## CAE 208 / MMAE 320: Thermodynamics Fall 2023

## October 3, 2023 <br> Energy analysis of closed systems (1)

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Dr. Mohammad Heidarinejad, Ph.D., P.E. Civil, Architectural and Environmental Engineering Illinois Institute of Technology muh182@iit.edu

## ANNOUNCEMENTS

## Announcements

- The solution to Assignment 4 is posted
$\square$ Please submit one file only
- Always look at the solutions posted
- Assignment 5 will be posted next Tuesday (Time to focus on the exam)
- Midterm is scheduled for October 10
- Today's lecture will be in the exam (Content in our upcoming Thursday lecture will not be included in the exam)
- A problem-solving lecture was posted on Blackboard


## Announcements

- For the first midterm exam:

The first part of the exam is closed book (You are allowed to have one page for your cheat sheet to include equations)
The second part of the exam is open book (only a thermodynamics book or thermodynamics property tables)

## CLASS ACTIVITY

## COMPRESSIBILITY FACTOR - A MEASURE OF OF DEVIATION FROM IDEAL-GAS BEHAVIOR

## Compressibility Factor

- The figure shows $\left|\frac{v_{\text {table }}-v_{\text {ideal }}}{v_{\text {table }}}\right| \times 100$



## Compressibility Factor

- Z factor for all gases is approximately the same at the same reduced temperature and pressure due to the principle of corresponding states

$$
\begin{aligned}
& v=\frac{R T}{P} \\
& T_{R}=\frac{T}{T_{C r}}
\end{aligned}
$$

## Compressibility Factor

- Z factor for all gases is approximately the same at the same reduced temperature and pressure due to the principle of corresponding states

$$
\begin{aligned}
& P v=Z R T \\
& v=\frac{Z R T}{P} \\
& Z=\frac{v_{\text {actual }}}{v_{\text {idea }}}
\end{aligned}
$$

## Compressibility Factor

- We can define a "generalized compressibility chart"
- Let's look at a few observations:



## CLASS ACTIVITY

## Class Activity

- Determine specific volume of refrigeratnt-134a at 1 MPa and $50^{\circ} \mathrm{C}$ using (a) the ideal-gas equation of state and (b) the generalized compressibility chart. Compare the values obtained to the actual value of $0.021796 \mathrm{~m}^{3} / \mathrm{kg}$ and determine the error involved in each case.


## Class Activity

- Solution (a):

| TABLE A-1 |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Molar mass, gas constant, and critical-point properties |  |  |  |

$$
\begin{gathered}
v=\frac{R T}{P}=\frac{\left(0.0815 \frac{\mathrm{~kJ}}{\mathrm{~kg} \cdot \mathrm{~K}}\right)(50+273.15 \mathrm{~K})}{1000 \mathrm{kPa}}=0.026325 \frac{\mathrm{~m}^{3}}{\mathrm{~kg}} \\
\text { Error }=\frac{0.026325-0.021796}{0.021796}=0.208
\end{gathered}
$$

## Class Activity

- Solution (b):

$$
\begin{aligned}
& P_{R}=\frac{P}{P_{c r}}=\frac{1 M P a}{4.059 \mathrm{MPa}}=0.246 \\
& \quad Z=0.84 \\
& T_{R}=\frac{T}{T_{c r}}=\frac{323 \mathrm{~K}}{374.2 \mathrm{~K}}=0.863 \\
& v_{\text {actual }}=Z v_{\text {ideal }}=(0.84)\left(0.026325 \frac{\mathrm{~m}^{3}}{\mathrm{~kg}}\right)=0.022113 \frac{\mathrm{~m}^{3}}{\mathrm{~kg}} \\
& \text { Error }=\frac{0.022113-0.021796}{0.021796} \sim 0.02
\end{aligned}
$$

## CLASS ACTIVITY

## Class Activity

- Determine the specific volume of refrigerant-134a vapor at 0.9 MPa and $70^{\circ} \mathrm{C}$ based on
a) The ideal-gas equation
b) The generalized compressibility chart
c) Data from tables. Also, determine the error involved in the first two cases.


## Class Activity

- Solution (a):

| TABLE A-1 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Molar mass, gas constant, and critical-point properties |  |  |  |  |  |  |
| Substance | Formula M | Molar mass, $M \mathrm{~kg} / \mathrm{kmol}$ | Gas constant, $R \mathrm{~kJ} / \mathrm{kg} \cdot \mathrm{K}^{*}$ | Critical-point properties |  |  |
|  |  |  |  | Temperature, K | Pressure, MPa | Volume, $\mathrm{m}^{3} / \mathrm{kmol}$ |
| Propane | $\mathrm{C}_{3} \mathrm{H}_{8}$ | 44.097 | 0.1885 | 370 | 4.26 | 0.1998 |
| Propylene | $\mathrm{C}_{3} \mathrm{H}_{6}$ | 42.081 | 0.1976 | 365 | 4.62 | 0.1810 |
| Sulfur dioxide | $\mathrm{SO}_{2}$ | 64.063 | 0.1298 | 430.7 | 7.88 | 0.1217 |
| Tetrafluoroethane (R-134a) | $\mathrm{CF}_{3} \mathrm{CH}_{2} \mathrm{~F}$ | 102.03 | 0.08149 | 374.2 | 4.059 | 0.1993 |
| Trichlorofluoromethane (R-11) | $\mathrm{CCl}_{3} \mathrm{~F}$ | 137.37 | 0.06052 | 471.2 | 4.38 | 0.2478 |
| Water | $\mathrm{H}_{2} \mathrm{O}$ | 18.015 | 0.4615 | 647.1 | 22.06 | 0.0560 |
| Xenon | Xe | 131.30 | 0.06332 | 289.8 | 5.88 | 0.1186 |

$$
\begin{array}{ll}
R=0.08149 \frac{\mathrm{~kJ}}{\mathrm{~kg}-\mathrm{K}} & T_{c r}=374.2 \mathrm{~K} \\
P_{c r}=4.049 \mathrm{MPa}
\end{array}
$$

## Class Activity

- Solution (a):

$$
P v=R T
$$

$$
v=\frac{R T}{P}=\frac{\left(0.08149 \frac{\mathrm{~kJ}}{\mathrm{~kg}-\mathrm{K}}\right)(273.15+70 \mathrm{~K})}{0.9 \times 10^{3} \mathrm{kPa}}=0.03105 \frac{\mathrm{~m}^{3}}{\mathrm{~kg}}
$$

## Class Activity

- Solution (b):

$$
P_{R}=\frac{P}{P_{c r}}=\frac{0.9}{4.049}=0.222 \quad T_{R}=\frac{T}{T_{c r}}=\frac{343}{374.2}=0.917
$$


$Z=0.894$

## Class Activity

- Solution (b):

$$
v=Z v_{\text {ideal }}=(0.894)\left(0.03105 \frac{\mathrm{~m}^{3}}{\mathrm{~kg}}\right)=0.02776 \frac{\mathrm{~m}^{3}}{\mathrm{~kg}}
$$

## Class Activity

## - Solution (c):

## TABLE A-13

Superheated refrigerant-134a

| $\begin{aligned} & T \\ & { }^{\circ} \mathrm{C} \end{aligned}$ | $\mathrm{m}^{3} / \mathrm{kg}$ | u <br> kJ/kg | $\begin{aligned} & h \\ & \mathrm{~kJ} / \mathrm{kg} \end{aligned}$ | $\begin{aligned} & s \\ & \mathrm{~kJ} / \mathrm{kg} \cdot \mathrm{~K} \end{aligned}$ | $\mathrm{m}^{3} / \mathrm{kg}$ | $\begin{aligned} & u \\ & \mathrm{~kJ} / \mathrm{kg} \end{aligned}$ | $h$ <br> kJ/kg | $\begin{aligned} & \mathrm{kJ} / \mathrm{kg} \cdot \mathrm{~K} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $P=0.80 \mathrm{MPa}\left(T_{\text {sat }}=31.31^{\circ} \mathrm{C}\right)$ |  |  |  | $P=0.90 \mathrm{MPa}\left(T_{\text {sat }}=35.51{ }^{\circ} \mathrm{C}\right)$ |  |  |  |
| Sat. | 0.025645 | 246.82 | 267.34 | 0.9185 | 0.022686 | 248.82 | 269.25 | 0.9169 |
| 40 | 0.027035 | 254.84 | 276.46 | 0.9481 | 0.023375 | 253.15 | 274.19 | 0.9328 |
| 50 | 0.028547 | 263.87 | 286.71 | 0.9803 | 0.024809 | 262.46 | 284.79 | 0.9661 |
| 60 | 0.029973 | 272.85 | 296.82 | 1.0111 | 0.026146 | 271.62 | 295.15 | 0.9977 |
| 70 | 0.031340 | 281.83 | 306.90 | 1.0409 | 0.027413 | 280.74 | 305.41 | 1.0280 |
| 80 | 0.032659 | 290.86 | 316.99 | 1.0699 | 0.028630 | 289.88 | 315.65 | 1.0574 |
| 90 | 0.033941 | 299.97 | 327.12 | 1.0982 | 0.029806 | 299.08 | 325.90 | 1.0861 |

QUIZ

## MOVING BOUNDARY WORK

## Moving Boundary Work

- The expansion or compression work is often called moving boundary work or simply boundary work



## Moving Boundary Work

- The expansion or compression work is often called moving boundary work or simply boundary work



## Moving Boundary Work

- The moving work associated with real engines or compressors cannot be determined exactly from a thermodynamic analysis alone. Why?



## Moving Boundary Work

- Consider the gas enclosed in the cylinder-piston device
- The process is quasi equilibrium ( $d s$ )

$$
\delta W_{b}=F d s=P A d s=P d V
$$



## Moving Boundary Work

- Let's think about $d V$ in terms of expansion and compression


## Moving Boundary Work

- The total boundary work done during the entire process as the piston moves is obtained by adding all the differential works from the initial state to the final state

$$
W_{b}=\int_{1}^{2} P d V
$$

## Moving Boundary Work

- For a quasi-equilibrium expansion process, we can write:

$$
\text { Area }=A=\int_{1}^{2} d A=\int_{1}^{2} P d V
$$



## Moving Boundary Work

- Let's look at some basic integration

$$
\text { Area }=A=\int_{1}^{2} d A=W_{b}=\int_{1}^{2} P d V
$$

## Moving Boundary Work

- Basically, we can say:

The area under the process curve on a $P-V$ diagram is equal, in magnitude, to the work done during a quasiequilibrium expansion or compression process of a closed system (on the P-V diagram, in presents the boundary work done per unit mass)

## Moving Boundary Work

- The boundary work done during a process depends on the path followed as well as the end states:



## Moving Boundary Work

- The net work done during a cycle is the difference between the work done by the system and the work done on the system. Why?



## Moving Boundary Work

- We can use the equation for nonquasi-equilibrium process since properties are defined for equilibrium states only

$$
W_{b}=\int_{1}^{2} P_{i} d V
$$

## Moving Boundary Work

- We can use the equation for nonquasi-equilibrium process since properties are defined for equilibrium states only

$$
W_{b}=W_{\text {friction }}+W_{\text {atm }}+W_{\text {crank }}=\int_{1}^{2}\left(F_{\text {friction }}+P_{\text {atm }} A+F_{\text {crank }}\right) d x
$$

## CLASS ACTIVITY

## Class Activity

- A rigid tank contains air at 500 kPa and $150{ }^{\circ} \mathrm{C}$. As a result of heat to the surroundings, the temperature and pressure inside the tank drop to $65^{\circ} \mathrm{C}$ and 400 kPa , respectively. Determine the boundary work done during this process


## Class Activity

- Solution




## CLASS ACTIVITY

## Class Activity

- A frictionless piston-cylinder device contains 10 lbm of steam at 60 psia and $320^{\circ} \mathrm{F}$. Heat is now transferred to the steam until the temperature reaches $400^{\circ} \mathrm{F}$. If the piston is not attached to a shaft and its mass is constant, determine work done by the steam during this process.


## Class Activity

- Solution:

$$
\begin{aligned}
& W_{b}=\int_{1}^{2} P d V=P_{0} \int_{1}^{2} d V=P_{0}\left(V_{2}-V_{1}\right) \\
& W_{b}=m P_{0}\left(v_{2}-v_{1}\right)
\end{aligned}
$$

## Class Activity

- Solution:

$$
\left\{\begin{array}{l}
P_{1}=60 \mathrm{psia} \\
T_{1}=320^{\circ} \mathrm{F}
\end{array} \quad v_{1}=7.4863 \frac{\mathrm{ft}^{3}}{\mathrm{lbm}}\right.
$$

## Use Table A-6

$$
\left\{\begin{array}{l}
P_{2}=60 \mathrm{psia} \\
T_{2}=400^{\circ} \mathrm{F}
\end{array} \quad v_{2}=8.3548 \frac{\mathrm{ft}^{3}}{l b m}\right.
$$

$$
\begin{aligned}
W_{b} & =m P_{0}\left(v_{2}-v_{1}\right) \\
& =(10 l b m)(8.3548-7.4863)\left(\frac{f t^{3}}{l b m}\right)\left(\frac{1 B t u}{5.404 p s i a-f t^{3}}\right)=96.4 \mathrm{Btu}
\end{aligned}
$$

## Class Activity

## Conversion Factors

| Dimension | Metric | English |
| :---: | :---: | :---: |
| Acceleration | $1 \mathrm{~m} / \mathrm{s}^{2}=100 \mathrm{~cm} / \mathrm{s}^{2}$ | $\begin{aligned} & 1 \mathrm{~m} / \mathrm{s}^{2}=3.2808 \mathrm{ft} / \mathrm{s}^{2} \\ & 1 \mathrm{ft} / \mathrm{s}^{2}=0.3048 \mathrm{~m} / \mathrm{s}^{2} \end{aligned}$ |
| Area | $1 \mathrm{~m}^{2}=104 \mathrm{~cm}^{2}=10^{6} \mathrm{~mm}^{2}=10^{-6} \mathrm{~km}^{2}$ | $\begin{aligned} & 1 \mathrm{~m}^{2}=1550 \mathrm{in.}^{2}=10.764 \mathrm{ft}^{2} \\ & 1 \mathrm{ft}^{2}=144 \mathrm{in.}^{2}=0.0929034 \mathrm{~m}^{2} \end{aligned}$ |
| Density | $1 \mathrm{~g} / \mathrm{cm}^{3}=1 \mathrm{~kg} / \mathrm{L}=1000 \mathrm{~kg} / \mathrm{m}^{3}$ | $\begin{aligned} & 1 \mathrm{~g} / \mathrm{cm}^{3}=62.428 \mathrm{lbm} / \mathrm{ft}^{3}=0.036127 \mathrm{lbm} / \mathrm{in}^{3} \\ & 1 \mathrm{lbm} / \mathrm{in} .^{3}=1728 \mathrm{lbm} / \mathrm{ft}^{3} \\ & 1 \mathrm{~kg} / \mathrm{m}^{3}=0.062428 \mathrm{lbm} / \mathrm{ft}^{3} \end{aligned}$ |
| Energy, Heat, Work, Internal Energy, Enthalpy | $\begin{aligned} & 1 \mathrm{~kJ}=1000 \mathrm{~J}=1000 \mathrm{~N} \cdot \mathrm{~m}=1 \mathrm{kPa} \cdot \mathrm{~m}^{3} \\ & 1 \mathrm{~kJ} / \mathrm{kg}=1000 \mathrm{~m}^{2} / \mathrm{s}^{2} \\ & 1 \mathrm{kWh}=3600 \mathrm{~kJ} \\ & 1 \mathrm{~Wh}=3600 \mathrm{~J} \\ & 1 \mathrm{cal}=4.1868 \mathrm{~J} \\ & 1 \mathrm{Cal}=4.1868 \mathrm{~kJ} \end{aligned}$ | $\begin{aligned} & 1 \mathrm{~kJ}=0.94782 \mathrm{Btu} \\ & 1 \mathrm{Btu}=1.055056 \mathrm{~kJ} \\ & =5.40395 \mathrm{psia} \cdot \mathrm{ft}^{3} \\ & =778.169 \mathrm{lbf} \cdot \mathrm{ft} \\ & 1 \mathrm{Btu} / \mathrm{lbm}=25.037 \mathrm{ft}^{2} / \mathrm{s}^{2} \\ & =2.326 \mathrm{~kJ} / \mathrm{kg} \\ & 1 \mathrm{~kJ} / \mathrm{kg}=0.430 \mathrm{Btu} / \mathrm{lbm} \\ & 1 \mathrm{kWh}=3412.14 \mathrm{Btu} \\ & 1 \text { therm }=10^{5} \mathrm{Btu}=1.055 \times 10^{5} \mathrm{~kJ} \\ & \text { (natural gas) } \end{aligned}$ |

## CLASS ACTIVITY

## Class Activity

- A piston-cylinder device initially contains $0.4 \mathrm{~m}^{3}$ of air at 100 kPa and $80^{\circ} \mathrm{C}$. The air is now compressed to $0.1 \mathrm{~m}^{3}$ in such a way that the temperature inside the cylinder remains constant. Determine the work done during this process


## Class Activity

- Solution:



$$
P V=m R T_{0} \rightarrow P=\frac{C}{V}
$$

$$
W_{b}=\int_{1}^{2} P d V=\int_{1}^{2}\left(\frac{C}{V}\right) d V=C \int_{1}^{2}\left(\frac{d V}{V}\right)
$$

## Class Activity

- Solution:


$$
W_{b}=(100 k P a)\left(0.4 m^{3}\right)\left(\operatorname{Ln}\left(\frac{0.1}{0.4}\right)\right)\left(\frac{1 k J}{1 k P a . m^{2}}\right)=-55.5 k J
$$

## Moving Boundary Work

- During expansion or compression processes of gases and volume are often related in $\mathrm{PV}^{\mathrm{n}}=\mathrm{C}$ which is known as a Polytropic process



$$
P=C V^{-n}
$$

## Moving Boundary Work

- Polytropic process

$$
\begin{aligned}
& P=C V^{-n} \\
& W_{b}=\int_{1}^{2} P d V=\int_{1}^{2}\left(C V^{-n}\right) d V=\frac{C\left(\left(V^{-n+1}-V^{-n+1}\right)\right.}{(-n+1)}=\frac{P_{2} V_{2}-P_{1} V_{1}}{1-n}
\end{aligned}
$$

## Moving Boundary Work

- Polytropic process

$$
\begin{aligned}
& C=P_{1} V_{1}^{n}=P_{2} V_{2}^{n} \\
& W_{b}=\frac{m R\left(T_{2}-T_{1}\right)}{1-n} \quad n \neq 1(k J)
\end{aligned}
$$

## Moving Boundary Work

- For the case of $\mathrm{n}=1$

$$
W_{b}=\int_{1}^{2} P d V=\int_{1}^{2} C V^{-1} d V=P V \times \operatorname{Ln}\left(\frac{V_{2}}{V_{1}}\right)
$$

## CLASS ACTIVITY

## Class Activity

- A piston-cylinder device contains $0.05 \mathrm{~m}^{3}$ of a gas initially at 200 kPa . At this state, a linear spring that has a spring constant of $150 \mathrm{kN} / \mathrm{m}$ is touching the piston but exerting no force on it. Now heat is transferred to the gas, causing the piston to rise and to compress the spring until the volume inside the cylinder doubles. If the cross-sectional area of the piston is $0.25 \mathrm{~m}^{2}$, determine
a) The final pressure inside the cylinder
b) The total work done by the gas
c) The fraction of this work done against the spring to compress it


## Class Activity

- Solution


$$
\begin{aligned}
& V_{2}=2 V_{1}=2\left(0.05 \mathrm{~m}^{3}\right)=0.1 \mathrm{~m}^{3} \\
& x=\frac{\Delta V}{A}=\frac{(0.1-0.05) \mathrm{m}^{3}}{0.25 \mathrm{~m}^{2}}=0.2 \mathrm{~m}
\end{aligned}
$$

## Class Activity

- Solution

$$
\begin{aligned}
& P, \mathrm{kPa} \\
& F=k x=\left(150 \frac{\mathrm{kN}}{\mathrm{~m}}\right)(0.2 \mathrm{~m})=30 \mathrm{kN} \\
& P=\frac{F}{A}=\frac{30 \mathrm{kN}}{0.25 \mathrm{~m}^{2}}=120 \mathrm{kN} \\
& 200+120=320 \mathrm{kN}
\end{aligned}
$$

## Class Activity

- Solution (b)


$$
W=\text { area }=\frac{(200+320) k P a}{2}\left[0.1^{2}-0.05^{2}\right]\left(\frac{1 k J}{1 k P a . m^{2}}\right)=13 k J
$$

## Class Activity

- Solution (c)


$$
W_{\text {spring }}=\frac{1}{2}[320-200] k P a\left(0.05 m^{3}\right)=3 k J
$$

$$
W_{\text {spring }}=\frac{1}{2} k\left(x_{2}^{2}-x_{1}^{2}\right)=\frac{1}{2}(150)\left(0.2^{2}-0^{2}\right)=3 k J
$$

## Moving Boundary Work

- Moving boundary work under different processes

| Process | Moving boundary work |
| :--- | :---: |
| Constant volume | 0 |
| Constant pressure | $P_{0}\left(V_{2}-V_{1}\right)$ |
| Isothermal | $P_{1} V_{1} \times \operatorname{Ln}\left(\frac{V_{2}}{V_{1}}\right)$ |
|  | $P_{1} V_{1} \times \operatorname{Ln}\left(\frac{P_{1}}{P_{2}}\right)$ |
|  | $m R T_{o} \times \operatorname{Ln}\left(\frac{V_{2}}{V_{1}}\right)$ |
| Polytropic | $\frac{P_{2} V_{2}-P_{1} V_{1}}{1-n}$ |
|  | $\frac{m R\left(T_{2}-T_{1}\right)}{1-n}$ |

## ENERGY BALANCE FOR CLOSED SYSTEMS

## Energy Balance for Closed Systems

- The net change (increase or decrease) in the total energy of the system during a process is equal to the difference between the total energy entering and the total energy leaving the system during the process
(Total energy entering the system) - (Total energy leaving the system) $=$ (Change in the total energy of the sysem)

$$
E_{\text {in }}-E_{\text {out }}=\Delta E_{\text {system }}
$$

## Energy Balance for Closed Systems

- Energy change of a system $\Delta E_{\text {system }}$

$$
\begin{aligned}
& \text { Energy change }=\text { Energy at final state }- \text { Energy at initial state } \\
& \qquad \Delta E_{\text {system }}=E_{\text {final }}-E_{\text {initial }}=E_{2}-E_{1}
\end{aligned}
$$

Energy is a property, and the value of a property does not change unless the state of the system changes

## Energy Balance for Closed Systems

- We can sum the heat, work, and mass, and the heat transfer:

$$
E_{\text {in }}-E_{\text {out }}=\left(Q_{\text {in }}-Q_{\text {out }}\right)+\left(W_{\text {in }}-W_{\text {out }}\right)=\Delta E_{\text {system }}
$$



Net energy transfer by heat, work

Change in internal, kinetic, potential, ..., energies

## Energy Balance for Closed Systems

- We can sum the heat, work, and mass, and the heat transfer in the rate form:


Rate of change in internal, kinetic, potential, ..., energies

## Energy Balance for Closed Systems

- The energy balance can be expressed on a per unit mass basis as

$$
e_{\text {in }}-e_{\text {out }}=\Delta e_{\text {system }}
$$

## Energy Balance for Closed Systems

- For constant rates, we can write:

$$
Q=\dot{Q} \Delta t
$$

$$
W=\dot{W} \Delta t
$$

$$
E=\left(\frac{d E}{d t}\right) \Delta t
$$

## Energy Balance for Closed Systems

- For a closed system undergoing a cycle, the initial and final states are identical:

$$
\begin{aligned}
& \Delta E=E_{\text {in }}-E_{\text {out }}=0 \rightarrow E_{\text {in }}=E_{\text {out }} \\
& W_{\text {net,out }}=Q_{n e t, \text { in }} \rightarrow \dot{W}_{n e t, o u t}=\dot{Q}_{n e t, i n}
\end{aligned}
$$



## Energy Balance for Closed Systems

- We can write:


