## CAE 208 / MMAE 320: Thermodynamics Fall 2023

## September 28, 2023 Properties of Pure Substances (4)

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## ANNOUNCEMENTS

## Announcements

- Assignment 4 is due tonight
a Please submit one file only
$\square$ Always look at the solutions posted
- Assignment 5 will be posted next Tuesday
- Midterm is scheduled for October 10


## Announcements

- Starting next week, I will gradually introduce the bonus parts for working with coding or the hands-on activity

RECAP

## Recap

- The saturated liquid states can be connected by a line called saturated liquid line and similarly the saturated vapor line



## Recap

## APPENDIX 1

## PROPERTY TABLES AND CHARTS（SI UNITS）

| ，TABLE A－1 | Molar mass，gas constant，and critical－point properties 852 |
| :---: | :---: |
| TABLE A－2 | Ideal－gas specific heats of various common gases 853 |
| TABLE A－3 | Properties of common liquids，solids，and foods 856 |
| TABLE A－4 | Saturated water－Temperature table 858 |
| T TABLE A－5 | Saturated water－Pressure table 860 |
| TABLE A－6 | Superheated water 862 |
| TABLE A－7 | Compressed liquid water 866 |
| TABLE A－8 | Saturated ice－water vapor 867 |
| 蛔 FIGURE A－9 | $T$－s diagram for water 868 |
| FIGURE A－10 | Mollier diagram for water 869 |
| TABLE A－11 | Saturated refrigerant－134a－Temperature table 870 |
| TABLE A－12 | Saturated refrigerant－134a－Pressure table 872 |
| 团 TABLE A－13 | Superheated refrigerant－134a 873 |
| $\square$ FIGURE A－14 | $P$－h diagram for refrigerant－134a 875 |
| 匀TABLE A－15 | Properties of saturated water 876 |
| STABLE A－16 | Properties of saturated refrigerant－134a 877 |
| TABLE A－17 | Properties of saturated ammonia 878 |
| TABLE A－18 | Properties of saturated propane 879 |
| \TABLE A－19 | Properties of liquids 880 |
| 团 TABLE A－20 | Properties of liquid metals 881 |
| TABLE A－21 | Ideal－gas properties of air 882 |
| TABLE A－22 | Properties of air at 1 atm pressure 884 |
| TABLE A－23 | Properties of gases at 1 atm pressure 885 |
| TABLE A－24 | Properties of solid metals 887 |
| TABLE A－25 | Properties of solid nonmetals 890 |
| TABLE A－26 | Emissivities of surfaces 891 |
| （ FIGURE A－27 | The Moody chart 893 |
| SIGURE A－28 | Nelson－Obert generalized compressibility chart 894 |

## Recap

## APPENDIX 2

## PROPERTY TABLES AND CHARTS (ENGLISH UNITS)

| Table A-1E | Molar mass, gas constant, and critical-point properties 896 |
| :--- | :--- |
| Table A-2E | Ideal-gas specific heats of various common gases 897 |
| Table A-3E | Properties of common liquids, solids, and foods 900 |
| Table A-4E | Saturated water-Temperature table 902 |
| Table A-5E | Saturated water-Pressure table 904 |
| Table A-6E | Superheated water 906 |
| Table A-7E | Compressed liquid water 910 |
| Table A-8E | Saturated ice-water vapor 911 |
| Tigure A-9E | T-s diagram for water 912 |

See the references folder on Blackboard

## Recap

- Could you show on the T-v or P-v diagram when do we use each table?


## Recap

- If specific volume or enthalpy is given, how do we determine if the substance is a compressed liquid, saturated liquid, saturated liquid-vapor mixture, saturated vapor, or super heated?


## Recap

- For the saturated liquid-vapor mixture, we need to define a new property named "quality"

$$
\begin{gathered}
x=\frac{m_{\text {vapor }}}{m_{\text {total }}} \\
m_{\text {total }}=m_{\text {liquid }}+m_{\text {vapor }}=m_{f}+m_{g}
\end{gathered}
$$



- We can write:

$$
\begin{aligned}
& v_{a v g}=v_{f}+x v_{f g} \\
& u_{a v g}=u_{f}+x u_{f g} \\
& h_{a v g}=h_{f}+x h_{f g}
\end{aligned}
$$



## CLASS ACTIVITY

## Class Activity

- Determine temperature of water at a state of $P=0.5 \mathrm{MPa}$ and $\mathrm{h}=2,890 \mathrm{~kJ} / \mathrm{kg}$.


## Class Activity

- Solution:

| TABLE A-5 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Saturated water-Pressure table |  |  |  |  |  |  |  |  |  |
| Press., $P \mathrm{kPa}$ | Sat. temp., $T_{\text {sat }}{ }^{\circ} \mathrm{C}$ | Specific volume,$\mathrm{m}^{3} / \mathrm{kg}$ |  | Internal energy, <br> $\mathrm{kJ} / \mathrm{kg}$ |  |  | Enthalpy, <br> kJ/kg |  |  |
|  |  | Sat. <br> liquid, <br> $v_{f}$ | Sat. <br> vapor, <br> $u_{g}$ | Sat. <br> liquid, <br> $u_{f}$ | $\begin{aligned} & \text { Evap., } \\ & u_{f g} \end{aligned}$ | Sat. <br> vapor, <br> $u_{g}$ | Sat. <br> liquid, <br> $h_{f}$ | Evap., $h_{f g}$ | Sat. <br> vapor, <br> $h_{g}$ |
| 325 | 136.27 | 0.001076 | 0.56199 | 572.84 | 1973.1 | 2545.9 | 573.19 | 2155.4 | 2728.6 |
| 350 | 138.86 | 0.001079 | 0.52422 | 583.89 | 1964.6 | 2548.5 | 584.26 | 2147.7 | 2732.0 |
| 375 | 141.30 | 0.001081 | 0.49133 | 594.32 | 1956.6 | 2550.9 | 594.73 | 2140.4 | 2735.1 |
| 400 | 143.61 | 0.001084 | 0.46242 | 604.22 | 1948.9 | 2553.1 | 604.66 | 2133.4 | 2738.1 |
| 450 | 147.90 | 0.001088 | 0.41392 | 622.65 | 1934.5 | 2557.1 | 623.14 | 2120.3 | 2743.4 |
| 500 | 151.83 | 0.001093 | 0.37483 | 639.54 | 1921.2 | 2560.7 | 640.09 | 2108.0 | 2748.1 |



## Class Activity

- Solution:

| Superheated water |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $T$ | $u$ | $u$ | $h$ | $s$ |
| ${ }^{\circ} \mathrm{C}$ | $\mathrm{m}^{3} / \mathrm{kg}$ | $\mathrm{kJ} / \mathrm{kg}$ | $\mathrm{kJ} / \mathrm{kg}$ | kJ/kg $\cdot \mathrm{K}$ |
|  | $P=0.50 \mathrm{MPa}\left(151.83{ }^{\circ} \mathrm{C}\right)$ |  |  |  |
| Sat. | 0.37483 | 2560.7 | 2748.1 | 6.8207 |
| 200 | 0.42503 | 2643.3 | 2855.8 | 7.0610 |
| 250 | 0.47443 | 2723.8 | 2961.0 | 7.2725 |
| 300 | 0.52261 | 2803.3 | 3064.6 | 7.4614 |
| 350 | 0.57015 | 2883.0 | 3168.1 | 7.6346 |
| 400 | 0.61731 | 2963.7 | 3272.4 | 7.7956 |
| 500 | 0.71095 | 3129.0 | 3484.5 | 8.0893 |
| 600 | 0.80409 | 3300.4 | 3702.5 | 8.3544 |

## Class Activity

- Solution:

| $\boldsymbol{T}\left({ }^{\circ} \boldsymbol{C}\right)$ | $\boldsymbol{h}\left(\frac{\boldsymbol{k J}}{\boldsymbol{k g}}\right)$ |
| :--- | :---: |
| 200 | $2,855.8$ |
| T | 2,890 |
| 250 | $2,961.0$ |
| ( |  |
| $h=m T+b$ |  |
| $m=\frac{\Delta \mathrm{y}}{\Delta x}=\frac{\Delta \mathrm{h}}{\Delta T}=\frac{2,961.0-2,855.8}{250-200}=2.12$ |  |

## Class Activity

- Solution:

| $\boldsymbol{T}\left({ }^{\circ} \boldsymbol{C}\right)$ | $\boldsymbol{h}\left(\frac{\boldsymbol{k} \boldsymbol{k}}{\boldsymbol{k g}}\right)$ |
| :---: | :---: |
| 200 | $2,855.8$ |
| T | 2,890 |
| 250 | $2,961.0$ |

$$
\begin{aligned}
& h=m T+b \\
& @ T=200^{\circ} \mathrm{C} \rightarrow h=2,855.8=2.12(200)+b \rightarrow b=2,431.8 \\
& h=2.12 T+2431.8 \\
& h=2,890 \frac{\mathrm{~kJ}}{\mathrm{~kg}}=2.12 T+2431.8 \rightarrow T=216.3^{\circ} \mathrm{C}
\end{aligned}
$$

## Superheated Vapor

- Compared to the saturated vapor, superheated vapor is characterized by

```
Lower pressures ( }P<\mp@subsup{P}{\mathrm{ sat }}{}\mathrm{ at a given T)
Higher temperatures ( }T>\mp@subsup{T}{\mathrm{ sat }}{}\mathrm{ at a given }P\mathrm{ )
Higher specific volumes ( U> vg
Higher internal energies ( }u>\mp@subsup{u}{\textrm{g}}{\textrm{g}}\mathrm{ at a given }P\mathrm{ or T)
Higher enthalpies ( }h>\mp@subsup{h}{g}{}\mathrm{ at a given P}\mathrm{ or T)
```


## COMPRESSED LIQUID

## Compressed Liquid

- Compressed liquid tables are not as commonly available (Table A-7)
- In the absence of compressed liquid data, a general approximation is to treat compressed liquid as saturated liquid at the given temperature



## Compressed Liquid

- At low to moderate pressures and temperatures, we can say:

$$
h \sim h_{f @ T}+v_{f @ T}\left(P-P_{s a t ~ @ T}\right)
$$

## Compressed Liquid

- In general, a compressed liquid is characterized by:

Higher pressures $\left(P>P_{\text {sat }}\right.$ at a given $\left.T\right)$
Lower temperatures ( $T<T_{\text {sat }}$ at a given $P$ )
Lower specific volumes ( $U<U_{f}$ at a given $P$ or $T$ )
Lower internal energies $\left(u<u_{\mathrm{f}}\right.$ at a given $P$ or $T$ )
Lower enthalpies ( $h<h_{f}$ at a given $P$ or $T$ )

## CLASS ACTIVITY

## Class Activity

- Determine the internal energy of compressed liquid water at $80^{\circ} \mathrm{C}$ and 5 MPa , using (a) data from compressed liquid table and (b) saturated liquid data. What is the error involved in the second case.


## Class Activity

- Solution:



## Class Activity

- Solution:

| TABLE A-7 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Compressed liquid water |  |  |  |  |
| $T$ | $u$ | $u$ | $h$ | $s$ |
| ${ }^{\circ} \mathrm{C}$ | $\mathrm{m}^{3} / \mathrm{kg}$ | kJ/kg | kJ/kg | $\mathrm{kJ} / \mathrm{kg} \cdot \mathrm{K}$ |
| $P=5 \mathrm{MPa}\left(263.94{ }^{\circ} \mathrm{C}\right)$ |  |  |  |  |
| Sat. | 0.0012862 | 1148.1 | 1154.5 | 2.9207 |
| 0 | 0.0009977 | 0.04 | 5.03 | 0.0001 |
| 20 | 0.0009996 | 83.61 | 88.61 | 0.2954 |
| 40 | 0.0010057 | 166.92 | 171.95 | 0.5705 |
| 60 | 0.0010149 | 250.29 | 255.36 | 0.8287 |
| 80 | 0.0010267 | 333.82 | 338.96 | 1.0723 |
| 100 | 0.0010410 | 417.65 | 422.85 | 1.3034 |

## Class Activity

- Solution:

| TABLE A-4 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Saturated water-Temperature table |  |  |  |  |  |  |  |  |  |
| Temp.,$T^{\circ} \mathrm{C}$ | Sat. <br> press., $P_{\text {sat }} \mathrm{kPa}$ | Specific volume,$\mathrm{m}^{3} / \mathrm{kg}$ |  | Internal energy, <br> kJ/kg |  |  | Enthalpy, kJ/kg |  |  |
|  |  | Sat. <br> liquid, $v_{f}$ | Sat. <br> vapor, $v_{g}$ | Sat. <br> liquid, <br> $u_{f}$ | Evap., $u_{f g}$ | Sat. vapor, $u_{g}$ | Sat. <br> liquid, <br> $h_{f}$ | Evap., $h_{f g}$ | Sat. <br> vapor, $h_{g}$ |
| 0.01 | 0.6117 | 0.001000 | 206.00 | 0.000 | 2374.9 | 2374.9 | 0.001 | 2500.9 | 2500.9 |
| 5 | 0.8725 | 0.001000 | 147.03 | 21.019 | 2360.8 | 2381.8 | 21.020 | 2489.1 | 2510.1 |
| 10 | 1.2281 | 0.001000 | 106.32 | 42.020 | 2346.6 | 2388.7 | 42.022 | 2477.2 | 2519.2 |
| 15 | 1.7057 | 0.001001 | 77.885 | 62.980 | 2332.5 | 2395.5 | 62.982 | 2465.4 | 2528.3 |
| 20 | 2.3392 | 0.001002 | 57.762 | 83.913 | 2318.4 | 2402.3 | 83.915 | 2453.5 | 2537.4 |
| 25 | 3.1698 | 0.001003 | 43.340 | 104.83 | 2304.3 | 2409.1 | 104.83 | 2441.7 | 2546.5 |
| 30 | 4.2469 | 0.001004 | 32.879 | 125.73 | 2290.2 | 2415.9 | 125.74 | 2429.8 | 2555.6 |
| 35 | 5.6291 | 0.001006 | 25.205 | 146.63 | 2276.0 | 2422.7 | 146.64 | 2417.9 | 2564.6 |
| 40 | 7.3851 | 0.001008 | 19.515 | 167.53 | 2261.9 | 2429.4 | 167.53 | 2406.0 | 2573.5 |
| 45 | 9.5953 | 0.001010 | 15.251 | 188.43 | 2247.7 | 2436.1 | 188.44 | 2394.0 | 2582.4 |
| 50 | 12.352 | 0.001012 | 12.026 | 209.33 | 2233.4 | 2442.7 | 209.34 | 2382.0 | 2591.3 |
| 55 | 15.763 | 0.001015 | 9.5639 | 230.24 | 2219.1 | 2449.3 | 230.26 | 2369.8 | 2600.1 |
| 60 | 19.947 | 0.001017 | 7.6670 | 251.16 | 2204.7 | 2455.9 | 251.18 | 2357.7 | 2608.8 |
| 65 | 25.043 | 0.001020 | 6.1935 | 272.09 | 2190.3 | 2462.4 | 272.12 | 2345.4 | 2617.5 |
| 70 | 31.202 | 0.001023 | 5.0396 | 293.04 | 2175.8 | 2468.9 | 293.07 | 2333.0 | 2626.1 |
| 75 | 38.597 | 0.001026 | 4.1291 | 313.99 | 2161.3 | 2475.3 | 314.03 | 2320.6 | 2634.6 |
| 80 | 47.416 | 0.001029 | 3.4053 | 334.97 | 2146.6 | 2481.6 | 335.02 | 2308.0 | 2643.0 |

## Class Activity

- Solution:

$$
\text { Error }=\frac{334.94-333.82}{333.82} \times 100=0.34 \%
$$

QUIZ

## Quiz

## Quiz

## THE IDEAL-GAS EQUATION OF STATE

## The Ideal-Gas Equation of State

- Property tables provide very accurate information about the properties, but they are
-Bulky
- Vulnerable to typographical errors
- It would be nice to have a simple relationship


## The Ideal-Gas Equation of State

- Any equation that relates the pressure, temperature, and specific volume of a substance is called an equation of state (there simple and complex ones)
- We used vapor and gas often interchangeably in the first three chapters


## The Ideal-Gas Equation of State

- The simplest and best-known equation of state for substances in the gas phase is the ideal-gas equation of state

$$
\begin{aligned}
& P=R\left(\frac{T}{v}\right) \\
& P v=R T
\end{aligned}
$$

Ideal_gas equation of state

## The Ideal-Gas Equation of State

- We can define gas constant for each gas:

$$
R=\frac{R_{u}}{M}
$$

$$
\left(\frac{k J}{k g \cdot K} \text { or } \frac{k P a . m^{3}}{k g \cdot K}\right)
$$

$R_{u}$ is the universal gas constant

$$
R_{u}=\left\{\begin{array}{l}
8.31447 \mathrm{~kJ} / \mathrm{kmol} \cdot \mathrm{~K} \\
8.31447 \mathrm{kPa} \cdot \mathrm{~m}^{3} / \mathrm{kmol} \cdot \mathrm{~K} \\
0.0831447 \mathrm{bar} \cdot \mathrm{~m}^{3} / \mathrm{kmol} \cdot \mathrm{~K} \\
1.98588 \mathrm{Btu} / \mathrm{lbmol} \cdot \mathrm{R} \\
10.7316 \mathrm{psia} \cdot \mathrm{ft}^{3} / \mathrm{lbmol} \cdot \mathrm{R} \\
1545.37 \mathrm{ft} \cdot \mathrm{lbf} / \mathrm{lbmol} \cdot \mathrm{R}
\end{array}\right.
$$

## The Ideal-Gas Equation of State

- Examples of gas constant for a few known gases:



## The Ideal-Gas Equation of State

- $M$ is the molar mass
$\square$ The mass of one mole of a substance in grams or the mas of kmol in kilograms
$\square \mathrm{Or}$, the mass of 1 lbmol in lbm
(e.g., for Nitrogen we have $\mathrm{N}=28 \mathrm{~kg} / \mathrm{kmol}=28 \mathrm{lbm} / \mathrm{lbmol}$ )


## The Ideal-Gas Equation of State

- Several variations of the ideal-gas equation of state

$$
N=\frac{m}{M}
$$

| TABLE A-1 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Molar mass, gas constant, and critical-point properties |  |  |  |  |  |
| Substance | Formula | Molar mass, $M \mathrm{~kg} / \mathrm{kmol}$ | Gas constant, $R \mathrm{~kJ} / \mathrm{kg} \cdot \mathrm{K} *$ | Critical-p |  |
|  |  |  |  | Temperature, K | Pressur |
| Air | - | 28.97 | 0.2870 | 132.5 | 3. |
| Ammonia | $\mathrm{NH}_{3}$ | 17.03 | 0.4882 | 405.5 | 11. |
| Argon | Ar | 39.948 | 0.2081 | 151 | 4. |
| Benzene | $\mathrm{C}_{6} \mathrm{H}_{6}$ | 78.115 | 0.1064 | 562 | 4. |
| Bromine | $\mathrm{Br}_{2}$ | 159.808 | 0.0520 | 584 | 10. |
| $n$-Butane | $\mathrm{C}_{4} \mathrm{H}_{10}$ | 58.124 | 0.1430 | 425.2 | 3. |
| Carbon dioxide | $\mathrm{CO}_{2}$ | 44.01 | 0.1889 | 304.2 | 7. |
| Carbon monoxide | CO | 28.011 | 0.2968 | 133 | 3. |
| Carbon tetrachloride | $\mathrm{CCl}_{4}$ | 153.82 | 0.05405 | 556.4 | 4. |
| Chlorine | $\mathrm{Cl}_{2}$ | 70.906 | 0.1173 | 417 | 7. |
| Chloroform | $\mathrm{CHCl}_{3}$ | 119.38 | 0.06964 | 536.6 | 5 |
| Dichlorodifluoromethane (R-12) | $\mathrm{CCl}_{2} \mathrm{~F}_{2}$ | 120.91 | 0.06876 | 384.7 | 4 |

## The Ideal-Gas Equation of State

- Several variations of the ideal-gas equation of state

$$
\begin{aligned}
& v=\frac{V}{m} \\
& P\left(\frac{V}{m}\right)=R T \rightarrow P V=m R T
\end{aligned}
$$

## The Ideal-Gas Equation of State

- Several variations of the ideal-gas equation of state

$$
N=\frac{m}{M}
$$

$$
P V=(N M) R T
$$

$$
P V=N R_{u} T
$$

$$
P\left(\frac{V}{N}\right)=R_{u} T \quad \rightarrow P \bar{V}=R_{u} T
$$

## The Ideal-Gas Equation of State

- Properties per unit mole are:



## The Ideal-Gas Equation of State

- By writing the equation twice for a fixed mass and simplifying we can write:

$$
\begin{gathered}
P V=m R T \\
\frac{P_{1} V_{1}}{T_{1}}=\frac{P_{2} V_{2}}{T_{2}}
\end{gathered}
$$

## CLASS ACTIVITY

## Class Activity

- The gage pressure of an automobile tire is measure to be 210 kPa before a trip and 220 kPa after the trip at a location where the atmospheric pressure is 95 kPa . Assuming the volume of the tire remains constant and the air temperature before the trip is $25^{\circ} \mathrm{C}$, determine air temperature after the trip.


## Class Activity

- Solution:

$$
P_{1}=P_{\text {gage }, 1}+P_{\text {atm }}=210+95=305 \mathrm{kPa}
$$

$$
P_{2}=P_{\text {gage }, 2}+P_{\text {atm }}=220+95=315 \mathrm{kPa}
$$

$$
\frac{P_{1} V_{1}}{T_{1}}=\frac{P_{2} V_{2}}{T_{2}}=\frac{315 \mathrm{kPa}}{305 \mathrm{kPa}}(25+273.15 \mathrm{~K})=307.8 \mathrm{~K}=34.8^{\circ} \mathrm{C}
$$

## Is Water an Ideal Gas?



FIGURE 4-46
Percentage of error $\left(\left[\left|v_{\text {talde }}-v_{\text {ideal }}\right| / v_{\text {table }}\right] \times 100\right)$ involved in assuming steam to be an ideal gas, and the region where steam can be treated as an ideal gas with les

## COMPRESSIBILITY FACTOR - A MEASURE OF OF DEVIATION FROM IDEAL-GAS BEHAVIOR

## Compressibility Factor



FIGURE 4-46
Percentage of error $\left(\left[\left|v_{\text {talle }}-v_{\text {ideal }}\right| / v_{\text {table }}\right] \times 100\right)$ involved in assuming steam to be an ideal gas, and the region where steam can be treated as an ideal gas with les percent error.

## Compressibility Factor

- Z factor for all gases is approximately the same at the same reduced temperature and pressure due to the principle of corresponding states

$$
\begin{gathered}
P_{R}=\frac{P}{P_{c r}} \\
T_{R}=\frac{T}{T_{C r}}
\end{gathered}
$$

## Compressibility Factor

- We can define a "generalized compressibility chart"
- Let's look at a few observations:



## CLASS ACTIVITY

## Class Activity

- Determine specific volume of refrigeratnt-134a at 1 MPa and $50^{\circ} \mathrm{C}$ using (a) the ideal-gas equation of state and (b) the generalized compressibility chart. Compare the values obtained to the actual value of $0.021796 \mathrm{~m}^{3} / \mathrm{kg}$ and determine the error involved in each case.


## Class Activity

- Solution (a):

| TABLE A-1 |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Molar mass, gas constant, and critical-point properties |  |  |  |

$$
\begin{gathered}
v=\frac{R T}{P}=\frac{\left(0.0815 \frac{\mathrm{~kJ}}{\mathrm{~kg} \cdot \mathrm{~K}}\right)(50+273.15 \mathrm{~K})}{1000 \mathrm{kPa}}=0.026325 \frac{\mathrm{~m}^{3}}{\mathrm{~kg}} \\
\text { Error }=\frac{0.026325-0.021796}{0.021796}=0.208
\end{gathered}
$$

## Class Activity

- Solution (b):

$$
\begin{aligned}
& P_{R}=\frac{P}{P_{c r}}=\frac{1 \mathrm{MPa}}{4.059 \mathrm{MPa}}=0.246 \\
& \quad Z=0.84 \\
& T_{R}=\frac{T}{T_{c r}}=\frac{323 \mathrm{~K}}{374.2 \mathrm{~K}}=0.863 \\
& v_{\text {actual }}=Z v_{\text {ideal }}=(0.84)\left(0.026325 \frac{\mathrm{~m}^{3}}{\mathrm{~kg}}\right)=0.022113 \frac{\mathrm{~m}^{3}}{\mathrm{~kg}} \\
& \text { Error }=\frac{0.022113-0.021796}{0.021796} \sim 0.02
\end{aligned}
$$

## CLASS ACTIVITY

## Class Activity

- Determine the specific volume of refrigerant-134a vapor at 0.9 MPa and $70^{\circ} \mathrm{C}$ based on
a) The ideal-gas equation
b) The generalized compressibility chart
c) Data from tables. Also, determine the error involved in the first two cases.


## Class Activity

- Solution (a):

| TABLE A-1 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Molar mass, gas constant, and critical-point properties |  |  |  |  |  |  |
| Substance | Formula M | Molar mass, $M \mathrm{~kg} / \mathrm{kmol}$ | Gas constant, $R \mathrm{~kJ} / \mathrm{kg} \cdot \mathrm{K}^{*}$ | Critical-point properties |  |  |
|  |  |  |  | Temperature, K | Pressure, MPa | Volume, $\mathrm{m}^{3} / \mathrm{kmol}$ |
| Propane | $\mathrm{C}_{3} \mathrm{H}_{8}$ | 44.097 | 0.1885 | 370 | 4.26 | 0.1998 |
| Propylene | $\mathrm{C}_{3} \mathrm{H}_{6}$ | 42.081 | 0.1976 | 365 | 4.62 | 0.1810 |
| Sulfur dioxide | $\mathrm{SO}_{2}$ | 64.063 | 0.1298 | 430.7 | 7.88 | 0.1217 |
| Tetrafluoroethane (R-134a) | $\mathrm{CF}_{3} \mathrm{CH}_{2} \mathrm{~F}$ | 102.03 | 0.08149 | 374.2 | 4.059 | 0.1993 |
| Trichlorofluoromethane (R-11) | $\mathrm{CCl}_{3} \mathrm{~F}$ | 137.37 | 0.06052 | 471.2 | 4.38 | 0.2478 |
| Water | $\mathrm{H}_{2} \mathrm{O}$ | 18.015 | 0.4615 | 647.1 | 22.06 | 0.0560 |
| Xenon | Xe | 131.30 | 0.06332 | 289.8 | 5.88 | 0.1186 |

$$
\begin{array}{ll}
R=0.08149 \frac{\mathrm{~kJ}}{\mathrm{~kg}-\mathrm{K}} & T_{c r}=374.2 \mathrm{~K} \\
P_{c r}=4.049 \mathrm{MPa}
\end{array}
$$

## Class Activity

- Solution (a):

$$
P v=R T
$$

$$
v=\frac{R T}{P}=\frac{\left(0.08149 \frac{\mathrm{~kJ}}{\mathrm{~kg}-\mathrm{K}}\right)(273.15+70 \mathrm{~K})}{0.9 \times 10^{3} \mathrm{kPa}}=0.03105 \frac{\mathrm{~m}^{3}}{\mathrm{~kg}}
$$

## Class Activity

- Solution (b):

$$
P_{R}=\frac{P}{P_{c r}}=\frac{0.9}{4.049}=0.222 \quad T_{R}=\frac{T}{T_{c r}}=\frac{343}{374.2}=0.917
$$


$Z=0.894$

## Class Activity

- Solution (b):

$$
v=Z v_{\text {ideal }}=(0.894)\left(0.03105 \frac{\mathrm{~m}^{3}}{\mathrm{~kg}}\right)=0.02776 \frac{\mathrm{~m}^{3}}{\mathrm{~kg}}
$$

## Class Activity

## - Solution (c):

## TABLE A-13

Superheated refrigerant-134a

| $T$ ${ }^{\circ} \mathrm{C}$ | $\mathrm{m}^{3} / \mathrm{kg}$ | $u$ <br> $\mathrm{kJ} / \mathrm{kg}$ | $h$ <br> kJ/kg | $\mathrm{kJ} / \mathrm{kg} \cdot \mathrm{~K}$ | $\mathrm{m}^{3} / \mathrm{kg}$ | u <br> $\mathrm{kJ} / \mathrm{kg}$ | $h$ <br> kJ/kg | $\mathrm{kJ} / \mathrm{kg} \cdot \mathrm{~K}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $P=0.80 \mathrm{MPa}\left(T_{\text {sat }}=31.31^{\circ} \mathrm{C}\right)$ |  |  |  | $P=0.90 \mathrm{MPa}\left(T_{\text {sat }}=35.51{ }^{\circ} \mathrm{C}\right)$ |  |  |  |
| Sat. | 0.025645 | 246.82 | 267.34 | 0.9185 | 0.022686 | 248.82 | 269.25 | 0.9169 |
| 40 | 0.027035 | 254.84 | 276.46 | 0.9481 | 0.023375 | 253.15 | 274.19 | 0.9328 |
| 50 | 0.028547 | 263.87 | 286.71 | 0.9803 | 0.024809 | 262.46 | 284.79 | 0.9661 |
| 60 | 0.029973 | 272.85 | 296.82 | 1.0111 | 0.026146 | 271.62 | 295.15 | 0.9977 |
| 70 | 0.031340 | 281.83 | 306.90 | 1.0409 | 0.027413 | 280.74 | 305.41 | 1.0280 |
| 80 | 0.032659 | 290.86 | 316.99 | 1.0699 | 0.028630 | 289.88 | 315.65 | 1.0574 |
| 90 | 0.033941 | 299.97 | 327.12 | 1.0982 | 0.029806 | 299.08 | 325.90 | 1.0861 |

