

# MAPPING OUTDOOR PARTICLE SIZE DISTRIBUTIONS TO HVAC FILTRATION EFFICIENCY FOR PM<sub>2.5</sub> AND ULTRAFINE PARTICLES

BERGs Summer Meeting Presentation

June/10/2014

Parham Azimi

Dan Zhao



# PARTICULATE MATTER

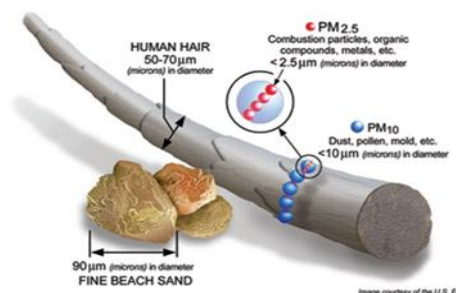
Tiny pieces of solid or liquid matter associated with the Earth's atmosphere.

Source: dust, motor vehicles, power plants

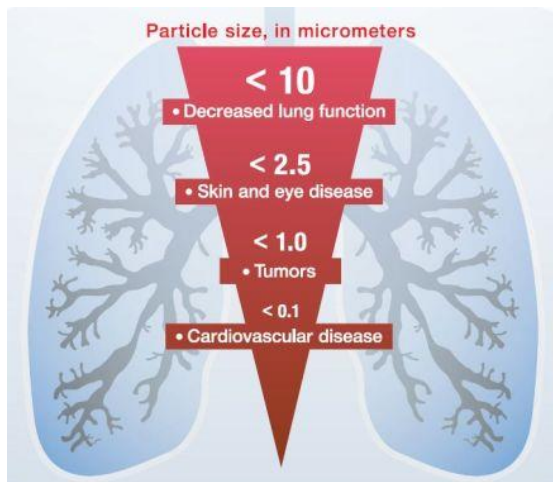
**PM10:** particles smaller than 10  $\mu\text{m}$

**PM2.5:** particles smaller than 2.5  $\mu\text{m}$

**UFP:** Ultrafine Particles, smaller than 100 nm



<http://www.epa.gov/airquality/particulatematter/basic.html>

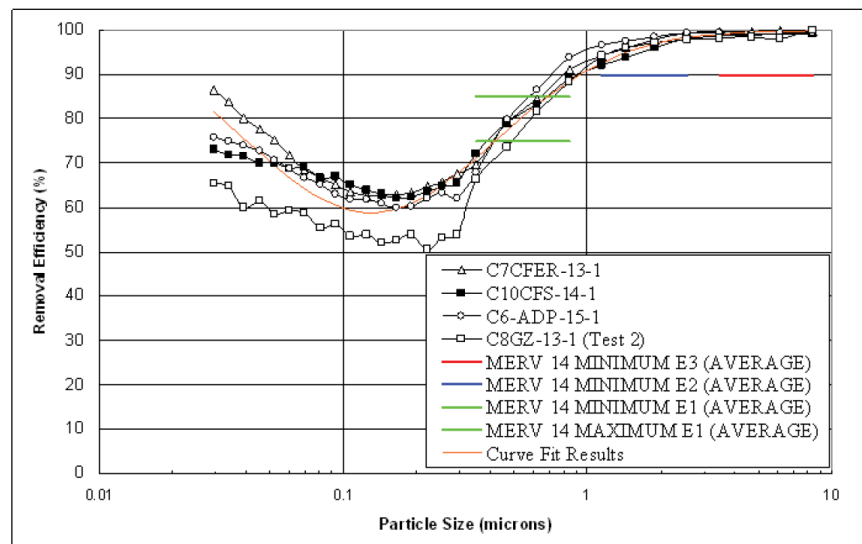


[http://www.tesa-clean-air.com/eng/fine\\_dust\\_particles](http://www.tesa-clean-air.com/eng/fine_dust_particles)



# HVAC FILTERS

- ASHRAE classify the HVAC filters with standard 52.2 based on **measured efficiency** and pressure drop after subjecting filter to test aerosols. The results is **MERV** (Minimum efficiency reporting value)
- It is based on minimum values for three particle size ranges.
  - E1: 0.3-1  $\mu\text{m}$
  - E2: 1-3  $\mu\text{m}$
  - E3: 3-10  $\mu\text{m}$



**TABLE 12-1 Minimum Efficiency Reporting Value (MERV) Parameters**

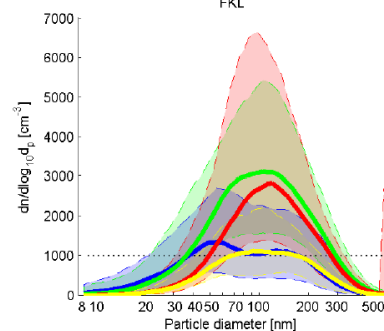
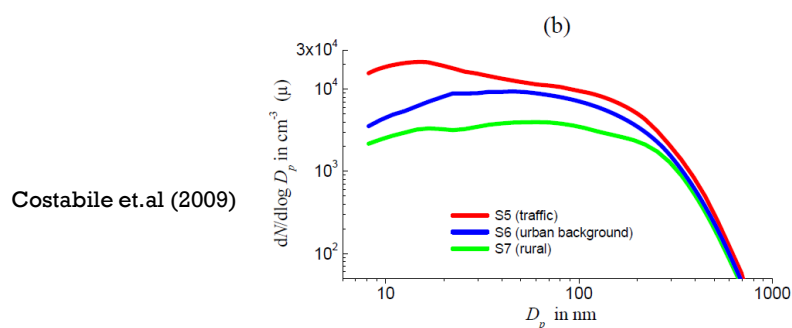
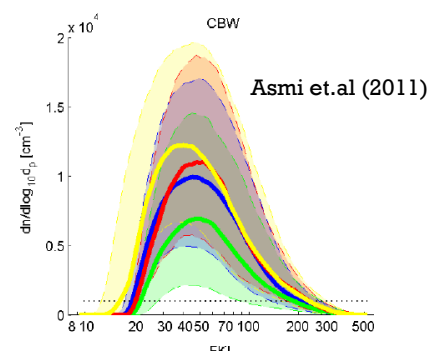
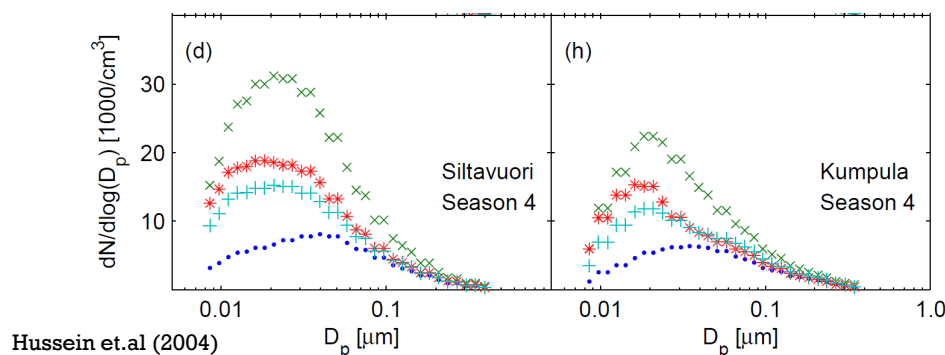
Standard 52.2 Minimum Efficiency Reporting Value (MERV)	Composite Average Particle Size Efficiency,% in Size Range, $\mu\text{m}$			Average Arrestance,%, by Standard 52.1 Method	Minimum Final Resistance	
	Range 1 0.30–1.0	Range 2 1.0–3.0	Range 3 3.0–10.0		Pa	in. of water
1	n/a	n/a	$E_3 < 20$	$A_{avg} < 65$	75	0.3
2	n/a	n/a	$E_3 < 20$	$65 \leq A_{avg} < 70$	75	0.3
3	n/a	n/a	$E_3 < 20$	$70 \leq A_{avg} < 75$	75	0.3
4	n/a	n/a	$E_3 < 20$	$75 \leq A_{avg}$	75	0.3
5	n/a	n/a	$20 \leq E_3 < 35$	n/a	150	0.6
6	n/a	n/a	$35 \leq E_3 < 50$	n/a	150	0.6
7	n/a	n/a	$50 \leq E_3 < 70$	n/a	150	0.6
8	n/a	n/a	$70 \leq E_3$	n/a	150	0.6
9	n/a	$E_2 < 50$	$85 \leq E_3$	n/a	250	1.0
10	n/a	$50 \leq E_2 < 65$	$85 \leq E_3$	n/a	250	1.0
11	n/a	$65 \leq E_2 < 80$	$85 \leq E_3$	n/a	250	1.0
12	n/a	$80 \leq E_2$	$90 \leq E_3$	n/a	250	1.0
13	$E_1 < 75$	$90 \leq E_2$	$90 \leq E_3$	n/a	350	1.4
14	$75 \leq E_1 < 85$	$90 \leq E_2$	$90 \leq E_3$	n/a	350	1.4
15	$85 \leq E_1 < 95$	$90 \leq E_2$	$90 \leq E_3$	n/a	350	1.4
16	$95 \leq E_1$	$95 \leq E_2$	$95 \leq E_3$	n/a	350	1.4

HEPA  $\rightarrow$  99.9% or greater removal efficiency for most particle sizes



# PARTICLE-SIZE DISTRIBUTIONS

- Number and mass concentration of particles are varied for different particle sizes.
- Also it is changing during day or from one location to other one. Even the shape of distribution can be changed.



Costabile et.al Spatio-temporal variability and principal components of the particle number size distribution in an urban atmosphere, Atmos. Chem. Phys., 9, 3163–3195, 2009

T. Hussein et.al. Urban aerosol number size distributions Atmos. Chem. Phys., 4, 391–411, 2004.

A.Asmi et.al. Number size distributions and seasonality of submicron particles in Europe 2008–2009, Atmos. Chem. Phys., 11, 5505–5538, 2011



# MAIN GOAL

- We want to find **UFP and PM2.5 removal efficiency** of different HVAC filters.
- It is a function of size-resolved removal efficiency of filters and size distribution of outdoor particles.

$$RE_{UFP} = 1 - \frac{\sum_{i=1}^{100} N_i \times (1 - R_i)}{\sum_{i=1}^{100} N_i}$$

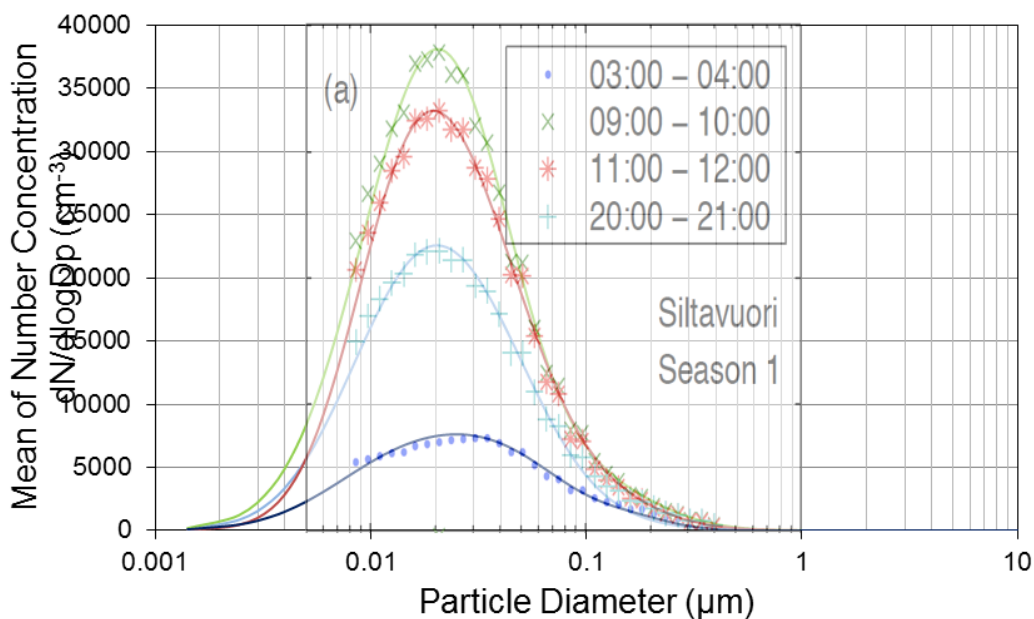
$$RE_{PM2.5} = 1 - \frac{\sum_{i=1}^{2500} N_i \times \rho_i \times \frac{\pi d_i^3}{6} \times (1 - R_i)}{\sum_{i=1}^{2500} N_i \times \rho_i \times \frac{\pi d_i^3}{6}}$$

- $RE_{UFP}$ : UFP Removal efficiency of a filter
- $RE_{PM2.5}$ : UFP Removal efficiency of a filter
- $d_i$ : diameter size of particles in size bin  $i$  (nm)
- $N_i$ : Number of concentration of particles with diameter of  $d_i$
- $R_i$ : Removal efficiency of filter for particles with diameter of  $d_i$
- $\rho_i$ : Density of particles with diameter of  $d_i$  (gr/cm<sup>3</sup>)



# MODELING PARTICLE-SIZE DISTRIBUTION OF AEROSOLS

- The most common way to present particle size distribution data for aerosols is in term of three modes, the **nuclei**, **accumulation**, and **coarse particle** modes. Each mode is a log normal distribution which they are added together.



Mode 1	N, #/cm <sup>3</sup>	24300
	Dp, $\mu\text{m}$	0.017
	log SD	0.33
Mode 2	N, #/cm <sup>3</sup>	8000
	Dp, $\mu\text{m}$	0.03
	log SD	0.28
Mode 3	N, #/cm <sup>3</sup>	2000
	Dp, $\mu\text{m}$	0.12
	log SD	0.28

	N, #/cm <sup>3</sup>	15800
	Dp, $\mu\text{m}$	0.0145
Mode 1	log SD	0.27
	N, #/cm <sup>3</sup>	12000
	Dp, $\mu\text{m}$	0.033
Mode 2	log SD	0.28
	N, #/cm <sup>3</sup>	2000
	Dp, $\mu\text{m}$	0.1
Mode 3	log SD	0.3

	N, #/cm <sup>3</sup>	13000
	Dp, $\mu\text{m}$	0.015
Mode 1	log SD	0.32
	N, #/cm <sup>3</sup>	8000
	Dp, $\mu\text{m}$	0.035
Mode 2	log SD	0.31
	N, #/cm <sup>3</sup>	200
	Dp, $\mu\text{m}$	0.15
Mode 3	log SD	0.25

Mode 1	N, #/cm <sup>3</sup>	5000
	Dp, $\mu\text{m}$	0.015
	log SD	0.35
Mode 2	N, #/cm <sup>3</sup>	3200
	Dp, $\mu\text{m}$	0.045
	log SD	0.3
Mode 3	N, #/cm <sup>3</sup>	300
	Dp, $\mu\text{m}$	0.17
	log SD	0.18



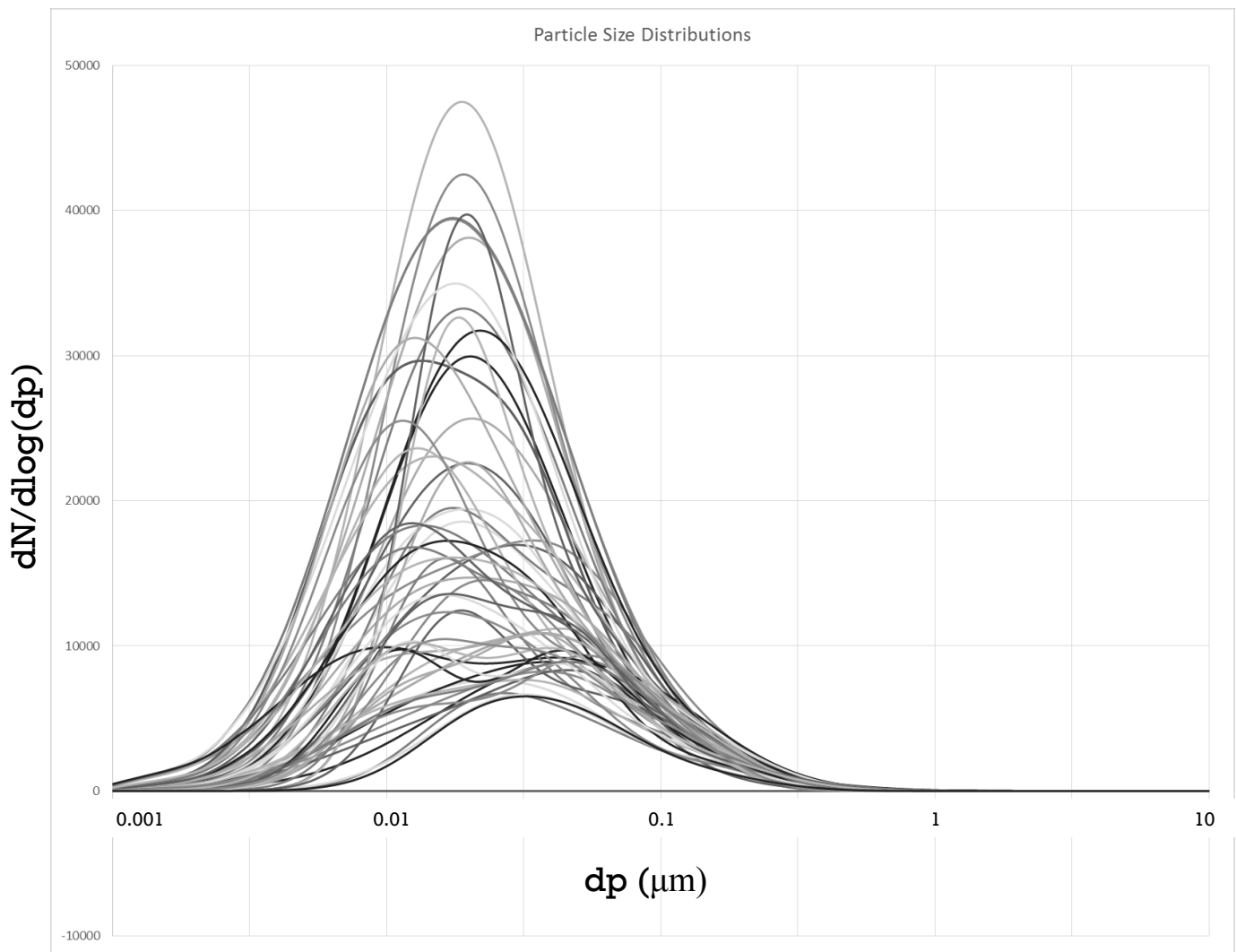
# SUMMARY OF PARTICLE SIZE DISTRIBUTIONS

- We have found the mass concentration of particles from number concentration assuming
  - The particles are spherical
  - Density of particles is constant and equal to 1 gr/cm<sup>3</sup> or it is varied from 1.25 gr/cm<sup>3</sup> to 1.75 gr/cm<sup>3</sup> with average of 1.3 g/cm<sup>3</sup> for  $dp < 140 \text{ nm}$ ; 1.4 g/cm<sup>3</sup> for  $140 \text{ nm} \leq dp < 420 \text{ nm}$ ; 1.5 g/cm<sup>3</sup> for  $420 \text{ nm} \leq dp < 1.2 \text{ }\mu\text{m}$ ; 1.6 g/cm<sup>3</sup> for  $1.2 \text{ }\mu\text{m} \leq dp < 3.5 \text{ }\mu\text{m}$ ; 1.7 g/cm<sup>3</sup> for  $3.5 \text{ }\mu\text{m} \leq dp < 10 \text{ }\mu\text{m}$ .
- We totally found and modeled
  - 197 distribution
  - From 40 locations all over the world (urban, rural and close to traffic)
  - From 12 different references and studies
  - which measured the long term size-resolved concentration of particles (more than 1 year)

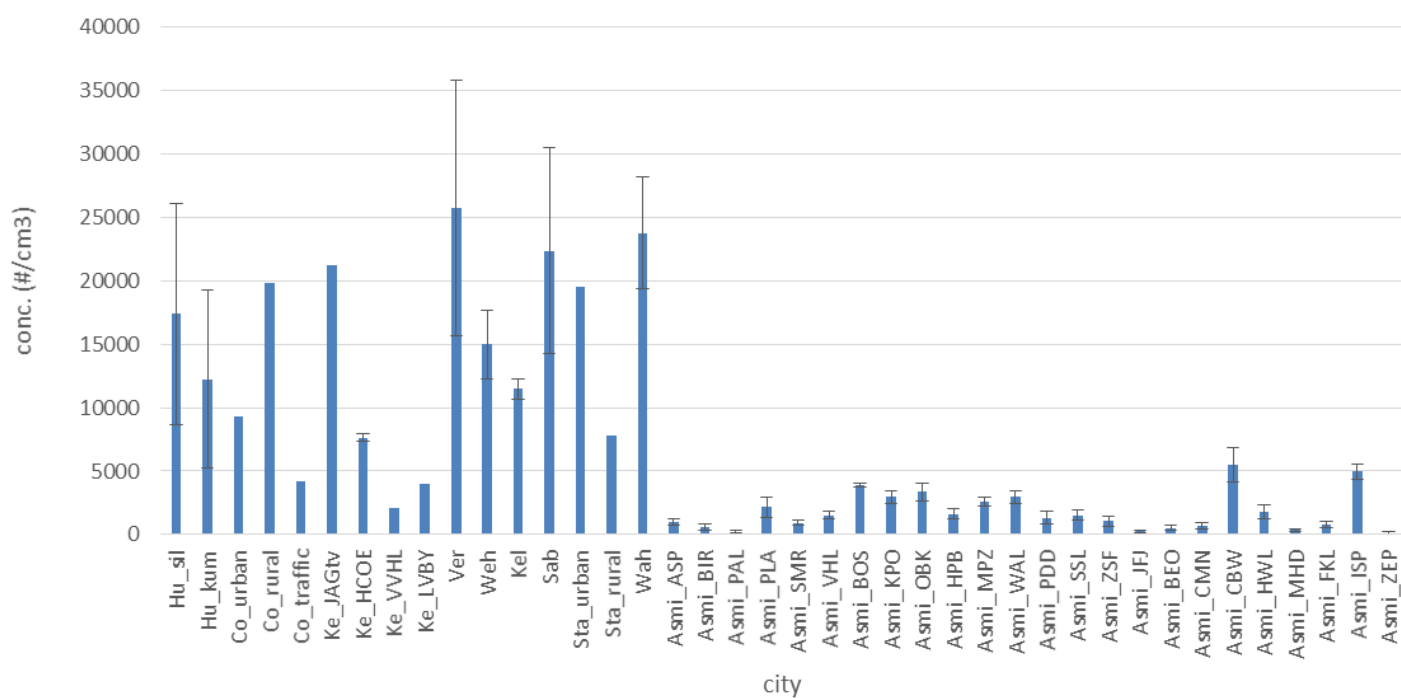
NO	Ref	Location Type	Location Name	Exp. duration	Season	UFP (#/cm <sup>3</sup> )	PM2.5 case 1 ( $\mu\text{g}/\text{cm}^3$ )	PM2.5 case 2 ( $\mu\text{g}/\text{cm}^3$ )	daytime	other charac.	MODE 1			MODE 2			MODE 3		
											N, #/cm <sup>3</sup>	Dp, $\mu\text{m}$	log SD	N, #/cm <sup>3</sup>	Dp, $\mu\text{m}$	log SD	N, #/cm <sup>3</sup>	Dp, $\mu\text{m}$	log SD
1	[1]	UR	Siltavori, EU	6 yr	WI	7785	3.1	4.4	3:00 - 4:00	Workday	16000	0.0189	0.19	8000	0.045	0.28	1800	0.11	0.25
65	[2]	UR	Schleussig, EU	2 yr	ALL	9340	15.1	21.6	N/A	Workday	800	0.06	0.28	550	0.075	0.15	400	0.18	0.2
66	[3]	RU	Melpitz, EU	2 yr	ALL	19780	17.5	24.9	N/A	Workday	3500	0.023	0.24	2000	0.06	0.24	500	0.17	0.18
180	[4]	TR	Pittsburg, US	1 yr	1	20416	3.6	5.1	morning	Workday	5100	0.022	0.27	3400	0.061	0.25	700	0.16	0.24

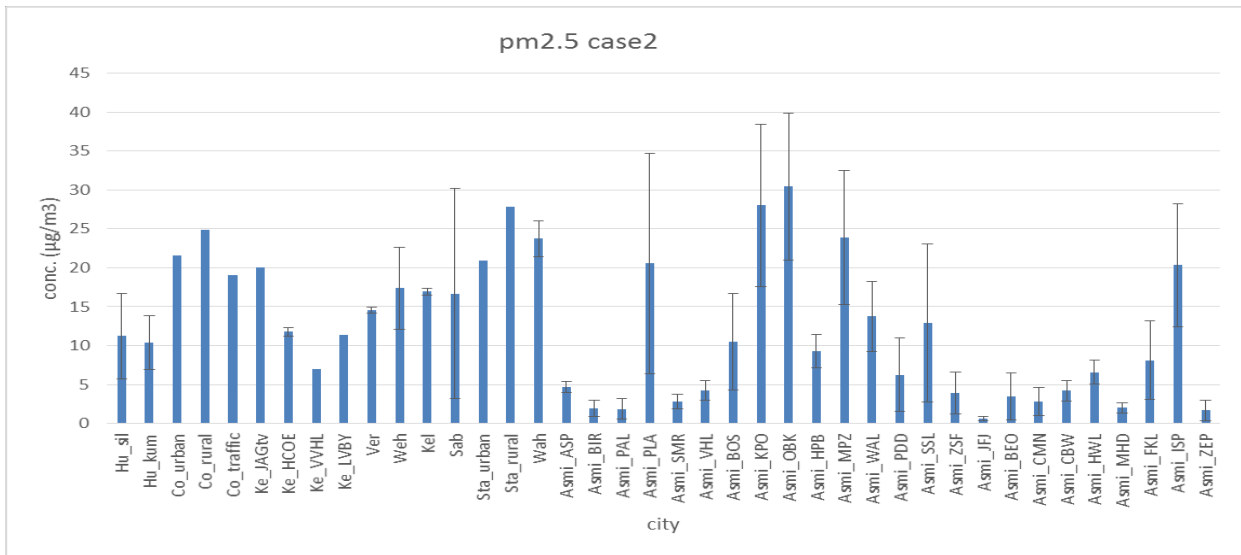
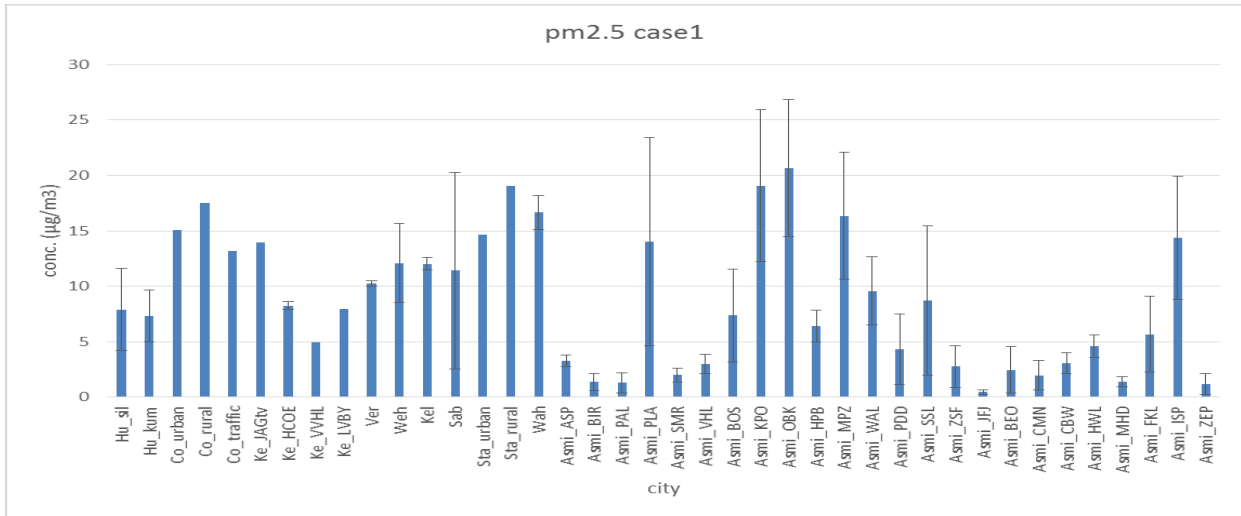






# UFP





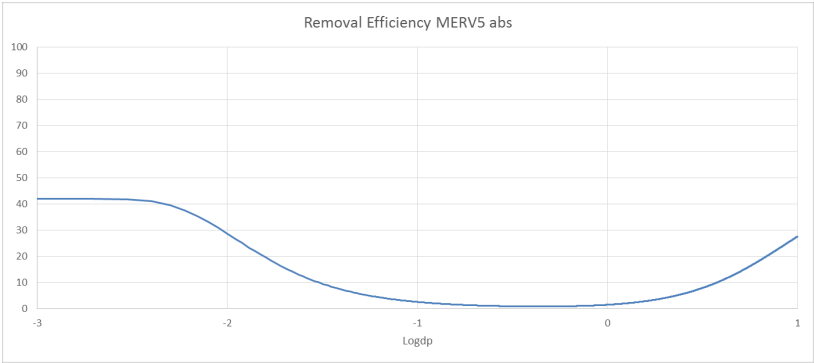
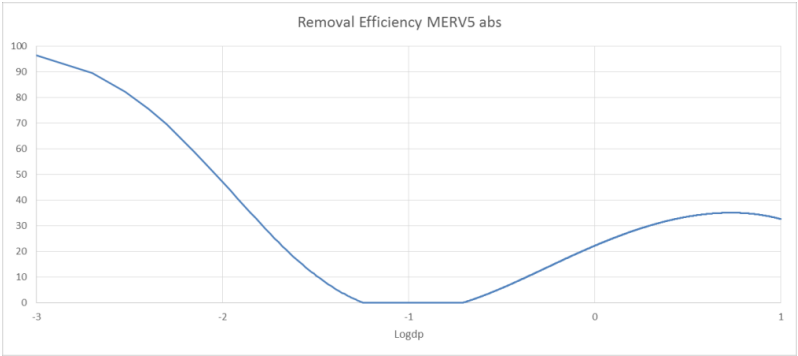
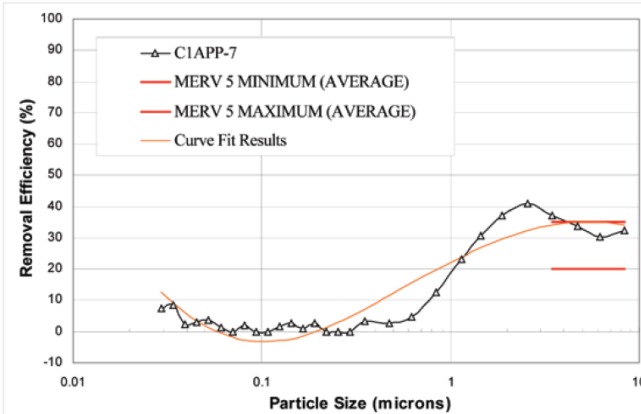
# SIZE-RESOLVE REMOVAL EFFICIENCY OF HVAC FILTERS

- We mostly used a report from EPA to find out the removal efficiency of the filters.
- They measured removal efficiency filters with 9 MERV ratings for particle sizes from 0.03  $\mu\text{m}$  to 10  $\mu\text{m}$ .

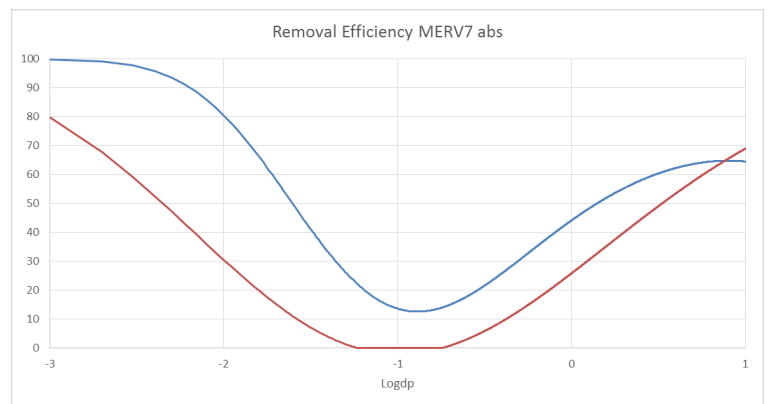
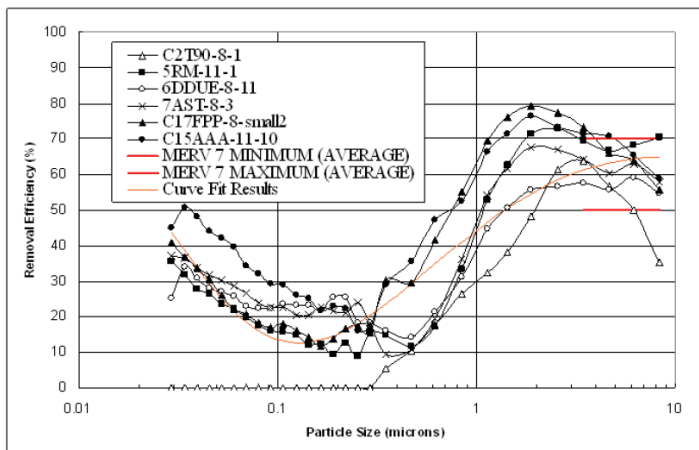
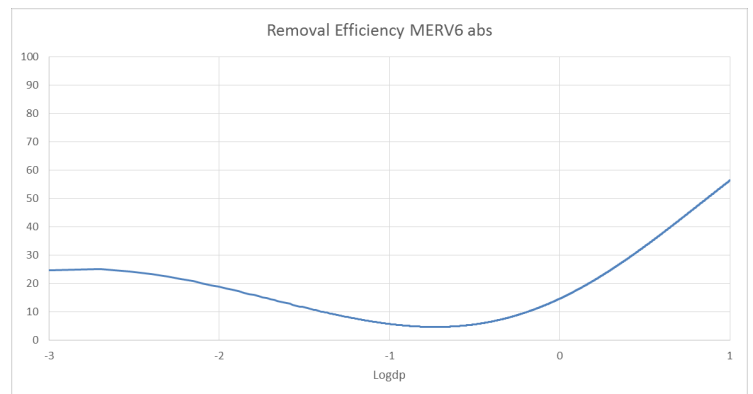
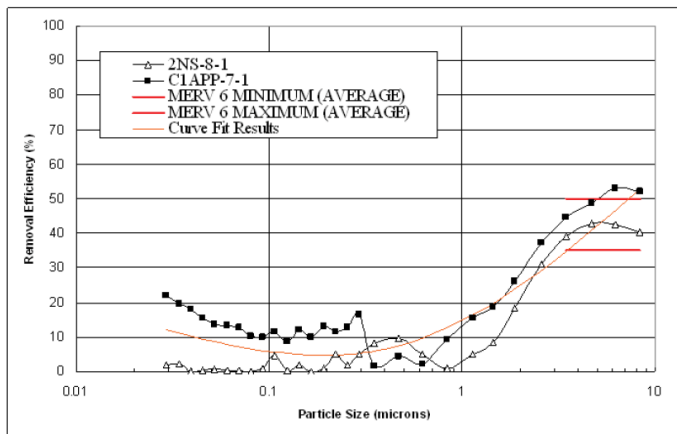
MERV Rating	Equation	Parameters	Correlation Coefficient ( $r^2$ )
5	$Y = a + bx + cx^2 + dx^3$ where $Y$ = log of percent penetration $x$ = log of particle diameter	$a = 1.8906$ $b = -0.1722$ $c = 0.0307$ $d = 0.0793$	0.8935
6	$Y = a + bx + cx^2 + dx^3$ where $Y$ = log of percent penetration $x$ = log of particle diameter	$a = 1.9311$ $b = -0.1441$ $c = -0.1243$ $d = -0.0234$	0.8332
7	$Y = a + bx + cx^2 + dx^3$ where $Y$ = log of percent penetration $x$ = log of particle diameter	$a = 1.7467$ $b = -0.3314$ $c = -0.0036$ $d = 0.1381$	0.9064
8	$(1/Y) = a + bx + cx^2 + dx^3$ where $Y$ = log of percent penetration $x$ = log of particle diameter	$a = 0.5839$ $b = 0.1675$ $c = 0.1289$ $d = 0.0188$	0.9658
10	$Y = a + bx + cx^2 + dx^3$ where $Y$ = log of percent penetration $x$ = log of particle diameter	$a = 1.7083$ $b = -0.5759$ $c = -0.6721$ $d = -0.1775$	0.9852
12	$Y = a + bx + cx^2 + dx^3$ where $Y$ = log of percent penetration $x$ = log of particle diameter	$a = 1.3943$ $b = -0.9080$ $c = -0.6240$ $d = -0.0404$	0.9902
14	$Y = a + bx + cx^2 + dx^3$ where $Y$ = log of percent penetration $x$ = log of particle diameter	$a = 0.9531$ $b = -1.4941$ $c = -0.8443$ $d = -0.0013$	0.9668
16	$\ln Y = a + bx + cx^2 + dx^3$ where $Y$ = percent penetration $x$ = log of particle diameter	$a = 0.3855$ $b = -2.0698$ $c = 0.5326$ $d = 1.3895$	0.9728
16+ (HEPA)	$Y = a + bx + cx^2 + dx^3 + ex^4$ where $Y$ = percent penetration $x$ = log of particle diameter	$a = 0.0361$ $b = -0.3506$ $c = 0.5119$ $d = 0.0481$ $e = -0.1816$	0.8917



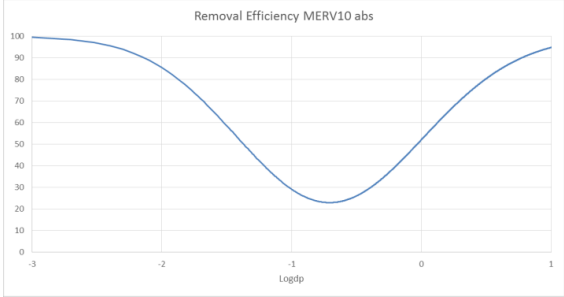
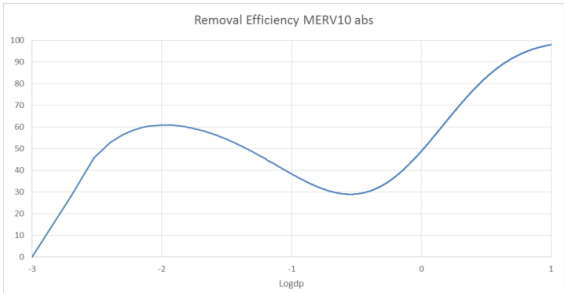
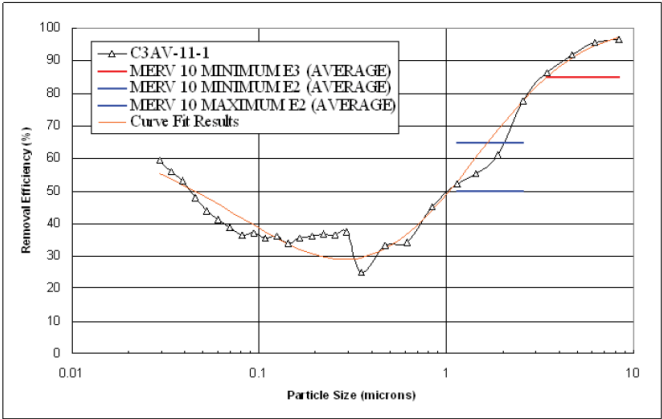
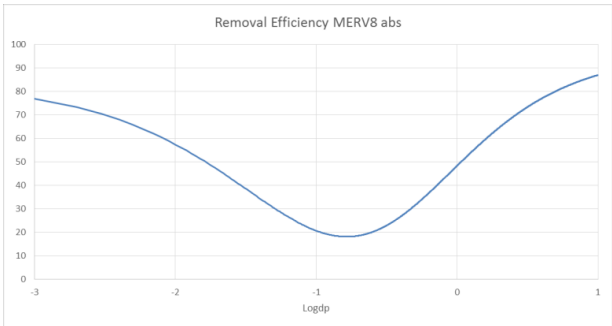
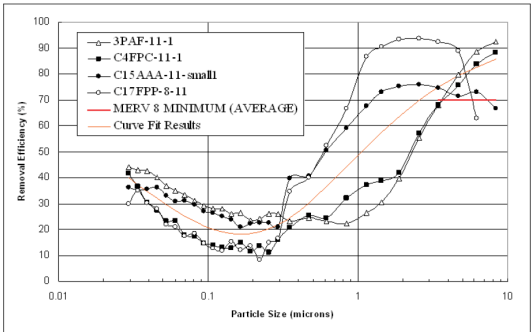
# SIZE-RESOLVE REMOVAL EFFICIENCY OF HVAC FILTERS



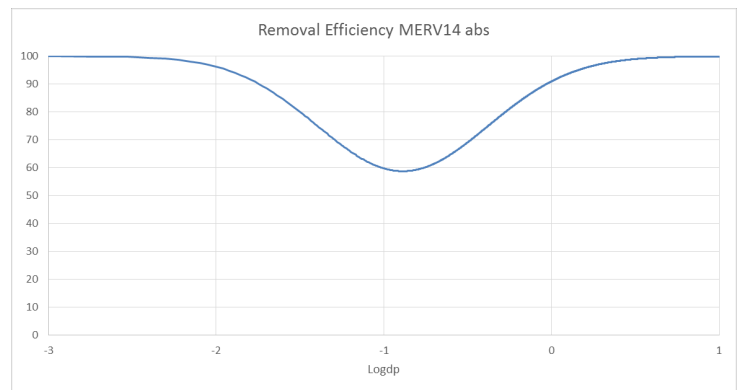
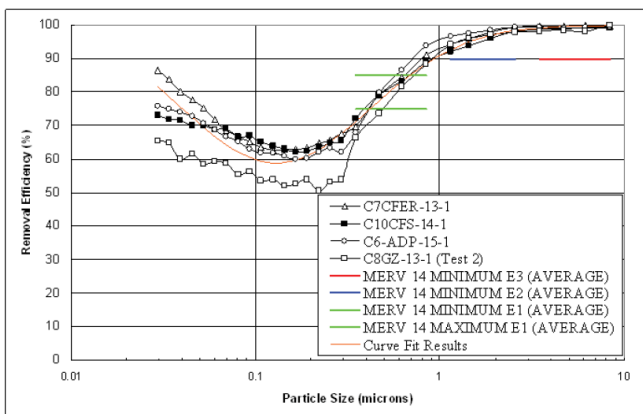
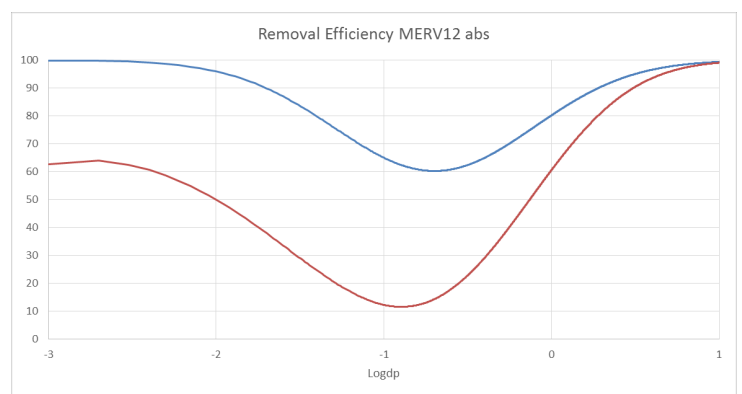
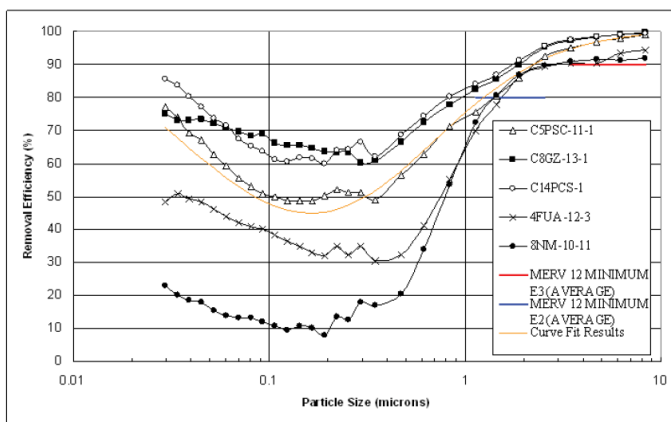
# SIZE-RESOLVE REMOVAL EFFICIENCY OF HVAC FILTERS



# SIZE-RESOLVE REMOVAL EFFICIENCY OF HVAC FILTERS

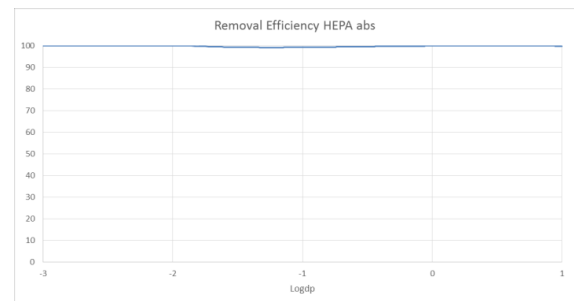
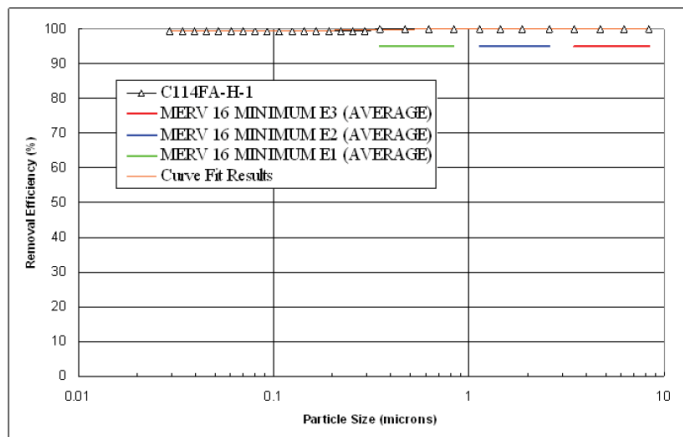
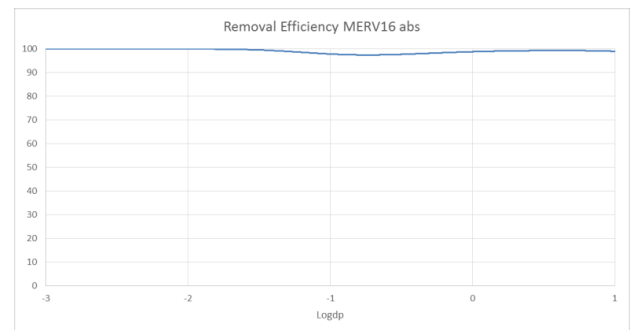
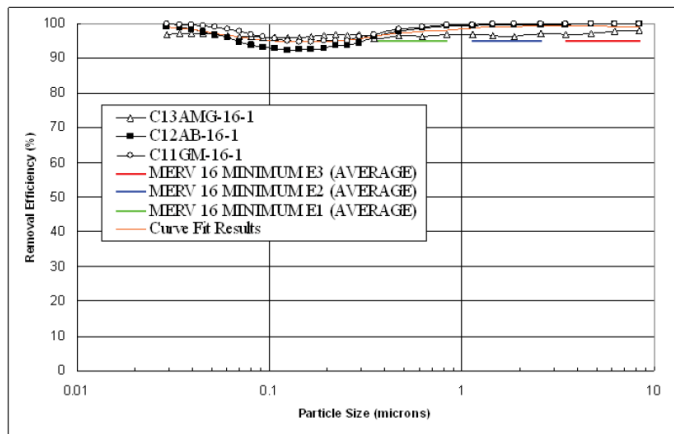


# SIZE-RESOLVE REMOVAL EFFICIENCY OF HVAC FILTERS

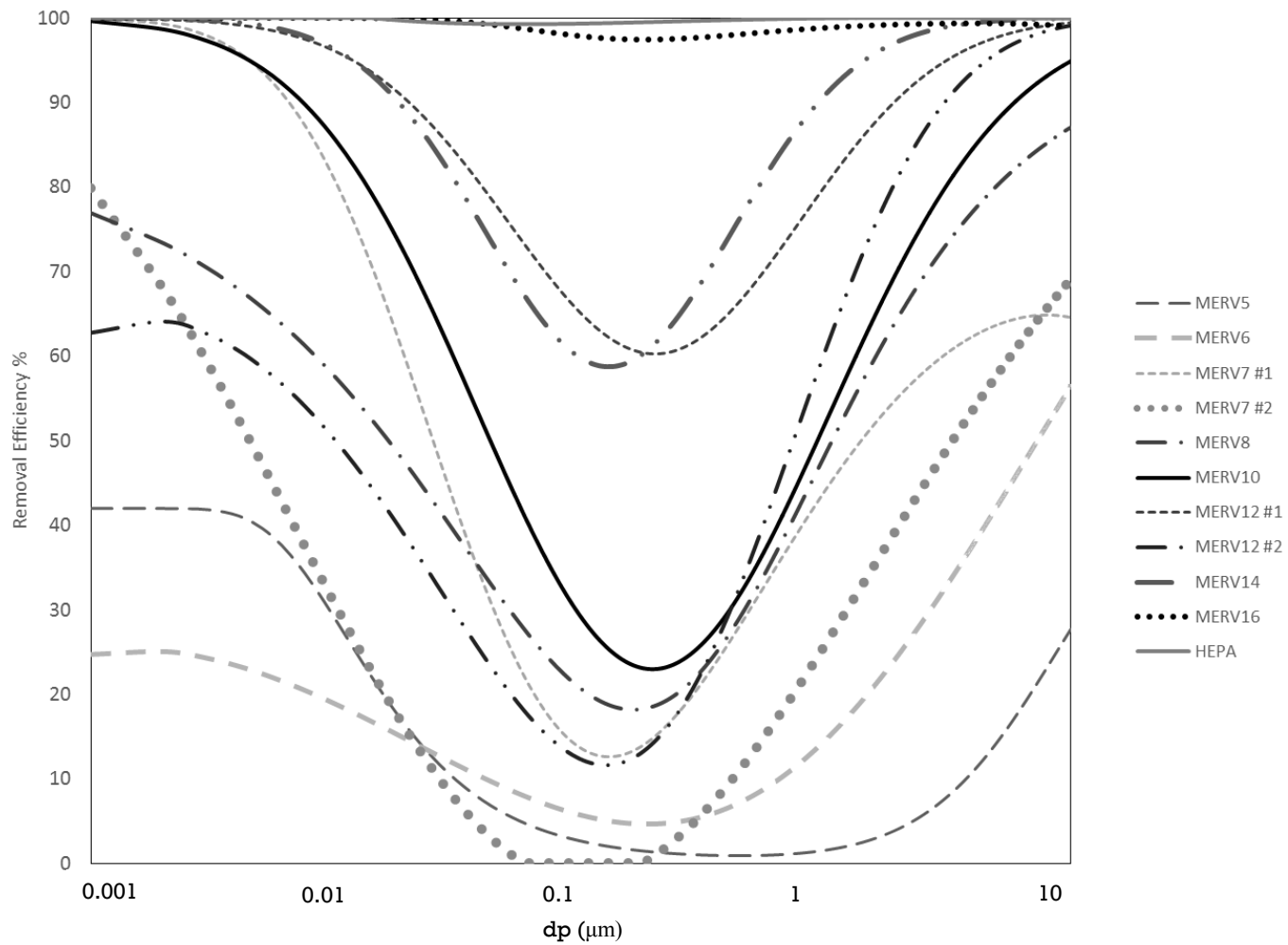




# SIZE-RESOLVE REMOVAL EFFICIENCY OF HVAC FILTERS



Removal Efficiency of HVAC Filters



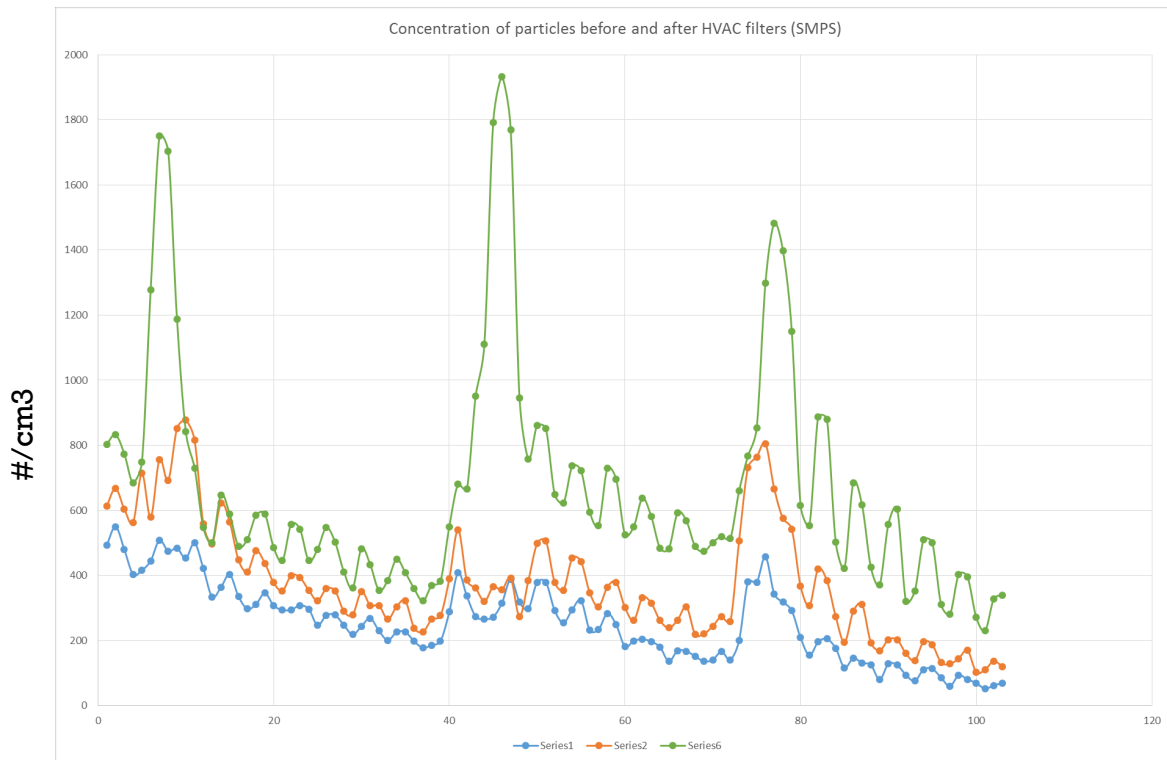
## PROBLEMS RELATED TO USING THESE REMOVAL EFFICIENCY DISTRIBUTIONS

- The removal efficiency of filters have been measured for particles sizes from 0.03 to 10  $\mu\text{m}$ . We do not know what really would happen for smaller particles.
- The modeled removal efficiency curves are not fitted to the measured data points properly
- These removal efficiencies are not measured for outdoor origin particles.

We tried to measured it for filters in StudioE but there were couple of problems:

- We measured concentration of particles before and after filters but in some cases results **were not looking reasonable**.
- The **concentration** of outdoor origin particles in some size bins was close to **zero**
- We could not reach to **steady state** conditions when the windows was open and when it was closed the concentration had been **dropped down so fast**, especially for high efficient filters





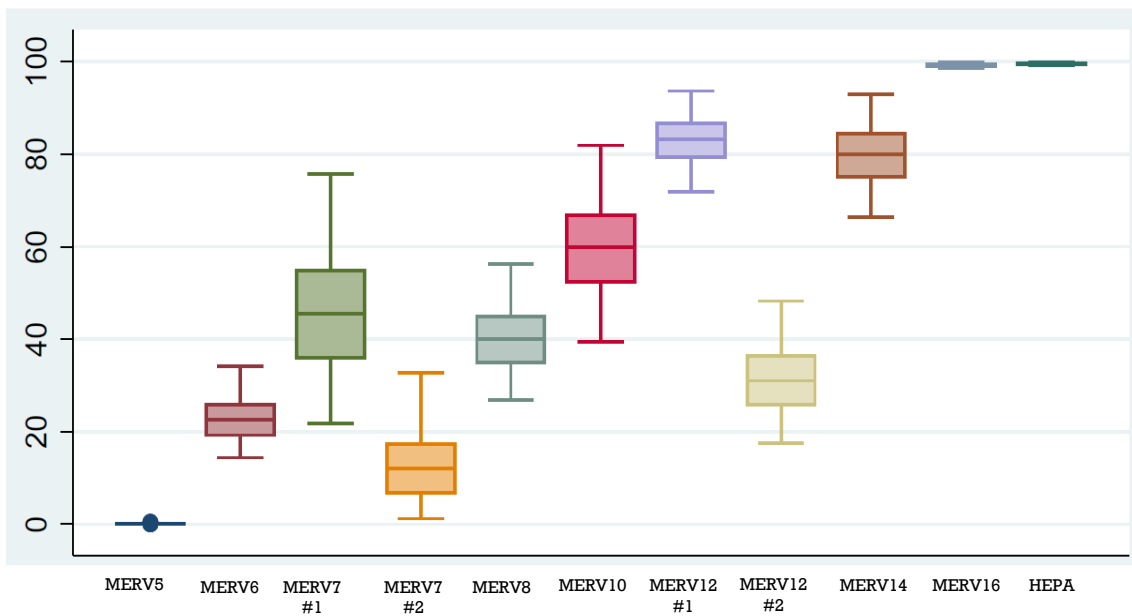
- We thought measuring the size-resolved removal efficiency of HVAC filters for outdoor origin particles would distract us from the main project, therefore we decided to leave it for now.
- We might measure removal efficiency based on the decay rate of particles. It has a capacity to become a master's thesis topic



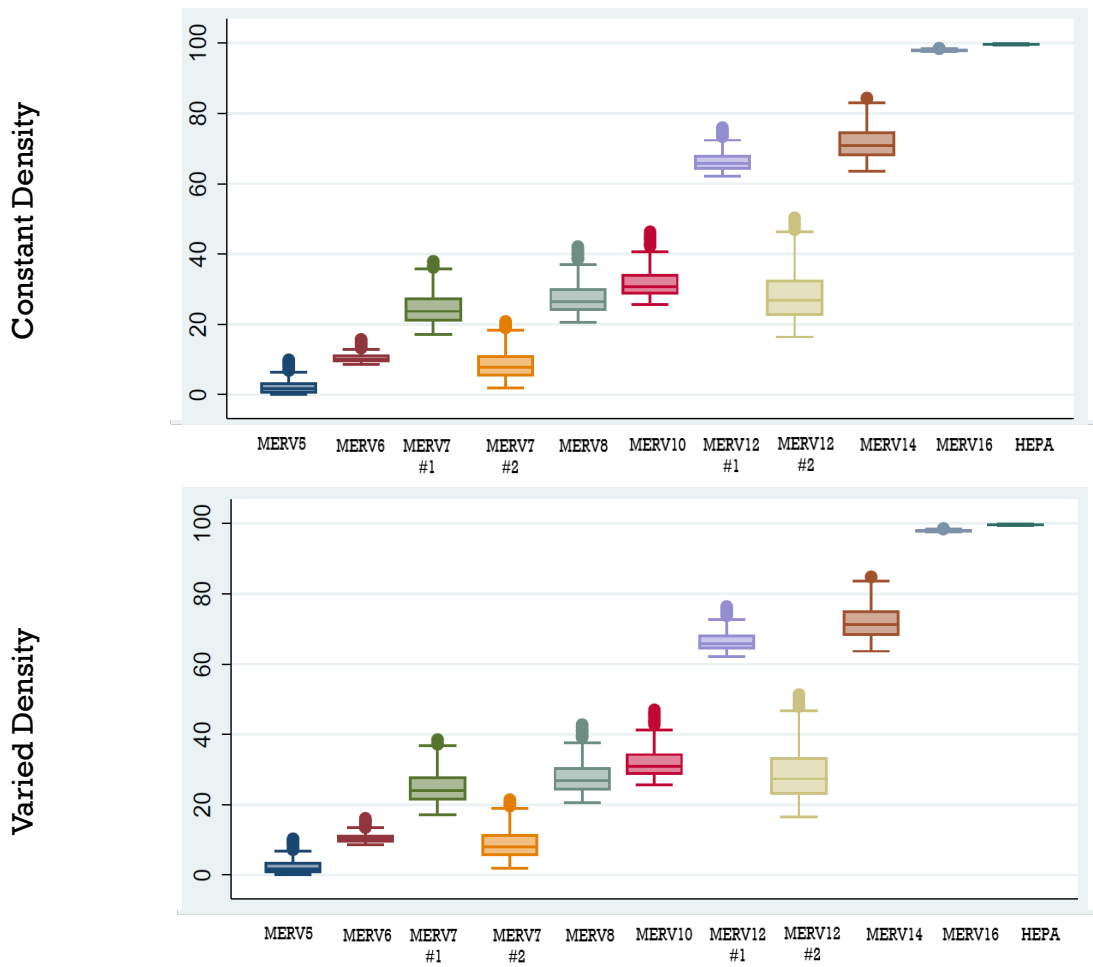
# REMOVAL EFFICIENCY OF OUTDOOR ORIGIN UFP

$$RE_{UFP} = 1 - \frac{\sum_{i=1}^{100} N_i \times (1 - R_i)}{\sum_{i=1}^{100} N_i}$$

$$RE_{PM_{2.5}} = 1 - \frac{\sum_{i=1}^{2500} N_i \times \rho_i \times \frac{\pi d_i^3}{6} \times (1 - R_i)}{\sum_{i=1}^{2500} N_i \times \rho_i \times \frac{\pi d_i^3}{6}}$$



# REMOVAL EFFICIENCY OF OUTDOOR ORIGIN PM2.5



**THANKS FOR YOUR ATTENTION**

*Questions*

