} m^2$

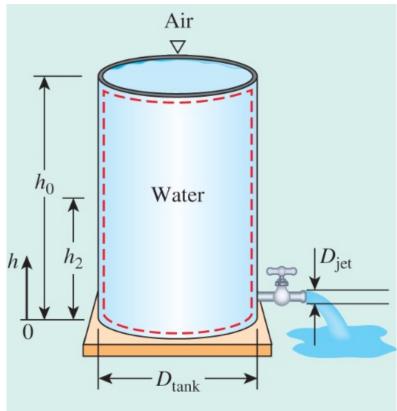
$$V_e = \frac{\dot{\forall}}{A_e} = \frac{0.757 \, L/s}{0.5027 \times 10^{-4} m^2} \left(\frac{1 \, m^3}{1000 \, L}\right) = 15.1 \, m/s$$

CLASS ACTIVITY

Class Activity

 A 4-ft high, 3-ft diameter cylindrical water tank whose top is open to the atmosphere is initially filled with water. Now the discharge plug near the bottom of the tank is pulled out, and a water jet whose diameter is 0.5 in streams.

The average velocity of the jet is approximated as $V = \sqrt{2gh}$ where h is the height of water in the tank measured from the center of the hole (a variable) and g is the gravitational acceleration. Determine how long it takes for the water level in the tank to drop 2 ft from the bottom.



$$\frac{dm_{CV}}{dt} = \dot{m}_{in} - \dot{m}_{out}$$

 $\dot{m}_{in} = 0$

$$\dot{m}_{out} = (\rho V A)_{out} = \rho \sqrt{2gh} A_{jet}$$

 $m_{CV} = \rho \forall = \rho A_{tank} h$

$$\frac{dm_{CV}}{dt} = \dot{m}_{in} - \dot{m}_{out}$$

$$-\rho\sqrt{2gh}\left(\frac{D_{tank}^2}{4}\right) = \frac{d}{dt}(\rho A_{tank}h)$$

$$-\rho\sqrt{2gh}\left(\frac{D_{tank}^2}{4}\right) = \rho(\frac{\pi D_{tank}^2}{4})\frac{dh}{dt}$$

$$dt = \frac{D_{tank}^2}{D_{jet}^2} \frac{dh}{\sqrt{2gh}}$$

$$dt = -\frac{D_{tank}^2}{D_{jet}^2} \frac{dh}{\sqrt{2gh}} \qquad \begin{cases} t = 0 \rightarrow & h = h_0 \\ t = t \rightarrow & h = h_2 \end{cases}$$

$$\int_0^t dt = -\frac{D_{tank}^2}{D_{jet}^2 \sqrt{2g}} \int_{h_1}^{h_2} \frac{dh}{\sqrt{h}}$$

$$t = \frac{\left(\sqrt{h_0} - \sqrt{h_2}\right)}{\sqrt{\frac{g}{2}}} \left(\frac{D_{tank}}{D_{jet}}\right)^2$$

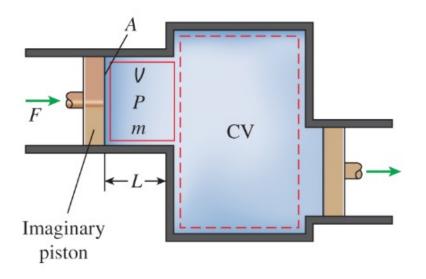
$$t = \frac{\left(\sqrt{4 \, ft} - \sqrt{2 \, ft}\right)}{\sqrt{\frac{32.2}{2}}} \left(\frac{3 \times 12 \, in}{0.5 \, in}\right)^2 = 757 \, s = 12.6 \, min$$

What does the entire flow exit the system?

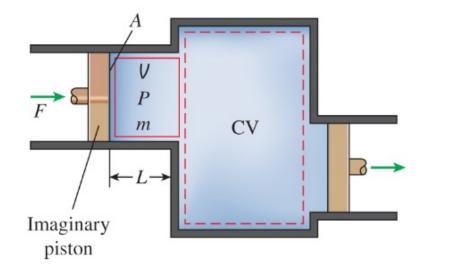
$$t = \frac{\left(\sqrt{4 \, ft} - \sqrt{0 \, ft}\right)}{\sqrt{\frac{32.2}{2}}} \left(\frac{3 \times 12 \, in}{0.5 \, in}\right)^2 = 43.1 \, min$$

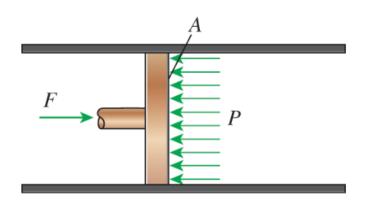
FLOW WORK AND ENERGY OF FLOWING FLUID

 Flow work (or flow energy): The work (or energy) required to push the mass into or out of the control volume. This work is necessary for maintaining a continuous flow through a control volume



 If the fluid pressure is P and the cross-sectional area of the fluid element is A, the force applied on the fluid by the imaginary piston is:





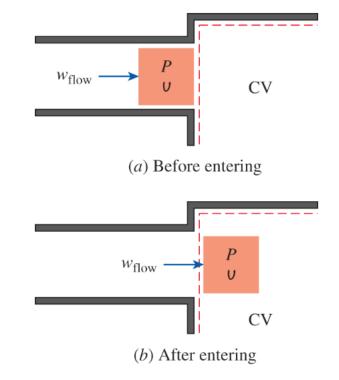
F = PA

 To push the entire fluid element into the control volume, this force must act through a distance L

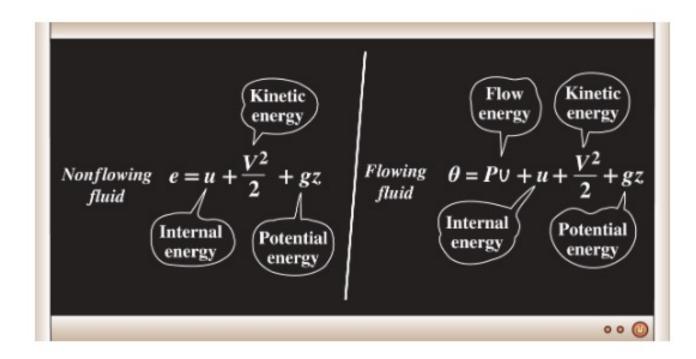
$$F = PA$$

$$W_{flow} = FL = PAL = P \forall$$

$$w_{flow} = Pv$$



• Total energy of a flowing fluid is:

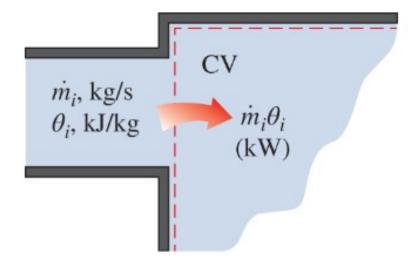


 $\theta = Pv + e = Pv + (u + ke + pe) = (u + Pv) + ke + pe$

• Energy transport by mass:

$$E_{mass} = m\theta = m(h + \frac{V^2}{2} + gz)$$

$$\dot{E}_{mass} = \dot{m}\theta = \dot{m}(h + \frac{V^2}{2} + gz)$$



• What does happen when mass is not constant:

$$E_{in,mass} = \int_{m_i} \theta_i \delta m_i = \int_{m_i} (h_i + \frac{V_i^2}{2} + gz_i) \, \delta m_i$$

CLASS ACTIVITY

Class Activity

- Air flows steadily in a pipe at 300 kPa, 77 °C, and 25 m/s at a rate of 18 kg/min. Determine:
 - a) The diameter of the pipe
 - b) The rate of flow energy
 - c) The rate of energy transport by mass
 - d) The error involved in part c if the kinetic energy is neglected.



Class Activity

- Solution (assumptions):
 - □ The flow is steady
 - □ The potential energy is negligible
 - □ R = 0.287 kJ/kg-K
 - \Box c_p=1.008 kJ/kg-K (at 350 K from Table A-2b)

• Solution (a):

$$v = \frac{RT}{P} = \frac{(0.287 \frac{kJ}{kg - K})(77 + 273)}{300 \, kPa} = 0.3349 \frac{m^3}{kg}$$

$$A = \frac{\dot{m}v}{V} = \frac{\left(\frac{18}{60}\frac{kg}{s}\right)(0.3349\frac{m^3}{kg})}{25\frac{m}{s}} = 0.004018\,m^2$$

$$D = \sqrt{\frac{4A}{\pi}} = \sqrt{\frac{4(0.004018 \ m^2)}{\pi}} = 0.0715 \ m$$

• Solution (b):

$$\dot{W}_{flow} = \dot{m}Pv = \left(\frac{18}{60}\frac{kg}{s}\right)(300\ kPa)\left(0.3349\frac{m^3}{kg}\right) = 30.14\ kW$$

• Solution (c):

$$\dot{E}_{mass} = \dot{m}(h + ke) = \dot{m}(c_pT + \frac{V^2}{2})$$

$$\dot{E}_{mass} = \left(\frac{18}{60} \frac{kg}{s}\right) \left[\left(1.008 \frac{kJ}{kg - K}\right) (77 + 273 K) + \left(\frac{1}{2}\right) \left(25 \frac{m}{s}\right)^2 \left(\frac{1 \frac{kJ}{kg}}{1000 \frac{m^2}{s^2}}\right) \right]$$

$$\dot{E}_{mass} = 105.94 \, kW$$

• Solution (d):

$$\dot{E}_{mass} = \dot{m}(h + ke) = \dot{m}h = \dot{m}c_pT$$

$$\dot{E}_{mass} = \dot{m}c_p T = \left(\frac{18}{60}\frac{kg}{s}\right) \left(1.005\frac{kJ}{kg-K}\right)(77 + 273K) = 105.84 \ kW$$