# CAE 208 Thermal-Fluids Engineering I MMAE 320: Thermodynamics Fall 2022

### October 25, 2022 Mass and Energy Analysis of Control Volumes (II)

Built Environment Research @ IIT

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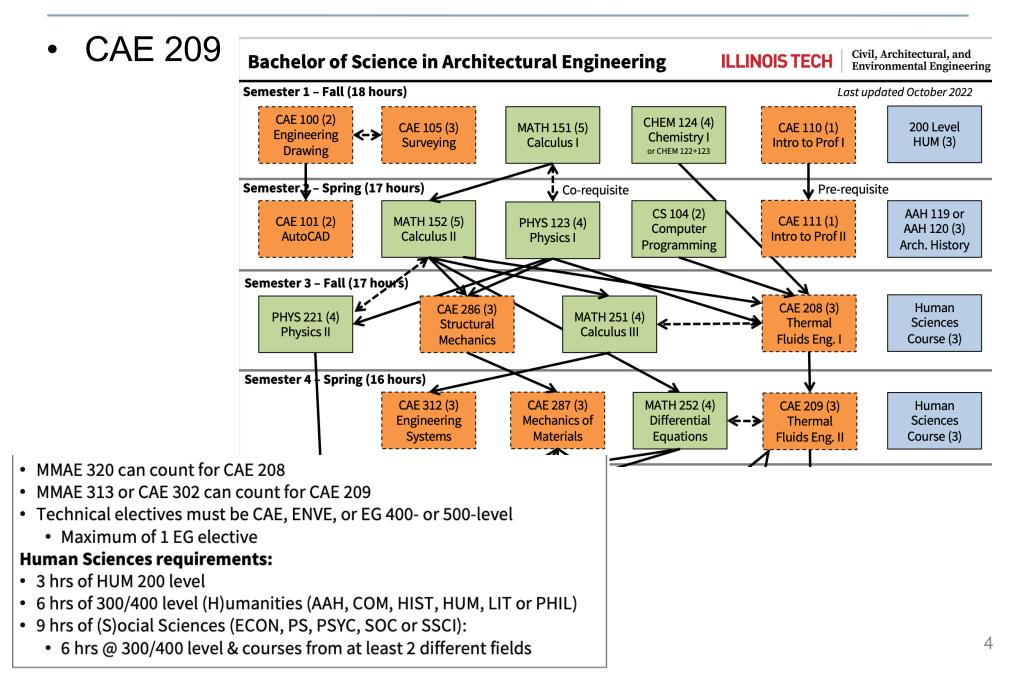
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### ANNOUNCEMENTS

#### Announcements

- Assignment 6 is posted
- Next midterm exam is November 10

#### Announcements



#### Announcements

#### • CAE 464

#### The Built Environment Research Group

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#### CAE 464/517: HVAC Systems Design (Spring 2021)

#### **Course Description**

This course introduce students to both theory and applied design procedures for HVAC equipment and systems. By taking this course students will be able to:

- 1. Understand fundamentals of fluid and energy flows for HVAC equipment and systems
- 2. Design and size air distribution systems, hydronic systems, and refrigeration systems
- 3. Design, draw, and read mechanical drawings
- 4. Design, review, and assess different HVAC designs
- 5. Propose recommendations to revise HVAC designs and retrofit existing HVAC systems
- 6. Utilize both hand calculations and computer modeling (graduate students) for sizing air distribution systems, hydronic systems, and refrigeration systems

Course Syllabus (updated as we go; includes current schedule)

Most recent syllabus, updated January 19, 2021

#### Lecture

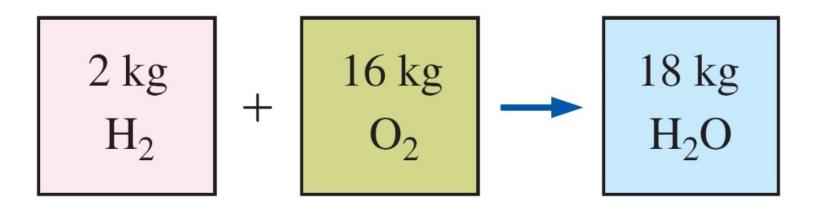
- Lecture 01: Course overview and introduction
- Lecture 02: Review of HVAC system drawings
- Lecture03: Installation
- Lecture 04: Psychrometrics processes and space conditioning
- Lecture 05: Design conditions and heating loads

#### http://built-envi.com/courses/cae-464-517-hvac-systems-design-spring-2021/

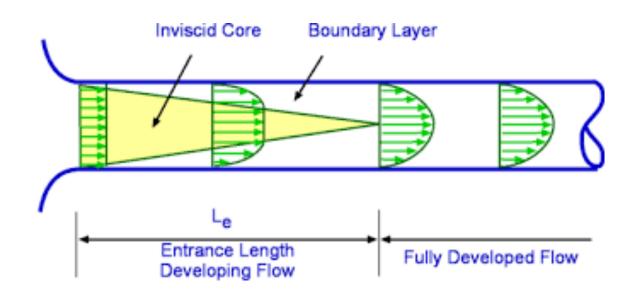
#### RECAP

#### Recap

 Conservation of mass: Mass, like energy, is a conserved property, and it cannot be created or destroyed during a process



 In using control volumes, mass can cross the boundaries, and so we must keep track of the amount of mass entering and leaving the control volume • Let's look at a flow in a pipe:



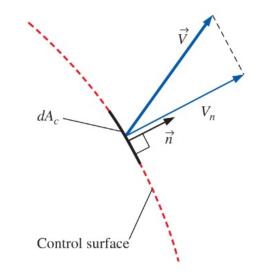
• Mass and volume flow rates

$$\delta \dot{m} = \rho V_n dA_c$$

$$\dot{m} = \int \delta \dot{m} = \int \rho V_n dA_c$$

$$\dot{m} = \rho V_{avg} A_c$$

$$\dot{m} = \rho \dot{\forall} = \frac{\dot{\forall}}{\nu}$$



• The conservation of mass for a control volume:

$$m_{in} - m_{out} = \Delta m_{CV}$$

$$\Delta m_{CV} = m_{final} - m_{initial}$$

$$\dot{m}_{in} - \dot{m}_{out} = \frac{dm_{CV}}{dt}$$

These equations are often referred to as the **mass balance** and are applicable to any control volume undergoing any kind of process.

• We can write the net flow rate:

$$\frac{d}{dt} \int_{CS} \rho d \forall = \sum_{in} \dot{m} - \sum_{out} \dot{m}$$

$$\frac{dm_{CV}}{dt} = \sum_{in} \dot{m} - \sum_{out} \dot{m}$$

• Special case: Incompressible flow:

$$\sum_{in} \dot{\forall} = \sum_{out} \dot{\forall}$$

• Steady, incompressible flow (single stream):

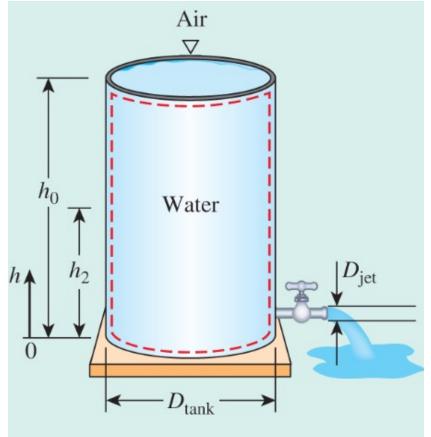
$$\dot{\forall}_1 = \dot{\forall}_2 \quad \rightarrow \quad V_1 A_1 = V_2 A_2$$

### **CLASS ACTIVITY**

#### **Class Activity**

 A 4-ft high, 3-ft diameter cylindrical water tank whose top is open to the atmosphere is initially filled with water. Now the discharge plug near the bottom of the tank is pulled out, and a water jet whose diameter is 0.5 in streams.

The average velocity of the jet is approximated as  $V = \sqrt{2gh}$  where h is the height of water in the tank measured from the center of the hole (a variable) and g is the gravitational acceleration. Determine how long it takes for the water level in the tank to drop 2 ft from the bottom.



$$\frac{dm_{CV}}{dt} = \dot{m}_{in} - \dot{m}_{out}$$

$$\dot{m}_{in} = 0$$

$$\dot{m}_{out} = (\rho V A)_{out} = \rho \sqrt{2gh} A_{jet}$$

 $m_{CV} = \rho \forall = \rho A_{tank} h$ 

$$\frac{dm_{CV}}{dt} = \dot{m}_{in} - \dot{m}_{out}$$
$$-\rho\sqrt{2gh} \left(\frac{D_{tank}^2}{4}\right) = \frac{d}{dt}(\rho A_{tank}h)$$
$$(D^2) = \pi D^2 - dh$$

$$-\rho\sqrt{2gh}\left(\frac{D_{tank}^2}{4}\right) = \rho(\frac{\pi D_{tank}^2}{4})\frac{dh}{dt}$$

$$dt = \frac{D_{tank}^2}{D_{jet}^2} \frac{dh}{\sqrt{2gh}}$$

$$dt = -\frac{D_{tank}^2}{D_{jet}^2} \frac{dh}{\sqrt{2gh}} \qquad \begin{cases} t = 0 \rightarrow & h = h_0 \\ t = t \rightarrow & h = h_2 \end{cases}$$

$$\int_0^t dt = -\frac{D_{tank}^2}{D_{jet}^2 \sqrt{2g}} \int_{h_1}^{h_2} \frac{dh}{\sqrt{h}}$$

$$t = \frac{\left(\sqrt{h_0} - \sqrt{h_2}\right)}{\sqrt{\frac{g}{2}}} \left(\frac{D_{tank}}{D_{jet}}\right)^2$$

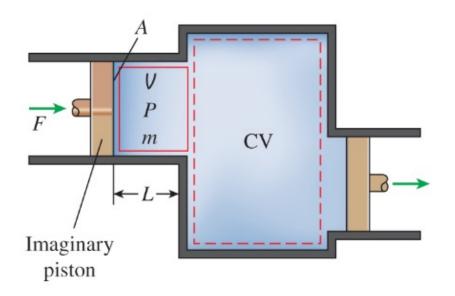
$$t = \frac{\left(\sqrt{4 \, ft} - \sqrt{2 \, ft}\right)}{\sqrt{\frac{32.2}{2}}} \left(\frac{3 \times 12 \, in}{0.5 \, in}\right)^2 = 757 \, s = 12.6 \, min$$

What does the entire flow exit the system?

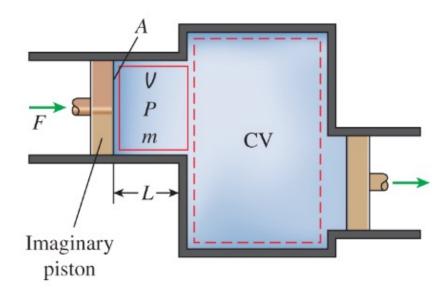
$$t = \frac{\left(\sqrt{4 \, ft} - \sqrt{0 \, ft}\right)}{\sqrt{\frac{32.2}{2}}} \left(\frac{3 \times 12 \, in}{0.5 \, in}\right)^2 = 43.1 \, min$$

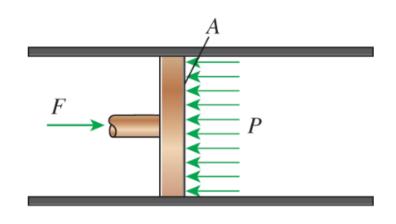
## FLOW WORK AND ENERGY OF FLOWING FLUID

 Flow work (or flow energy): The work (or energy) required to push the mass into or out of the control volume. This work is necessary for maintaining a continuous flow through a control volume



 If the fluid pressure is P and the cross-sectional area of the fluid element is A, the force applied on the fluid by the imaginary piston is:





F = PA

 To push the entire fluid element into the control volume, this force must act through a distance L

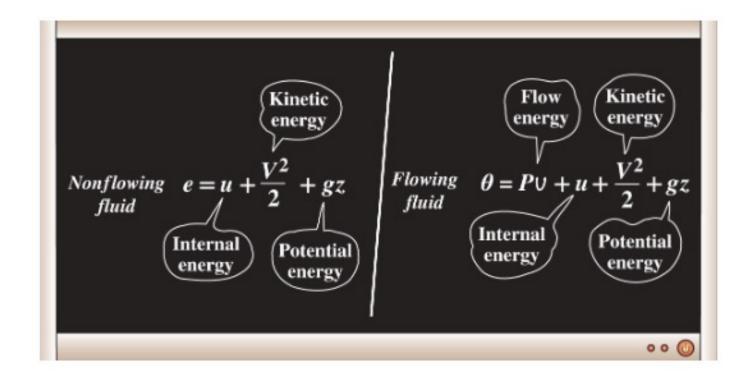
$$F = PA$$

$$W_{flow} = FL = PAL = P \forall$$
(a) Before entering
$$W_{flow} = Pv$$

$$W_{flow} = Pv$$
(b) CV

(b) After entering

• Total energy of a flowing fluid is:

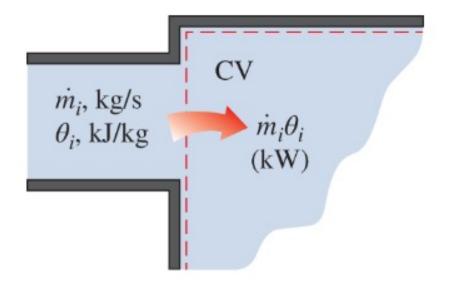


 $\theta = Pv + e = Pv + (u + ke + pe) = (u + Pv) + ke + pe$ 

• Energy transport by mass:

$$E_{mass} = m\theta = m(h + \frac{V^2}{2} + gz)$$

$$\dot{E}_{mass} = \dot{m}\theta = \dot{m}(h + \frac{v}{2} + gz)$$



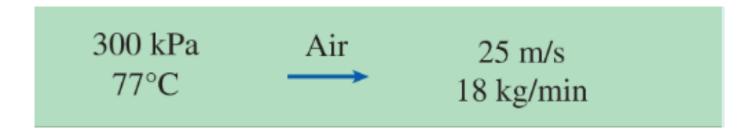
• What does happen when mass is not constant:

$$E_{in,mass} = \int_{m_i} \theta_i \delta m_i = \int_{m_i} (h_i + \frac{V_i^2}{2} + gz_i) \, \delta m_i$$

### **CLASS ACTIVITY**

#### **Class Activity**

- Air flows steadily in a pipe at 300 kPa, 77 °C, and 25 m/s at a rate of 18 kg/min. Determine:
  - a) The diameter of the pipe
  - b) The rate of flow energy
  - c) The rate of energy transport by mass
  - d) The error involved in part c if the kinetic energy is neglected.



#### **Class Activity**

Solution (assumptions):
The flow is steady
The potential energy is negligible
R = 0.287 kJ/kg-K
c<sub>p</sub>=1.008 kJ/kg-K (at 350 K from Table A-2b)

• Solution (a):

$$v = \frac{RT}{P} = \frac{(0.287 \frac{kJ}{kg - K})(77 + 273)}{300 \, kPa} = 0.3349 \frac{m^3}{kg}$$

$$A = \frac{\dot{m}v}{\forall} = \frac{\left(\frac{18}{60}\frac{kg}{s}\right)(0.3349\frac{m^3}{kg})}{25\frac{m}{s}} = 0.004018\ m^2$$

$$D = \sqrt{\frac{4A}{\pi}} = \sqrt{\frac{4(0.004018 \ m^2)}{\pi}} = 0.0715 \ m$$

• Solution (b):

$$\dot{W}_{flow} = \dot{m}Pv = \left(\frac{18}{60}\frac{kg}{s}\right)(300\ kPa)\left(0.3349\frac{m^3}{kg}\right) = 30.14\ kW$$

• Solution (c):

$$\dot{E}_{mass} = \dot{m}(h + ke) = \dot{m}(c_pT + \frac{V^2}{2})$$

$$\dot{E}_{mass} = \left(\frac{18}{60} \frac{kg}{s}\right) \left[ \left(1.008 \frac{kJ}{kg - K}\right) (77 + 273 K) + \left(\frac{1}{2}\right) \left(25 \frac{m}{s}\right)^2 \left(\frac{1 \frac{kJ}{kg}}{1000 \frac{m^2}{s^2}}\right) \right]$$

 $\dot{E}_{mass} = 105.94 \ kW$ 

• Solution (d):

 $\dot{E}_{mass} = \dot{m}(h + ke) = \dot{m}h = \dot{m}c_pT$ 

$$\dot{E}_{mass} = \dot{m}c_p T = \left(\frac{18}{60}\frac{kg}{s}\right) \left(1.005\frac{kJ}{kg-K}\right)(77 + 273K) = 105.84 \ kW$$

# ENERGY ANALYSIS OF STEADY-FLOW SYSTEMS

#### **Energy Analysis of Steady-Flow Systems**

 A large number of engineering devices such as turbines, compressors, and nozzles operate for long periods of time under the same conditions once the transient start-up period is completed and steady operation is established, and they are classified as *steady-flow devices*.



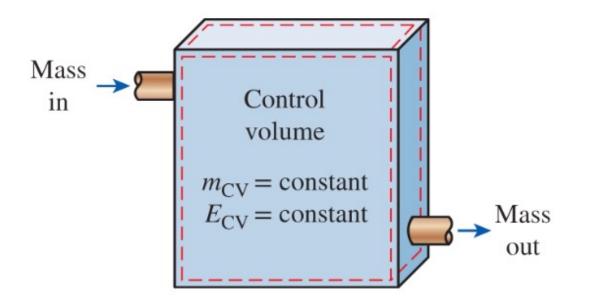
#### **Energy Analysis of Steady-Flow Systems**

 Process involving such devices can be represented reasonably well by a somewhat idealized process, called steady-flow process which was defined as a process during which a fluid flows through a control volume steadily

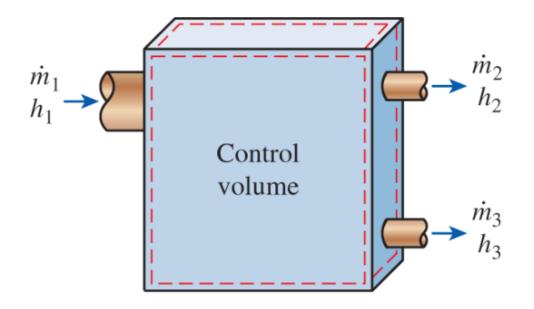
What do you think about a spatial and temporal change in a tank with a steady-flow?

- Steady-flow process:
  - No intensive or extensive properties within the control volume change with time
  - □ Boundary work is zero (why?)

$$\Box \Delta E_{CV} = 0 \text{ (why?)}$$



Steady-flow process:
 Power remain constant why?



• Steady-flow process:

$$\sum_{in} \dot{m} = \sum_{out} \dot{m}$$

$$\dot{m}_1=\dot{m}_2 \rightarrow \rho_1 A_1 V_1=\rho_2 A_2 V_2$$

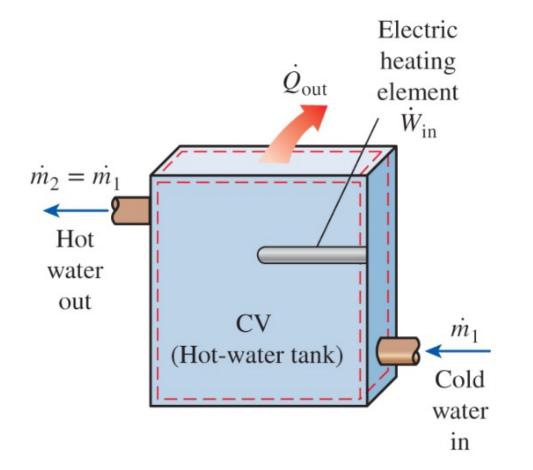
• Steady-flow process:

$$\dot{E}_{in} - \dot{E}_{out} = \frac{dE_{system}}{dt} = 0 \qquad \rightarrow \qquad \qquad \dot{E}_{in} = \dot{E}_{out}$$

$$\dot{Q}_{in} + W_{in} + \sum_{in} \dot{m}\theta = \dot{Q}_{out} + W_{out} + \sum_{out} \dot{m}\theta$$

$$\dot{Q}_{in} + W_{in} + \sum_{in} \dot{m}(h + \frac{V^2}{2} + gz) = \dot{Q}_{out} + W_{out} + \sum_{out} \dot{m}(h + \frac{V^2}{2} + gz)$$

Consider an electric hot water heater under steady condition



Consider an electric hot water heater under steady condition

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m} \left( h + \frac{V^2}{2} + gz \right) - \sum_{in} \dot{m} (h + \frac{V^2}{2} + gz)$$

$$\dot{Q} - \dot{W} = \dot{m} \left( h_2 - h_1 + \frac{V_2^2 - V_1^2}{2} + g(z_2 - z_1) \right)$$

$$q - w = h_2 - h_1 + \frac{V_2^2 - V_1^2}{2} + g(z_2 - z_1)$$

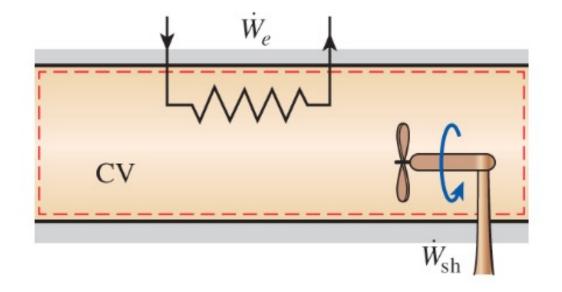
 $q - w = h_2 - h_1$ 

• Let's look at  $\dot{Q}$ 

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m} \left( h + \frac{V^2}{2} + gz \right) - \sum_{in} \dot{m} (h + \frac{V^2}{2} + gz)$$

• Let's look at  $\dot{W}$ :

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m} \left( h + \frac{V^2}{2} + gz \right) - \sum_{in} \dot{m} (h + \frac{V^2}{2} + gz)$$



• Let's look at  $\Delta h = h_2 - h_1 = c_{p,avg}(T_2 - T_1)$ 

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m} \left( h + \frac{V^2}{2} + gz \right) - \sum_{in} \dot{m} (h + \frac{V^2}{2} + gz)$$

• Let's look at  $\Delta ke$ 

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m} \left( h + \frac{V^2}{2} + gz \right) - \sum_{in} \dot{m} \left( h + \frac{V^2}{2} + gz \right)$$

o				
0	$V_1$	$V_2$	Δke	
	m/s	m/s	kJ/kg	
	0	45	1	
	50	67	1	
	100	110	1	
	200	205	1	
	500	502	1	
0				
~	~			~

$$\frac{J}{kg} \equiv \frac{N \cdot m}{kg} \equiv \left(kg\frac{m}{s^2}\right) \frac{m}{kg} \equiv \frac{m^2}{s^2}$$
$$\left(Also, \frac{Btu}{lbm} \equiv 25,037 \frac{ft^2}{s^2}\right)$$

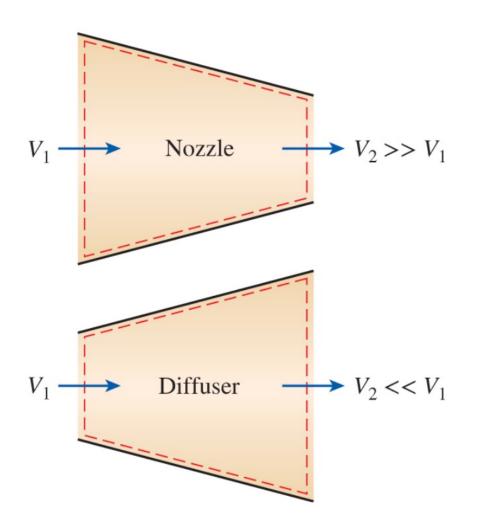
• Let's look at  $\Delta pe$  (when do you think it becomes important?)

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m} \left( h + \frac{V^2}{2} + gz \right) - \sum_{in} \dot{m} (h + \frac{V^2}{2} + gz)$$

# SOME STEADY-FLOW ENGINEERING DEVICES

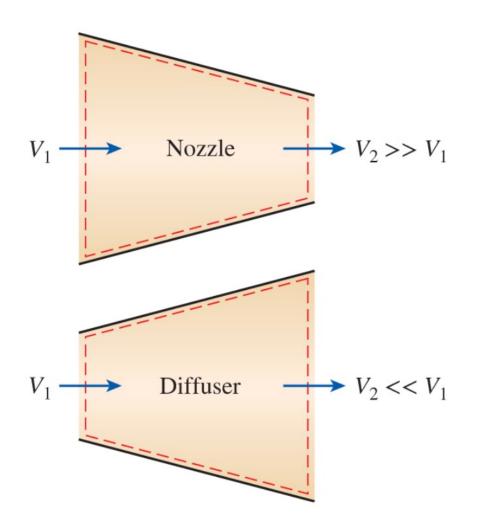
#### **Some Steady-Flow Energy Devices**

Nozzles and Diffusers



#### **Some Steady-Flow Energy Devices**

Nozzles and Diffusers



 $\dot{Q} \cong 0$  $\dot{W} = 0 (most times)$  $\Delta pe \cong 0$ 

 $\Delta ke \neq 0$ 

# **CLASS ACTIVITY**

# **Class Activity**

- Air at 10 °C and 80 kPa enters the diffuser of a jet engine steadily with a velocity of 200 m/s. The inlet area of the diffuser is 0.4 m<sup>2</sup>. The air leaves the diffuser with a velocity that is very small compared with the inlet velocity. Determine:

   a) The mass flow rate of the air
  - b) The temperature of the air leaving the diffuser

- Solution (assumptions):
  - 1. This is a steady-flow process ( $\Delta m_{CV} = 0$  and  $\Delta E_{CV} = 0$ )
  - 2. Air is an ideal gas since it is at a high temperature and low pressure relative to its critical-point values
  - 3. The potential energy balance change is zero
  - 4.  $\Delta pe = 0$
  - 5. Heat transfer is negligible
  - 6. Kinetic energy at the diffuser exit is negligible
  - 7. There are no work interactions

#### **Class Activity**

• Solution (a):

 $\dot{m}_1 = \dot{m}_2 = \dot{m}$ 

$$v_1 = \frac{RT_1}{P_1} = \frac{\left(0.287 \ kPa - \frac{m^3}{kg - K}\right)(283 \ K)}{80 \ kPa} = 1.015 \frac{m^3}{kg}$$



## **Class Activity**

• Solution (b):

$$\dot{E}_{in}=\dot{E}_{out}=\frac{dE_{system}}{dt}=0$$

 $\dot{E}_{in} = \dot{E}_{out}$ 

$$\dot{m}\left(h_1 + \frac{V_1^2}{2}\right) = \dot{m}(h_2 + V_2^2)$$

$$h_2 = h_1 - \frac{V_2^2 - V_1^2}{2}$$



 $(V_2^2 \ll V_1^2)$ 

• Solution (b):

Using Table A - 21 
$$\rightarrow h_1 = h_{@ 283 K} = 283.14 \frac{kJ}{kg}$$



$$h_2 = 283.14 \frac{kJ}{kg} - \frac{0 - \left(200 \frac{m}{s}\right)^2}{2} \left(\frac{1 \frac{kJ}{kg}}{1000 \frac{m^2}{s^2}}\right) = 303.14 \frac{kJ}{kg}$$

From Table  $A - 21 \rightarrow T_2 = 303 K$